

SKA-low array

Eloy de Lera Acedo

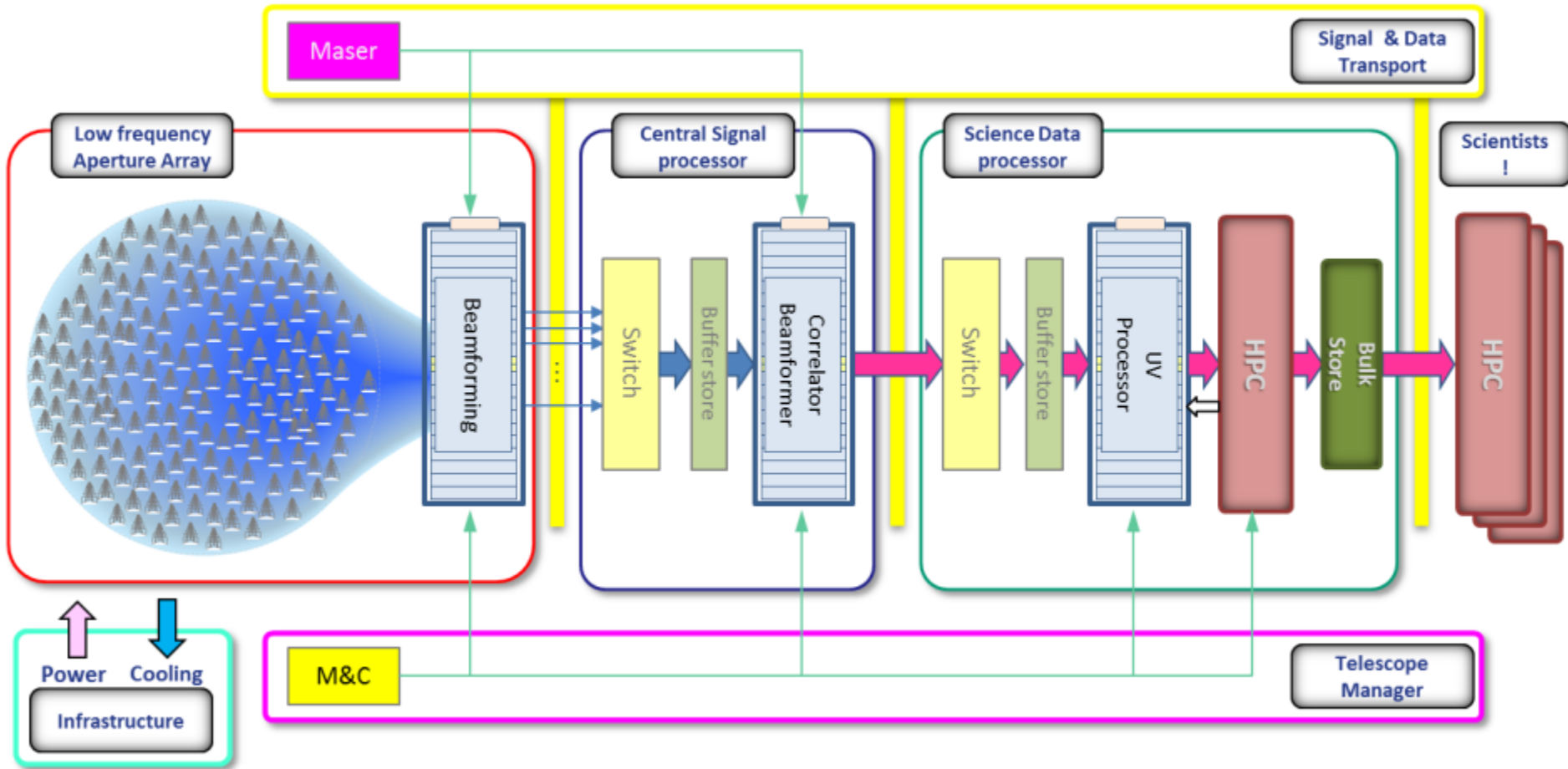
Cambridge University

Overview

- The SKA-low array system
- SKA-low front-end technology development
- Simulations and calibration for SKA-low
- Future work and conclusions

