

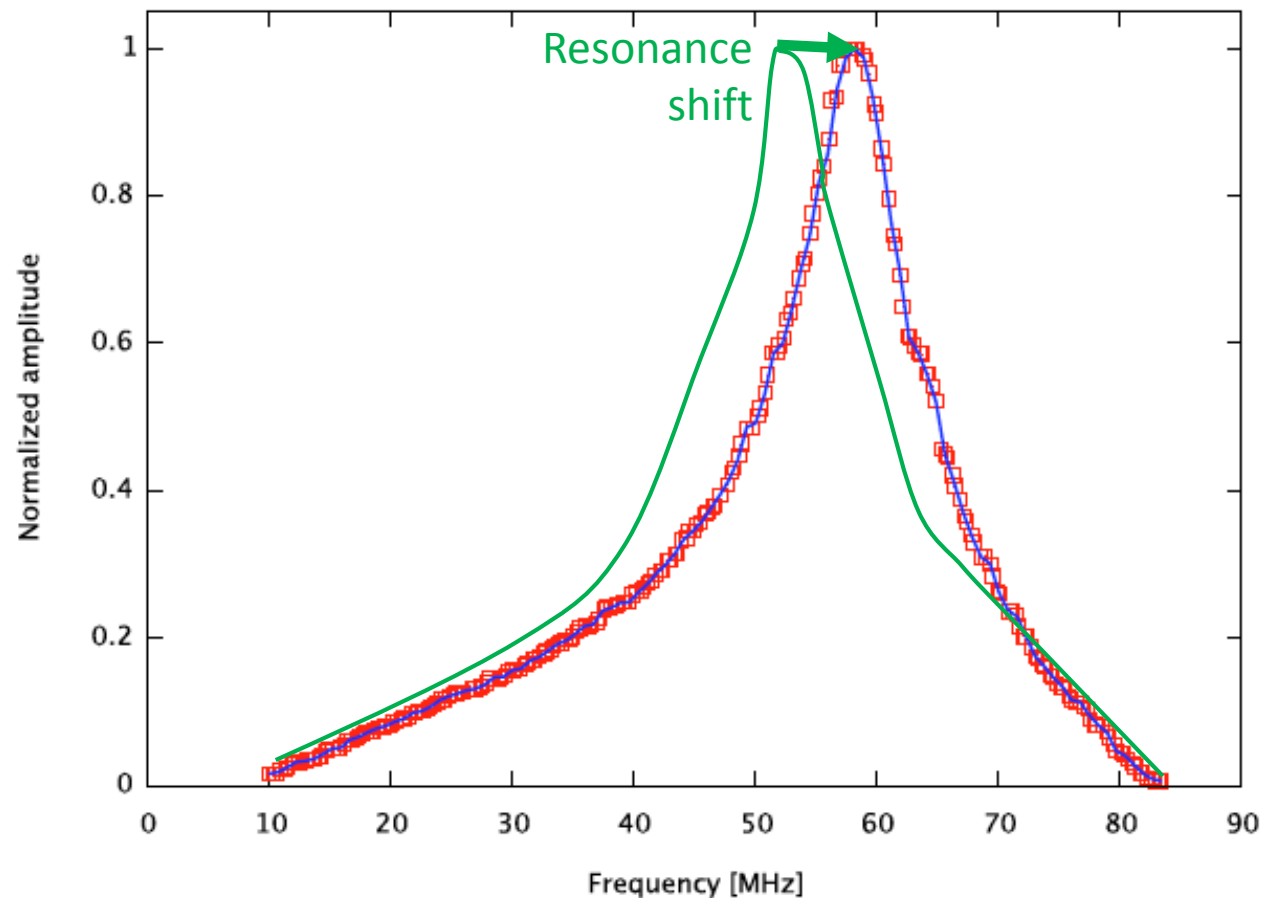


Mutual coupling in Lofar LBA & calibrating using characteristic basis functions

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Lofar LBA resonance shift



"Truth & Consequences" of finite LBA input impedance

- Is the LBA an *active* antenna?

- No. It's resonant antenna operating over a 10:1 band

- Does this only mean a *scalar* shift in the gain patterns?