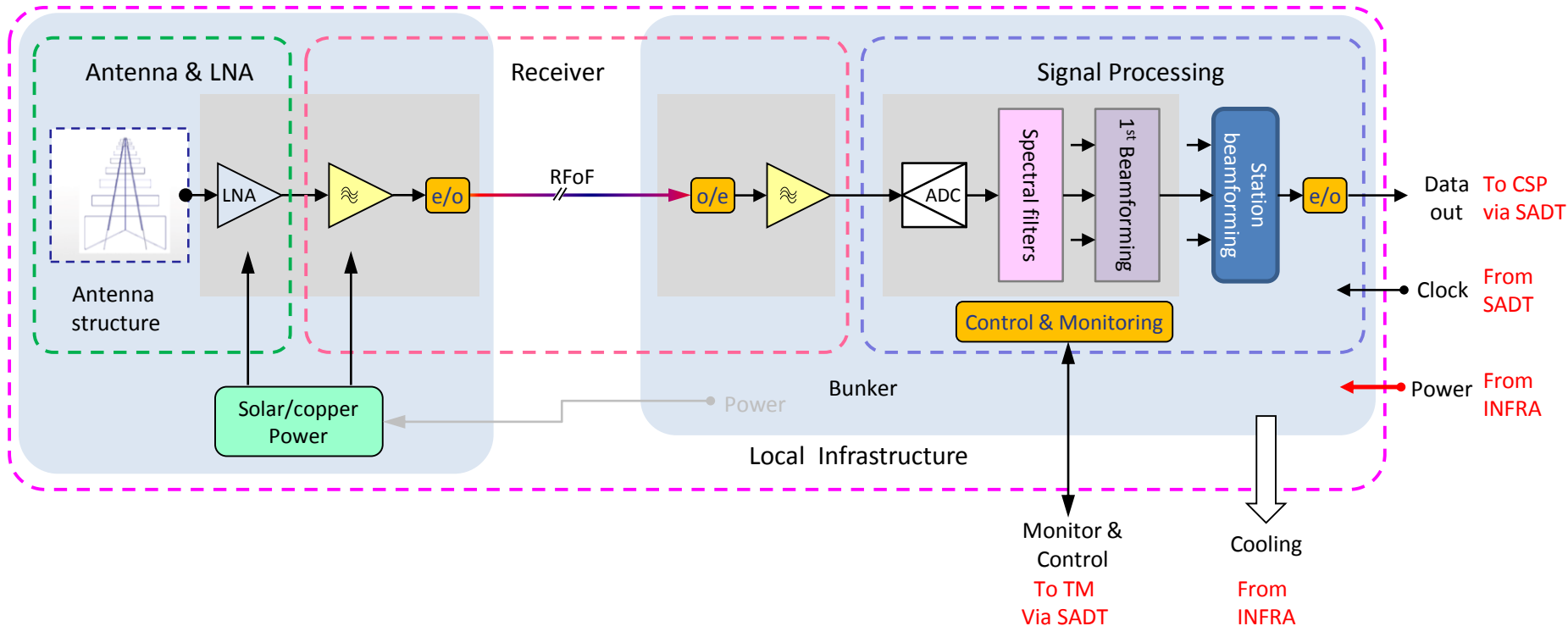
The SKA-low array system

SKA-low end-to-end system architecture



A central bunker will integrate the LFAA beamforming/correlation, signal transport, Maser clock and local monitoring and control

LFAA signal flow



LFAA consortium

- ✓ Project Leader: Jan Geralt bij de Vaate (ASTRON)
- ✓ Project Engineer: Andy Faulkner (Cambridge)
- ✓ Project Scientist: Carol Jackson (ICRAR)
- ✓ Project manager: Andre van Es (ASTRON)

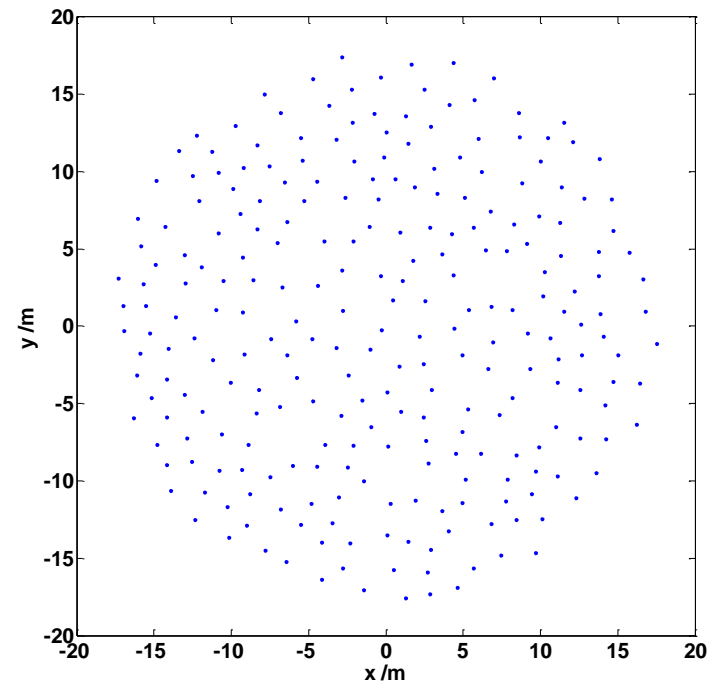
Work Packages:

- Engineering management (Jan Geralt bij de Vaate - ASTRON)
- System Engineering (Andy Faulkner - UCam)
- Antenna and low noise amplifier (Eloy de Lera Acedo - UCam)
- Receiver (Jader Monari – INAF)
- Signal Processing (Kris Zarb Adami – Oxford)
- Array Prototypes (Adrian Sutinjo – ICRAR)
- Local Infrastructure (Tom Booler – ICRAR)
- Local Monitoring and Control (Pieter Benthem - ASTRON)

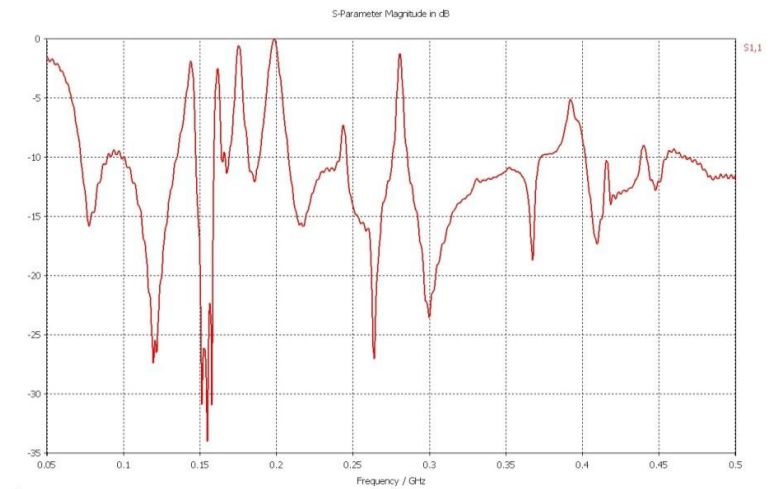
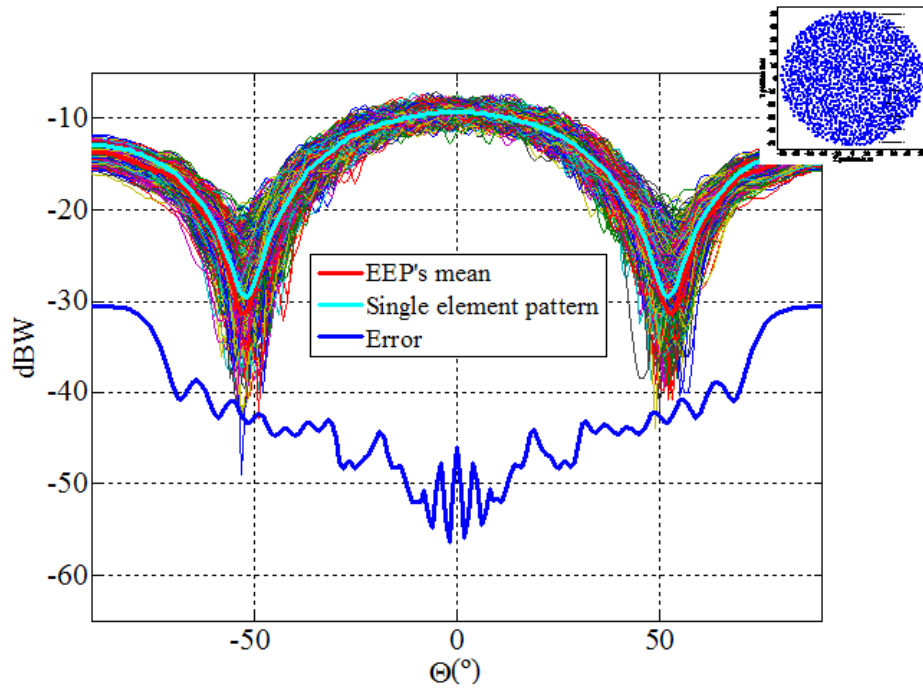
| Component | Includes | Budget cost for SKA1 (each antenna sub-system) |
|---------------------------------|---|---|
| Antenna Mechanical components | Radiating arms, Support structure including base, Electronics housing, Ground plane (if required), Mechanical shielding, Fixings | €60 |
| Signal Chain Electronic systems | Low noise amplifier, Matching components, Amplifiers and filters, Laser driver , Laser control, Local power regulation, Connectors, Circuit boards, Shielding mounted on board | €40 |
| Solar power unit | Solar cells, Control electronics, Battery/super-capacitor, Enclosure and fixings, Cable connections and connectors | €50 |
| Deployment | Antenna sub-system assembly, Transport from site receiving area to antenna placement site, Deployment at site including final assembly, Accurate positioning and alignment, Connection to fibre links, Local installation test and identification | €30 |
| Totals | | €180 |