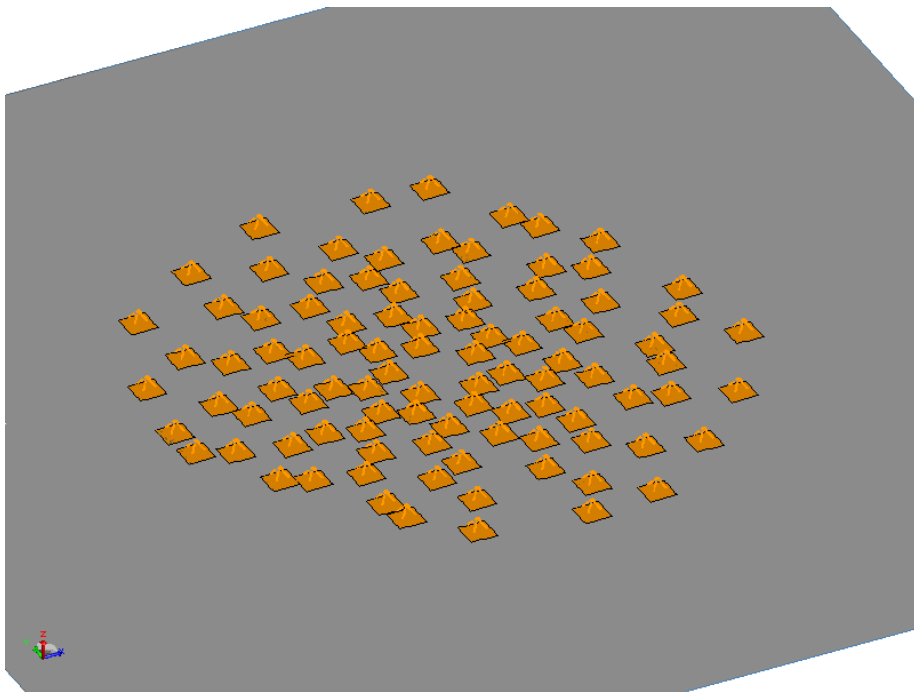
- No. Finite impedance (instead of open-circuit) means finite current on antenna => scattered radiation

- This leads to mutual-coupling

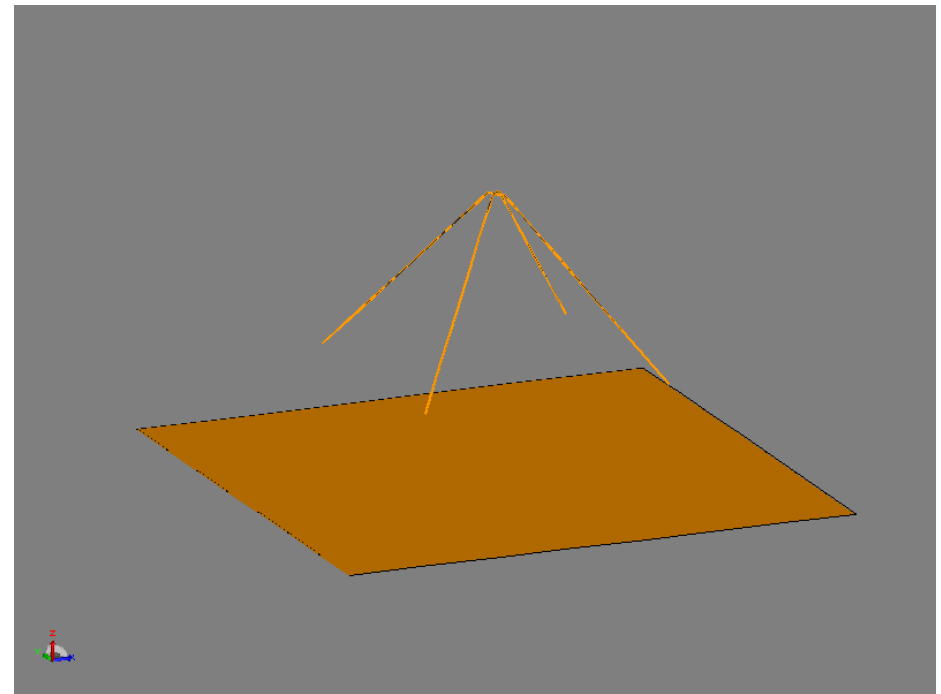
- Use EM simulation to confirm and quantify