| Week | Date | Event | Comments |
|--------|---------------|--|--|
| T0 | 1 Nov. 2013 | Official start of the consortium work. Also, the initial release of the "Level 1" requirements for the SKA1. | |
| T0+12 | 1 March 2014 | Release of detailed "Level 1" requirements | |
| T0+34 | 1 July 2014 | Preliminary installation plan (including demonstration plan). | This needs to show how the antenna sub-systems will be installed and how long it takes |
| T0+46 | 14 Sept. 2014 | System Requirements Review (documents only) | Internal draft documentation that gets submitted to SKAO |
| T0+50 | Oct. 2014 | Preliminary Design Review | Documents and presentation on way forward |
| T0+72 | 1 April 2015 | AAVS1 Detailed design Review | Decide on what actually gets built for the major demonstrator |
| T0+85 | 1 July 2015 | Completed installation plan including demonstration | Need to show that the deployment of LFAA can be done as stated |
| T0+112 | 31 Dec. 2015 | Installation and commissioning of AAVS1 completed | This should be a complete and working array |
| T0+140 | 1 July 2016 | Submit test and evaluation report for AAVS1 | |
| T0+148 | 1 Sept. 2016 | Critical Design Review for LFAA, including submission of manufacturing documentation | The final big review |
| T0+156 | 1 Nov. 2016 | Closure of Pre-construction Phase | End of project |

Introduction

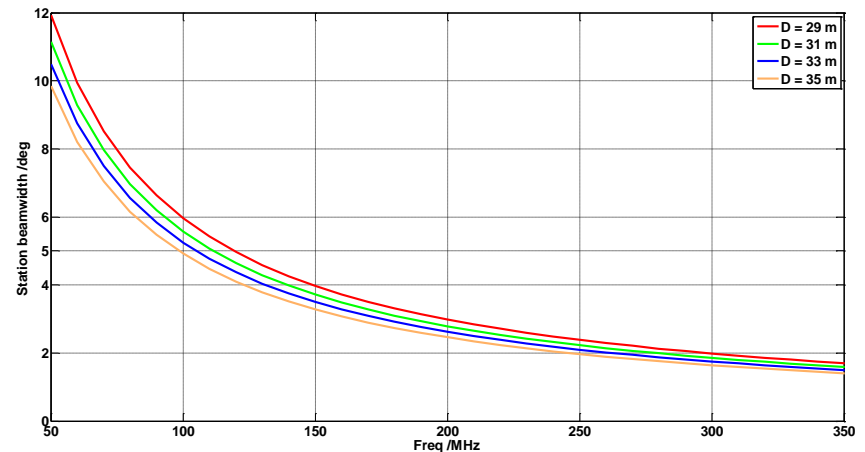


Introduction



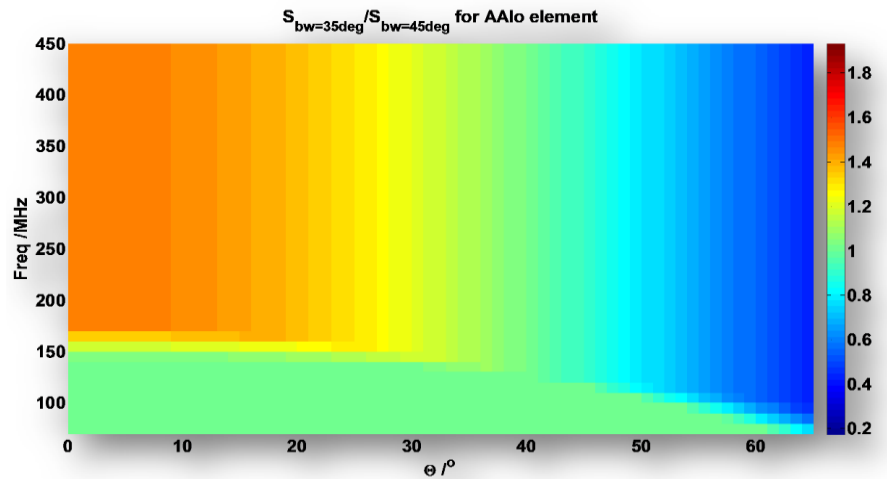
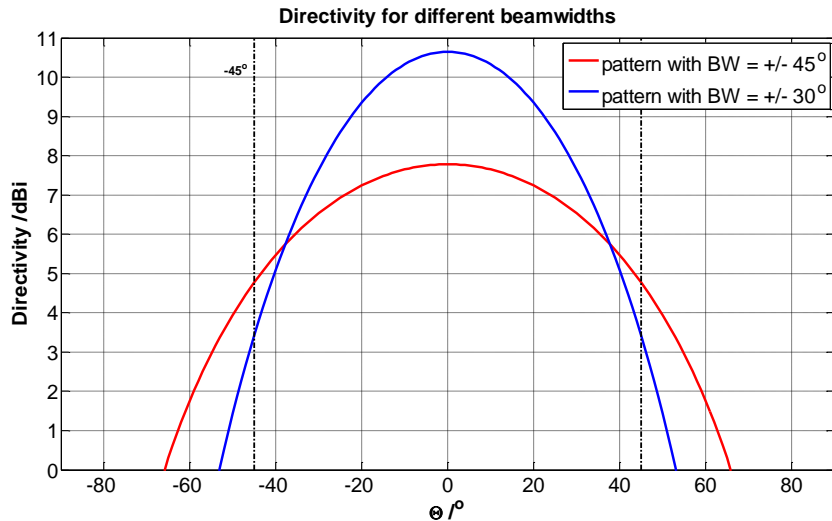
Introduction