International Lofar (SE-607) LBA

Array

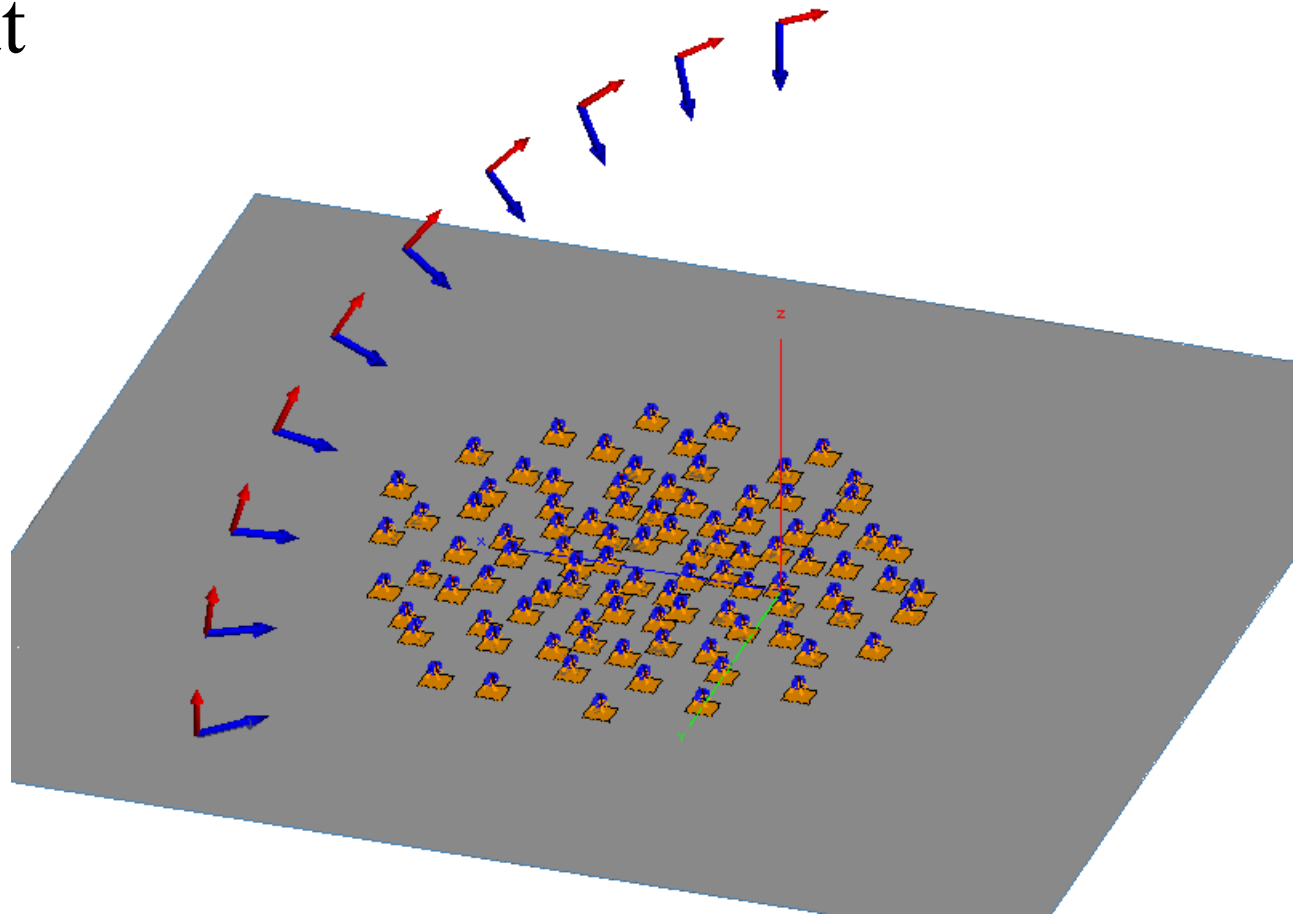


Element

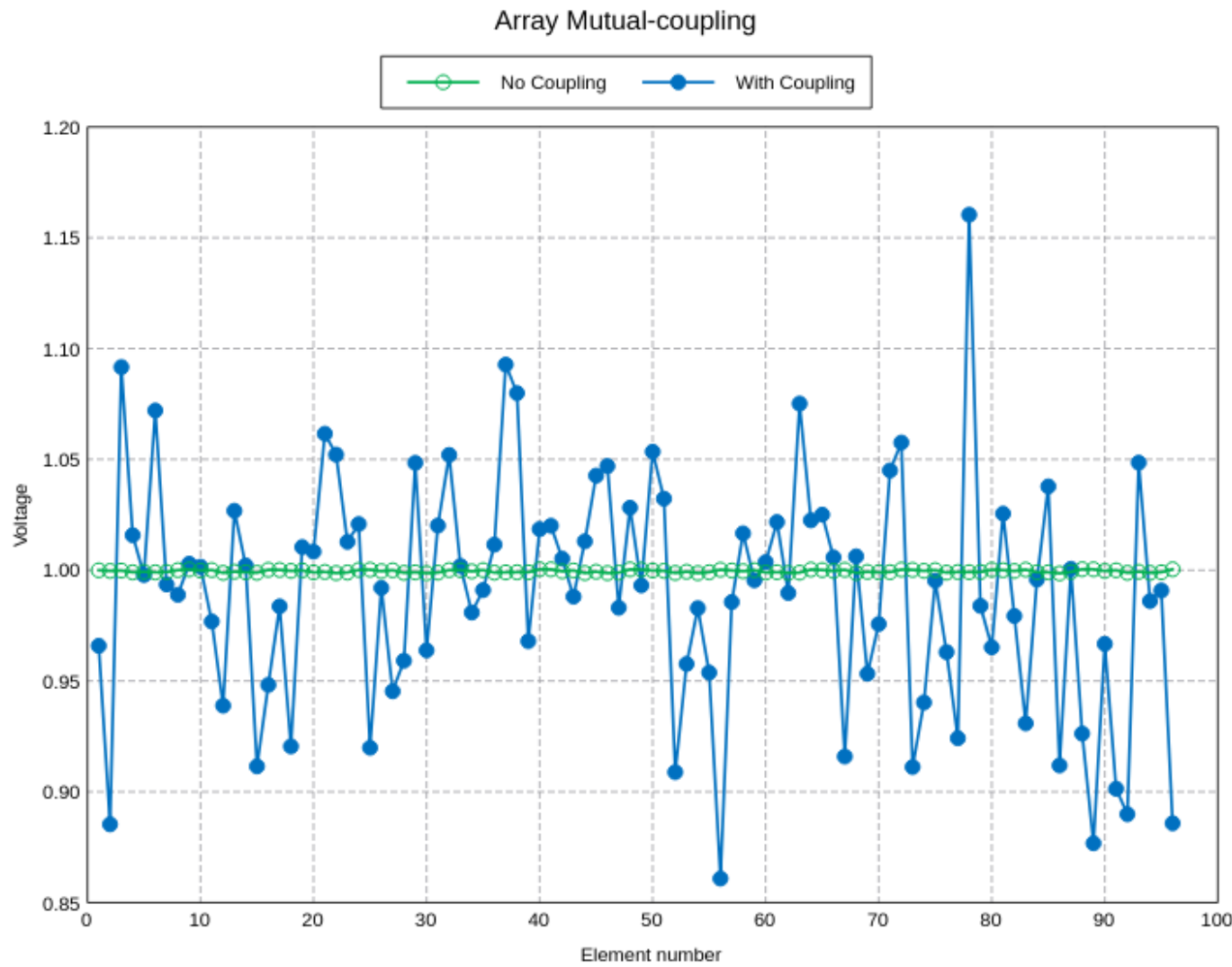


FEKO simulations

- Include finite input impedance LNA
- Run in receiver mode
 - Launch plane waves with given polarization
- Measure voltages on each LNA



Sim Results



Voltage Magnitude (Frequency = 55 MHz; Plane Wave Theta = 0 deg; Plane Wave Phi = 45 deg)