- 2^{18} antennas
- $D_{\text{station}} = 35$ m
- 256 antennas/station
- $D_{\text{average}} = 1.93$ m

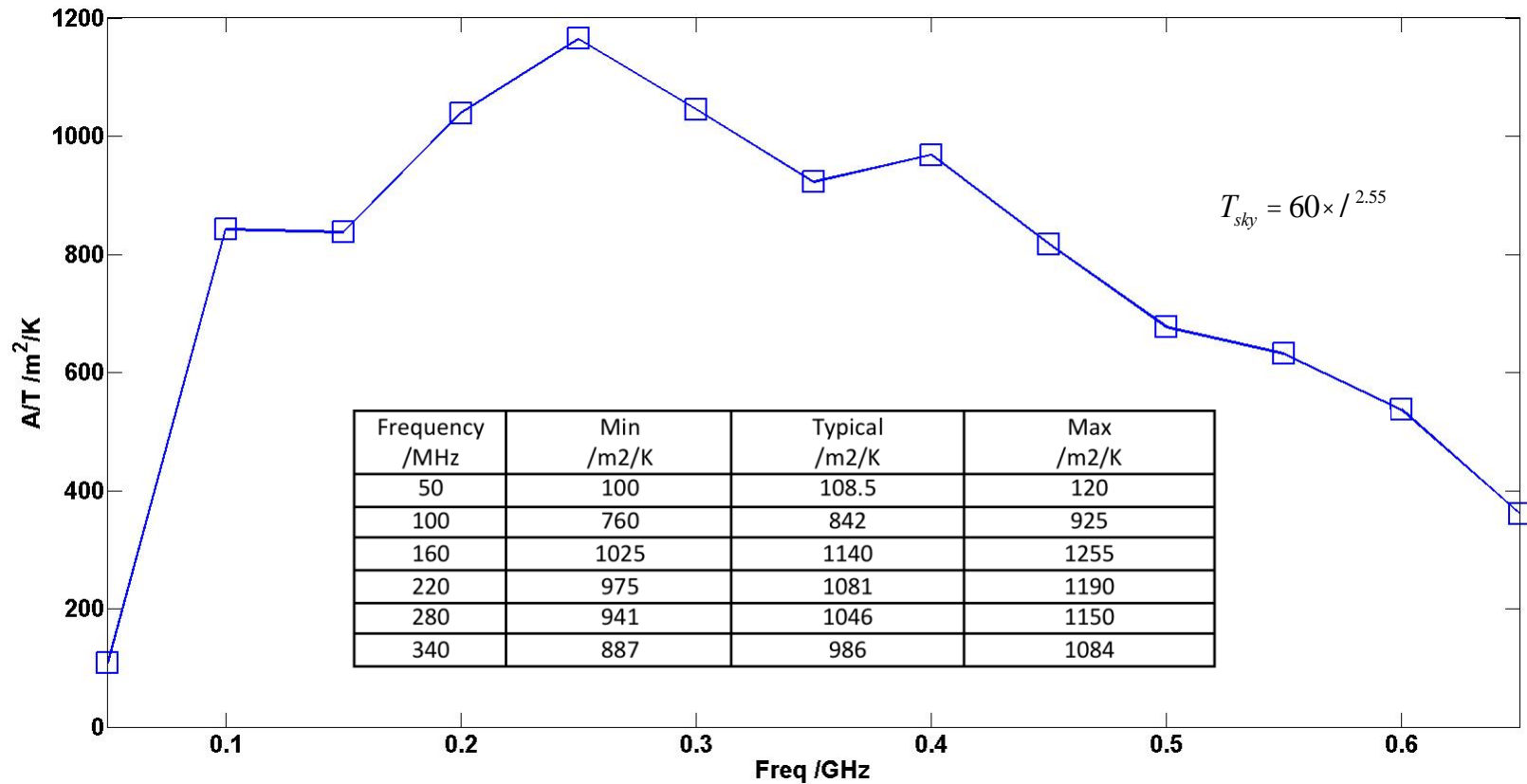


LFAA Sensitivity

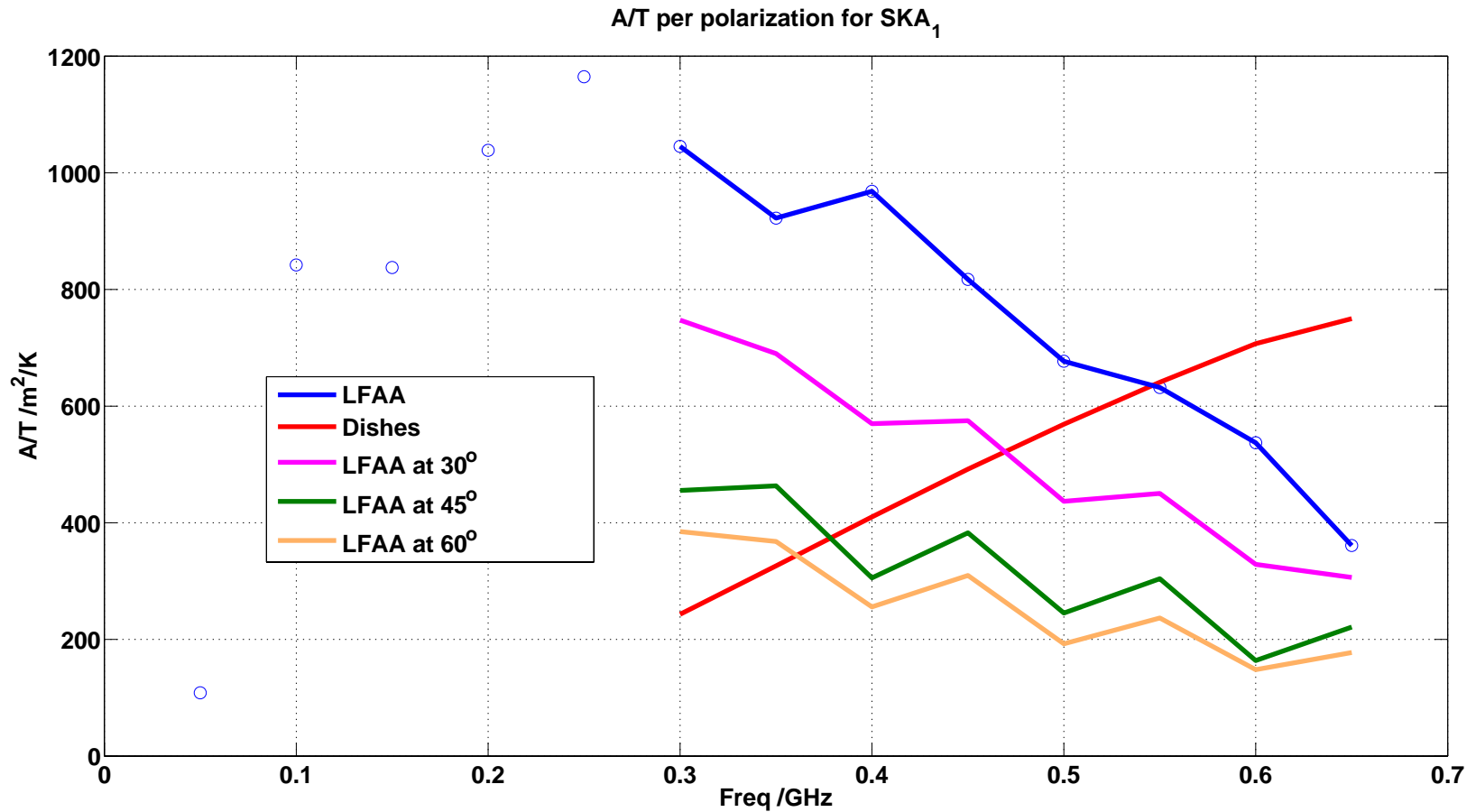
$$\left. \frac{A_{\text{eff}}}{T_{\text{sys}}} \right|_{q,j} = \frac{l^2 / 4\rho \times G_{q,j}}{h_{\text{rad}} \times T_A + (1 - h_{\text{rad}}) \times T_0 + T_{\text{rec}} / (1 - |G|^2)}$$



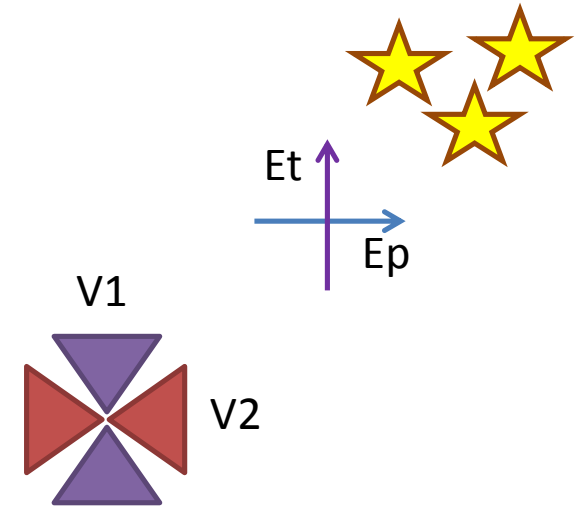
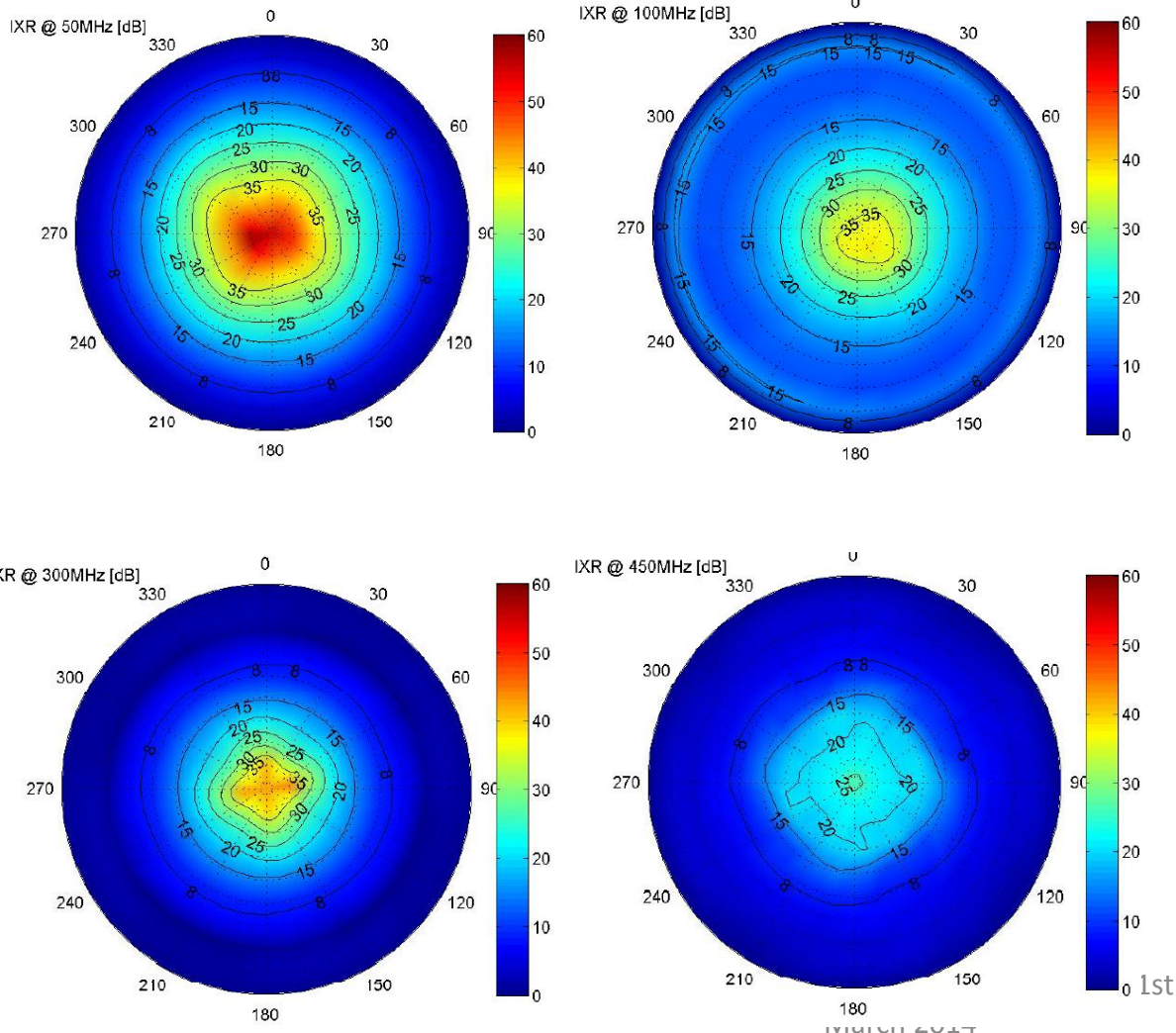
LFAA Sensitivity