Coupling
induces 10%
deviation from
uncoupled
voltage

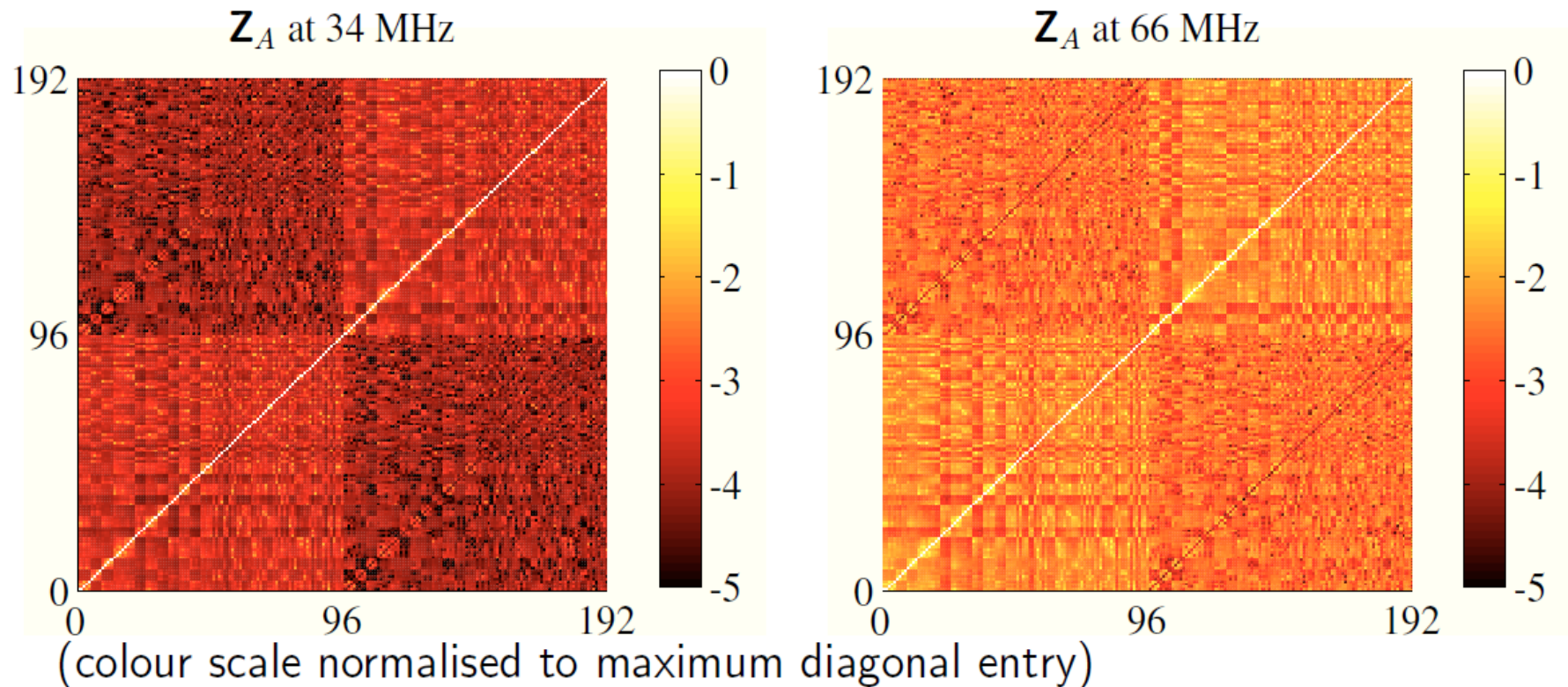
Lofar CBF

André Young

Full-wave simulation of LOFAR LBA in FEKO

Array impedance matrix

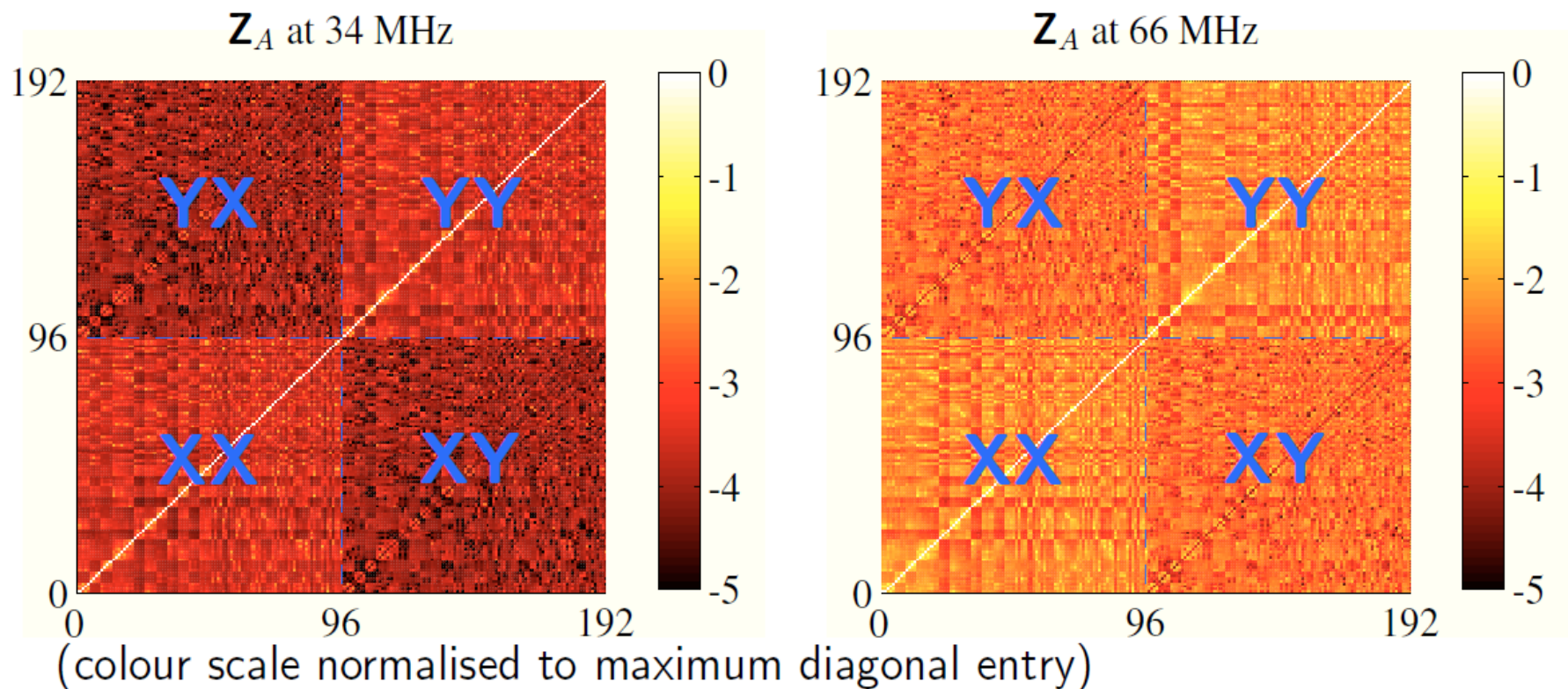
- ▶ mutual impedances generally higher at higher end of band