LFAA Sensitivity (extended band)



LFAA polarization



$$IXR_J = \left(\frac{\kappa(J) + 1}{\kappa(J) - 1} \right)^2$$

➤ Credit: "IXR SKALA with GP vs Vivaldi V2 with Soil C", 08/10/2012 – B. Fiorelli).

SKA-low front-end technology development

SKALA: Design



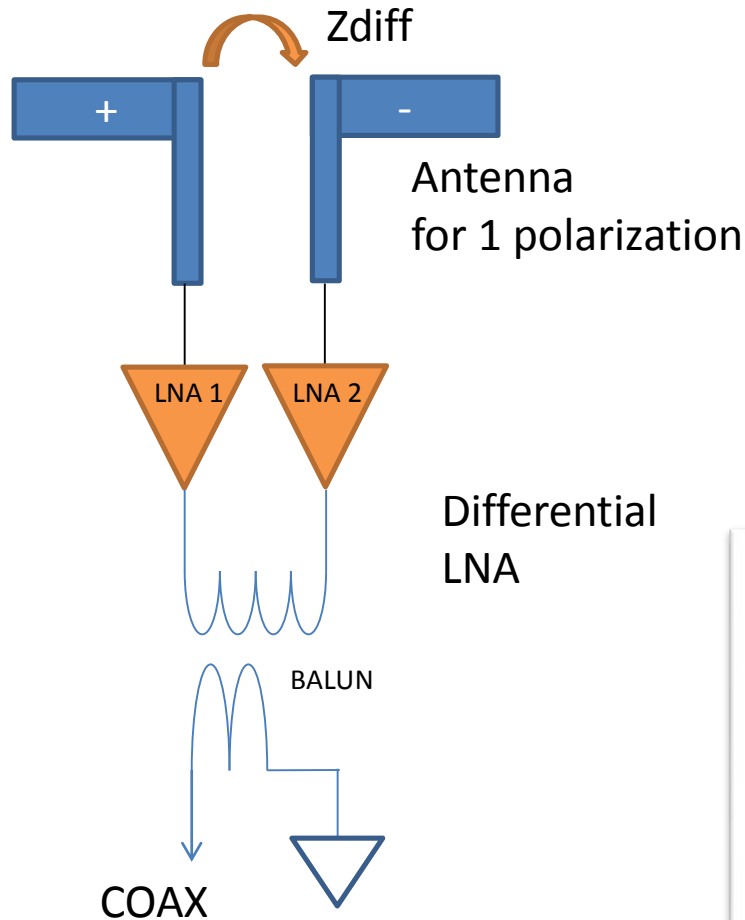
Antenna + LNA:
90€/element

- SKALA: SKA Log-periodic Antenna
 - Good Impedance
 - Pattern width controllable (7:1 band!)
 - Low back lobe at high frequencies
- Dual polarization
- 9 wide dipoles: top 2 are not resonant in band
- Maximizing A/T in the +/- 45 deg. Region

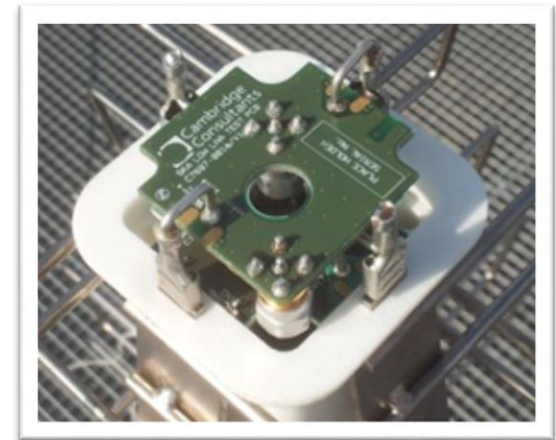
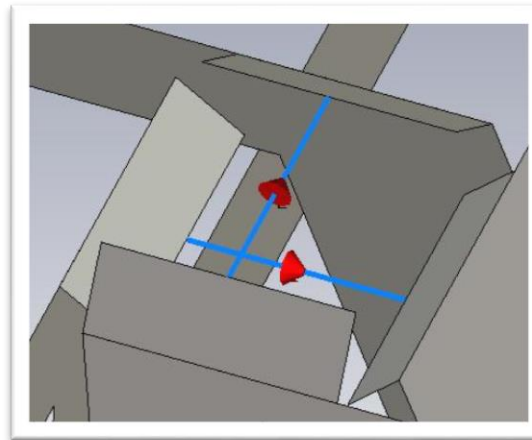
$$\left. \frac{A_{\text{eff}}}{T_{\text{sys}}} \right|_{\theta, \phi} = \frac{\lambda^2 / 4\pi \cdot G_{\theta, \phi}}{\eta_{\text{rad}} \cdot T_{\text{A}} + (1 - \eta_{\text{rad}}) \cdot T_0 + T_{\text{rec}}}$$