Full-wave simulation of LOFAR LBA in FEKO

Array impedance matrix

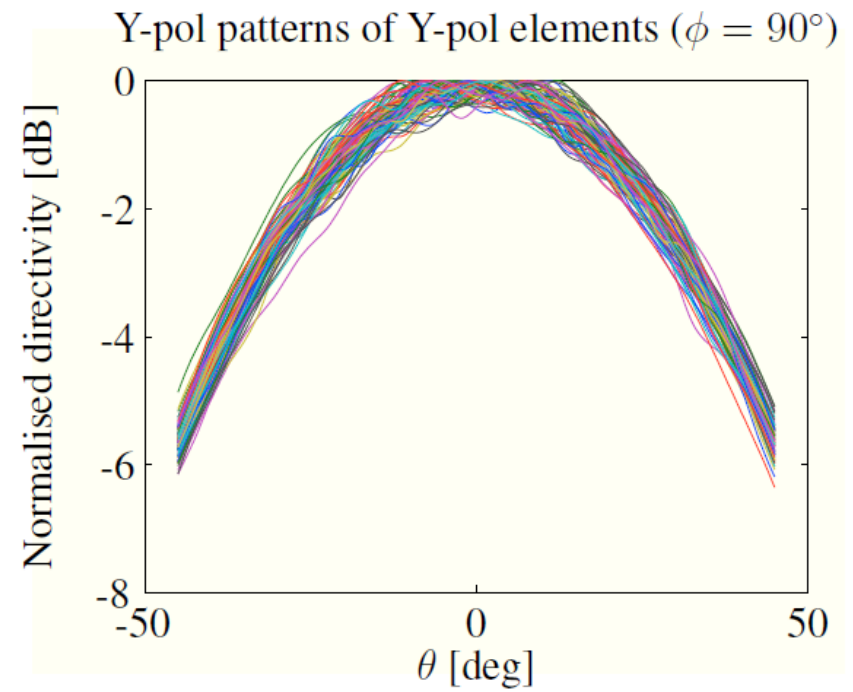
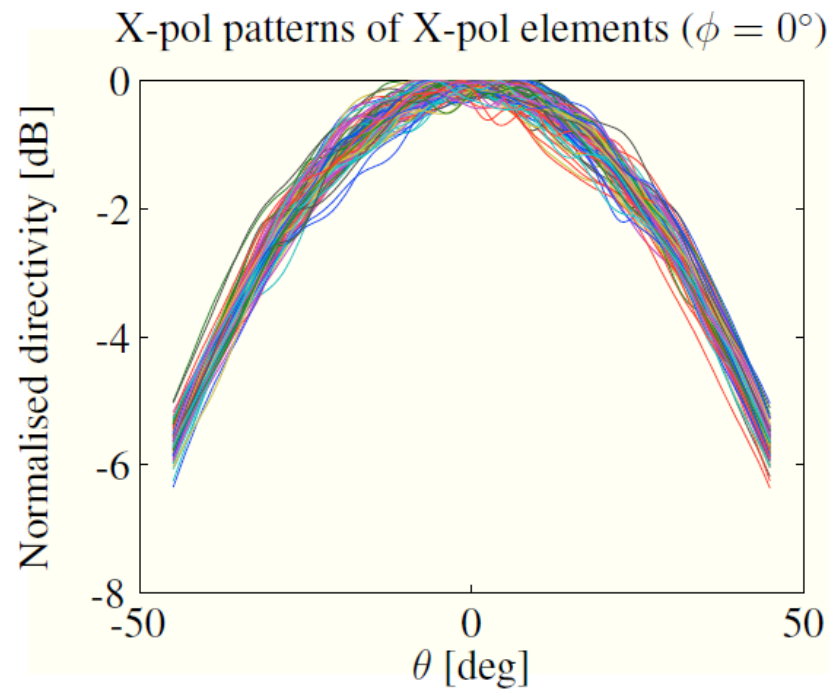
- ▶ mutual impedances generally higher at higher end of band



Full-wave simulation of LOFAR LBA in FEKO

Open-circuit voltage patterns

- ▶ result of mutual coupling clearly visible in variation among element patterns (65 MHz)