- Distance to ground plane
- Opening angle (trade off: A_{eff} and XP): 10°
- Antenna size/footprint
- Growing factor

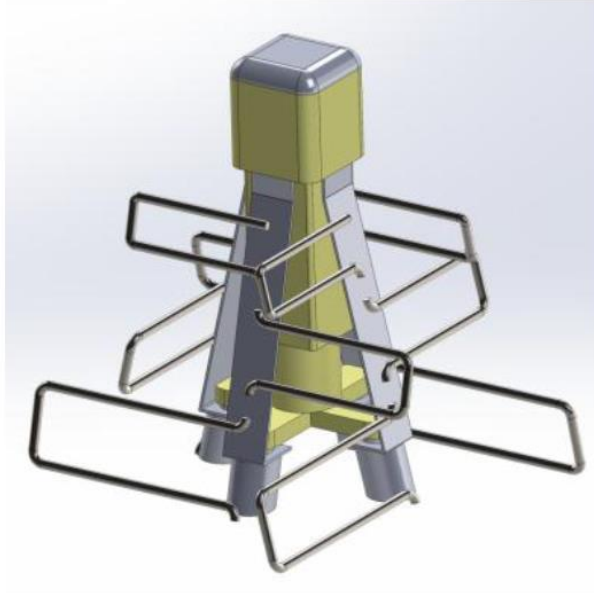
SKALA: Design



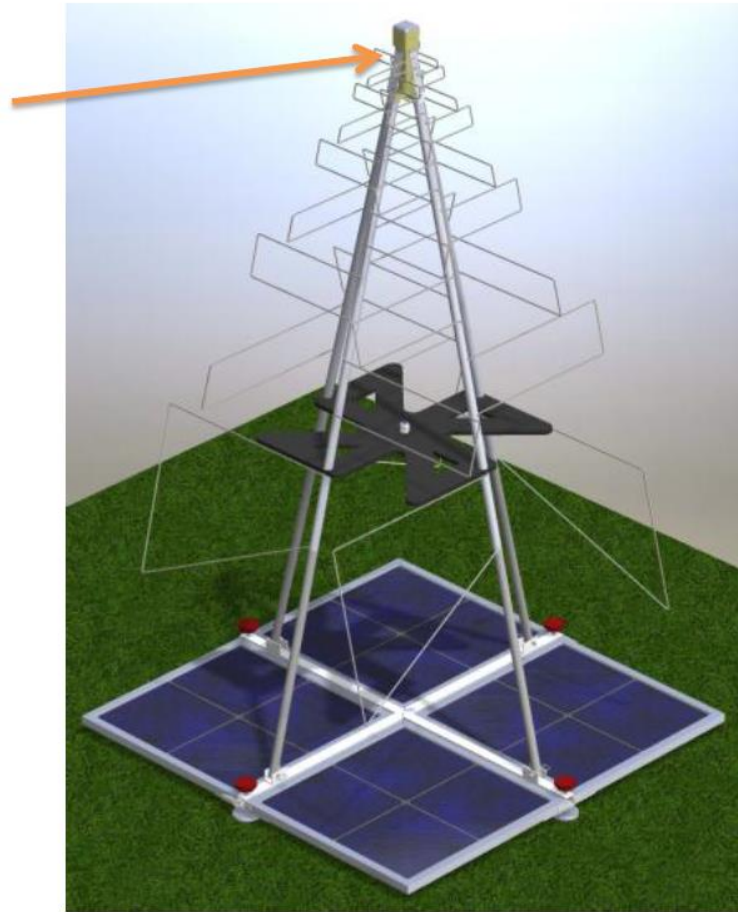
- Ideally; differentially fed for lowest noise.
- Feeding at the top for practical reasons:
 - Avoid Damage in case of flooding
 - LNA and electronics (RFoF, etc.) could be integrated at the top of the antenna.



SKALA-2

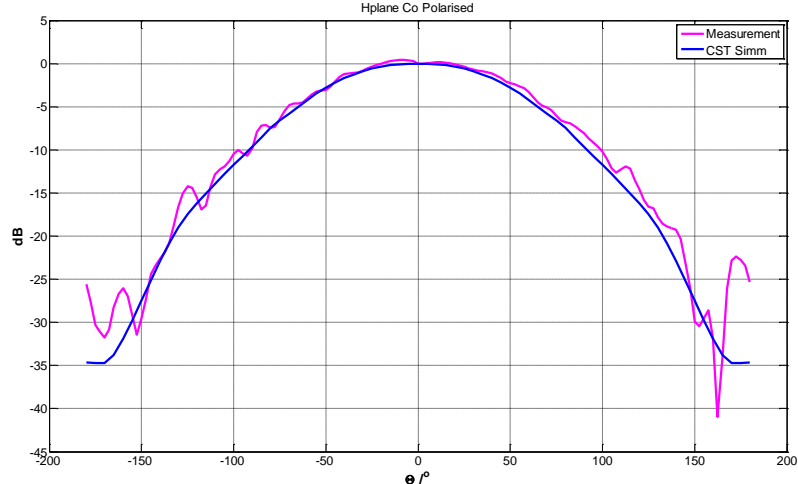
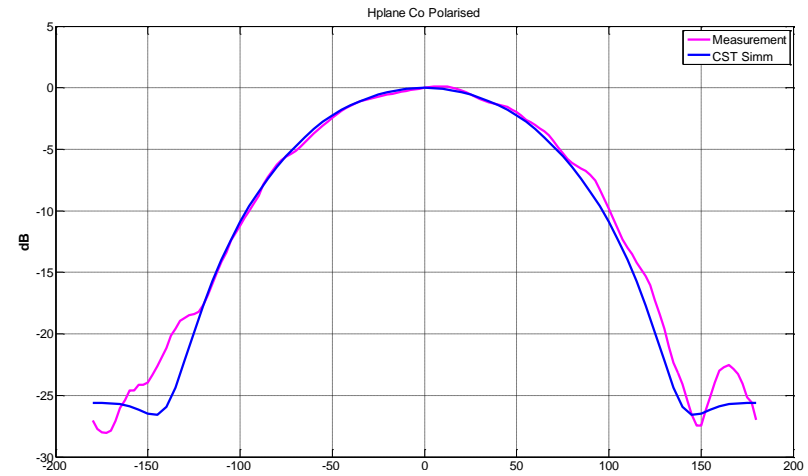
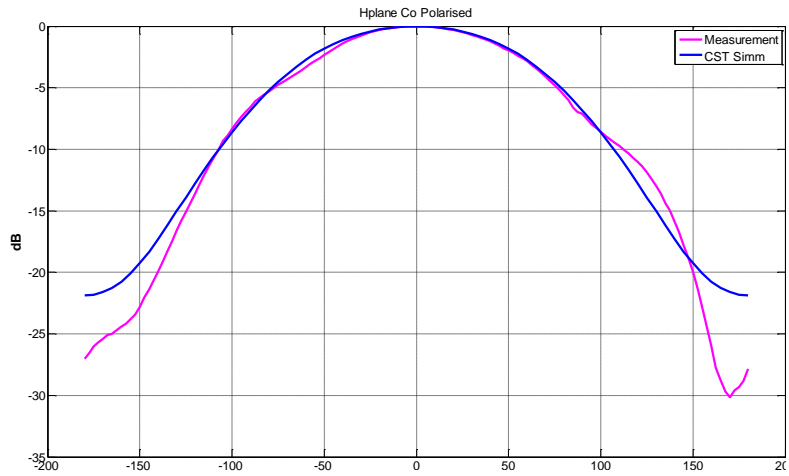