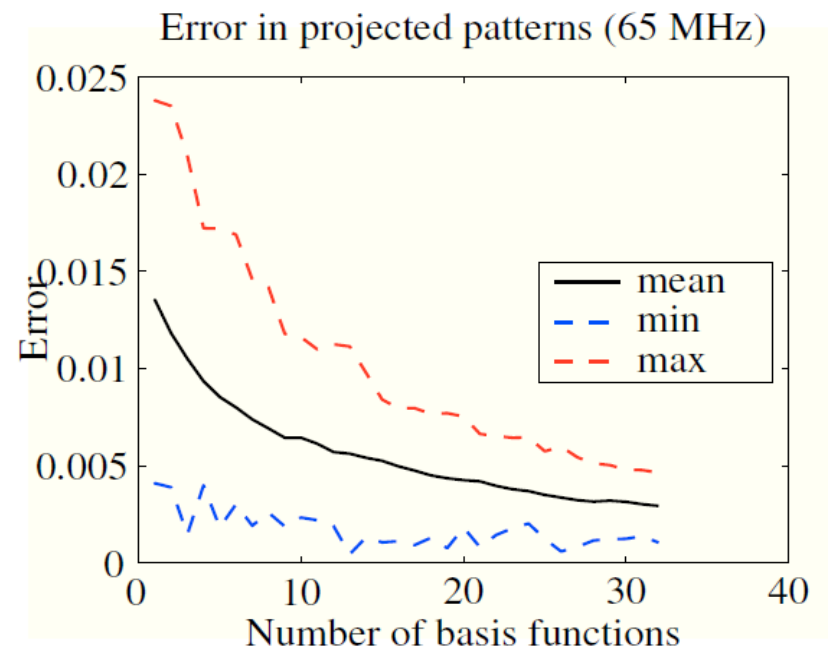
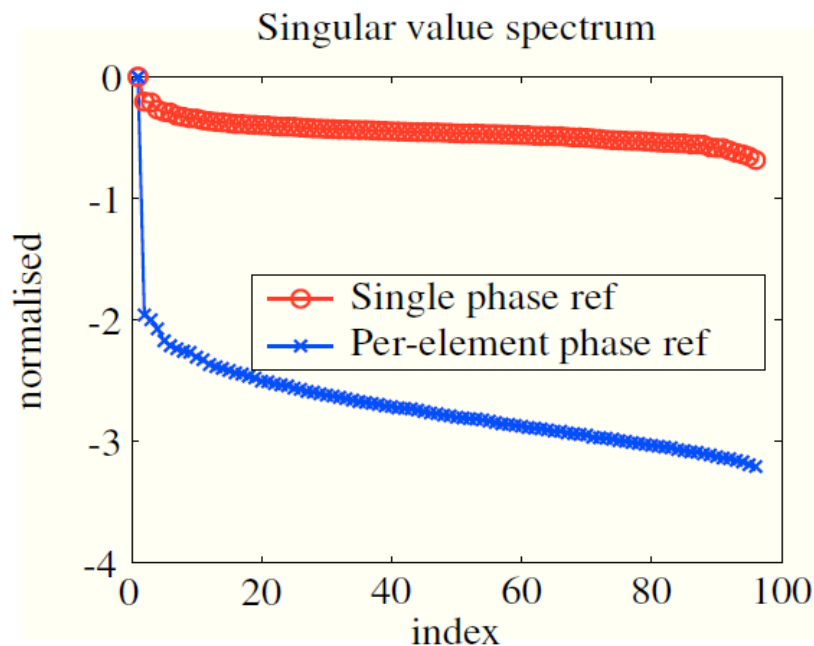
Low-order model for patterns?

Use SVD to extract dominant modes in all element patterns

$$\mathbf{F}_x^T = [\mathbf{f}_x(\Omega_1) \quad \mathbf{f}_x(\Omega_2) \quad \cdots \quad \mathbf{f}_x(\Omega_N)]^T, \quad \mathbf{U}\mathbf{\Sigma}\mathbf{V}^H = \mathbf{F}_x^T$$

Project element pattern $\mathbf{p}_{i,x} = [\mathbf{f}_x]_i \left(\{\Omega\}_{n=1}^N \right)$ onto $\text{span} \{\mathbf{u}_k\}_{k=1}^{N_B}$

$$\hat{\mathbf{p}}_{i,x} = \mathbf{U}_{N_B} (\mathbf{U}_{N_B}^H \mathbf{U}_{N_B})^{-1} \mathbf{U}_{N_B}^H \mathbf{p}_{i,x}, \quad \text{Error} = \|\hat{\mathbf{p}}_{i,x} - \mathbf{p}_{i,x}\| / \|\mathbf{p}_{i,x}\|$$



(per-element phase ref)

Compensating for Gain / Impedance Variation

Known conditions \rightarrow simulate; **unknown** conditions \rightarrow model

Open-circuit voltages at antenna terminals for incident field

$$\mathbf{v}_{\text{oc}} = \sum_{j=1}^{N_j} e_{x,j} \mathbf{f}_x(\Omega_j) + e_{y,j} \mathbf{f}_y(\Omega_j) = \mathbf{F}_x \mathbf{e}_x + \mathbf{F}_y \mathbf{e}_y$$

Voltages appearing across load network

$$\mathbf{v} = \mathbf{Q} \mathbf{v}_{\text{oc}}, \quad \mathbf{Q} = \mathbf{G} \mathbf{Z}_L (\mathbf{Z}_L + \mathbf{Z}_A)^{-1}$$

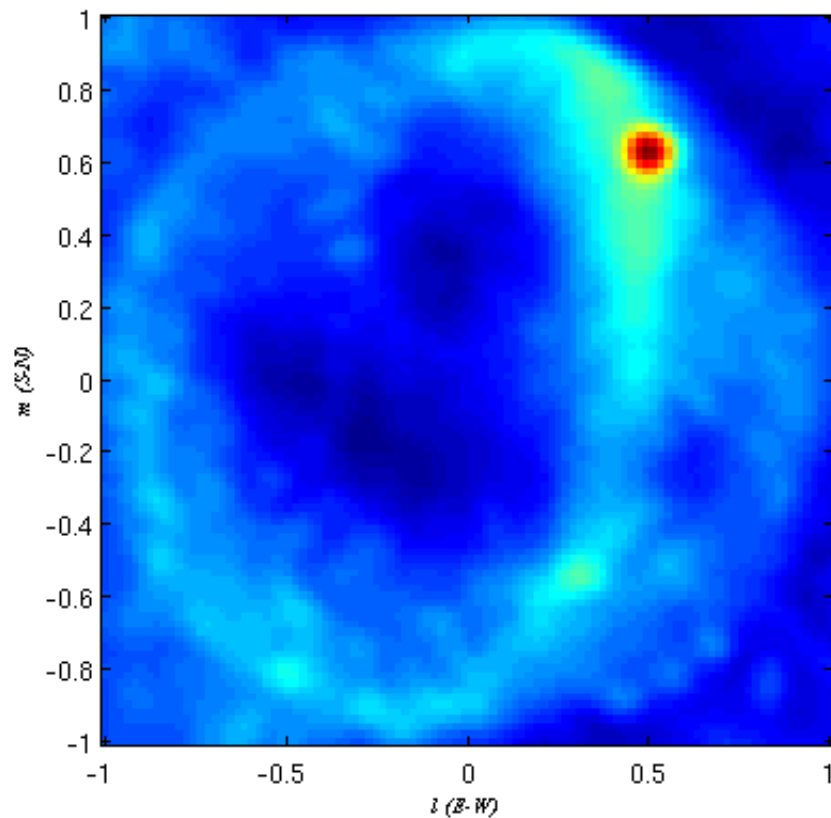
Correlation matrix for entire array

$$\mathbf{R}_v = \mathbf{P} \mathbf{B} \mathbf{P}^H, \quad \mathbf{P} = \mathbf{Q} \mathbf{F}, \quad \mathbf{F} = [\mathbf{F}_x \quad \mathbf{F}_y], \quad \mathbf{B} = \mathbb{E} \left\{ \begin{bmatrix} \mathbf{e}_x \mathbf{e}_x^H & \mathbf{e}_x \mathbf{e}_y^H \\ \mathbf{e}_y \mathbf{e}_x^H & \mathbf{e}_y \mathbf{e}_y^H \end{bmatrix} \right\}$$

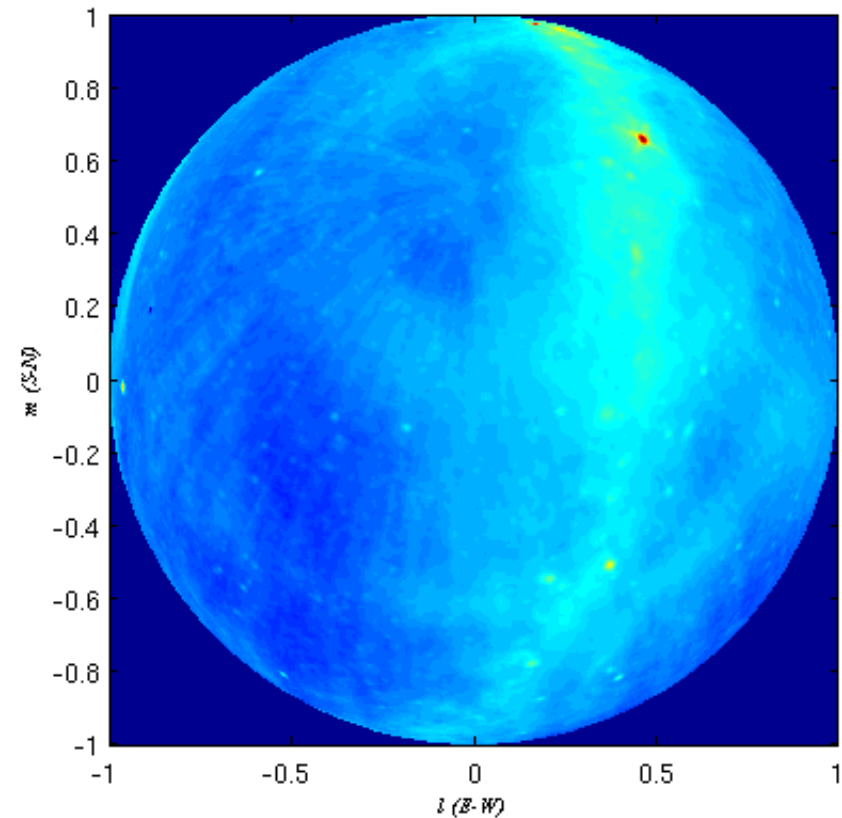
Construct basis for \mathbf{P} based on expected variations in \mathbf{G} and \mathbf{Z}_L

Calibration & Imaging

Lofar SE607 LBA @ 49.9 MHz 20131219T003017Z



Model sky over SE607 @ 50 MHz 20131219T003017Z



Conclusion

- Lofar LBA has mutual-coupling
- Characteristic basis functions may be a useful tool for calibration

Thanks