Credit: MIT



Measurements: Pattern

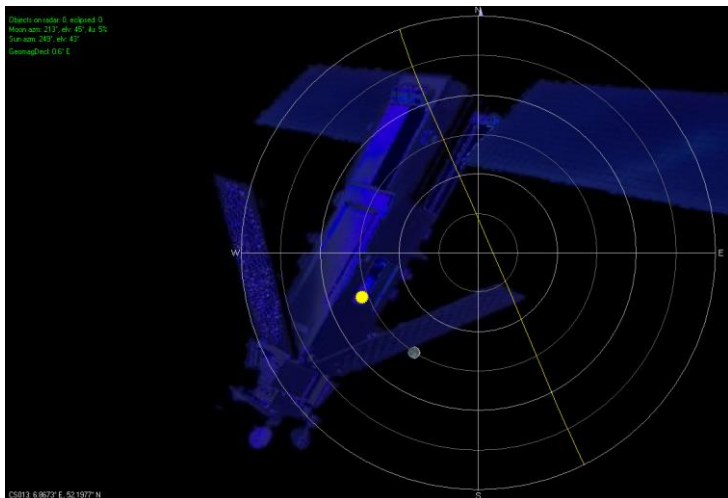
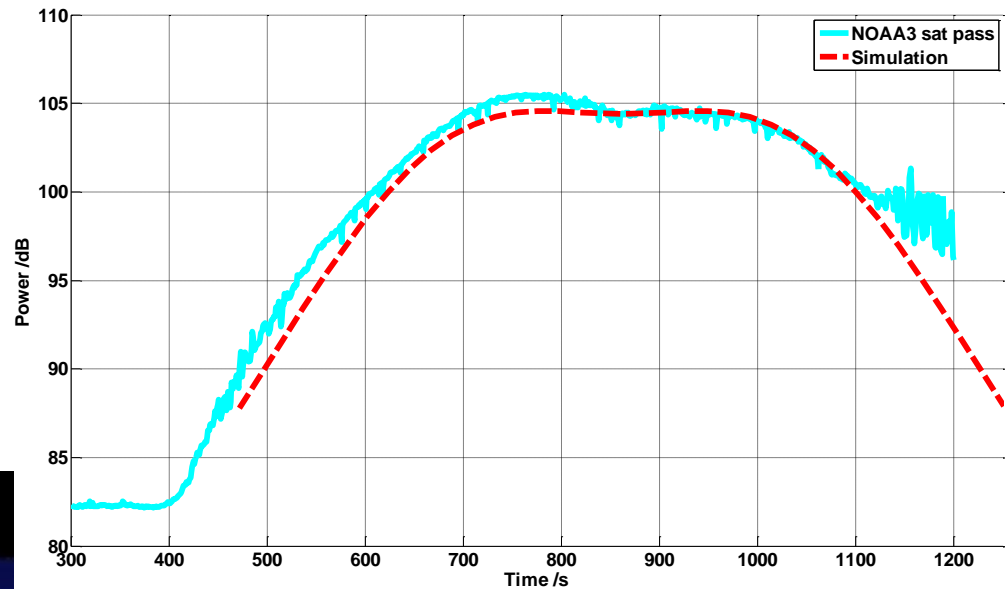
150 MHz 300 MHz
450 MHz



Measurements: Pattern (with LOFAR)



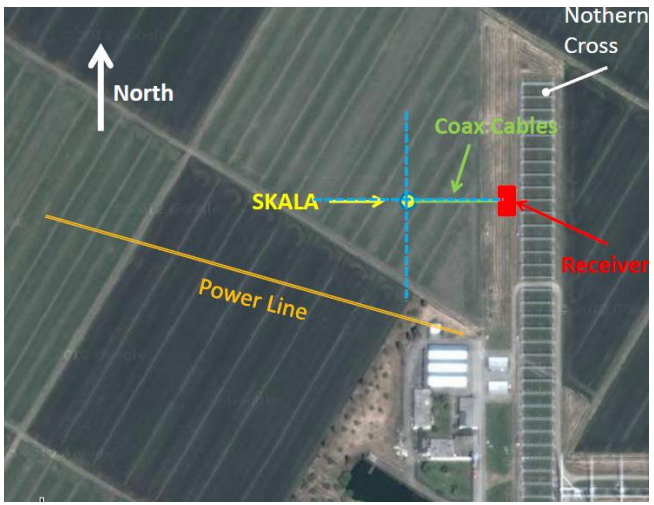
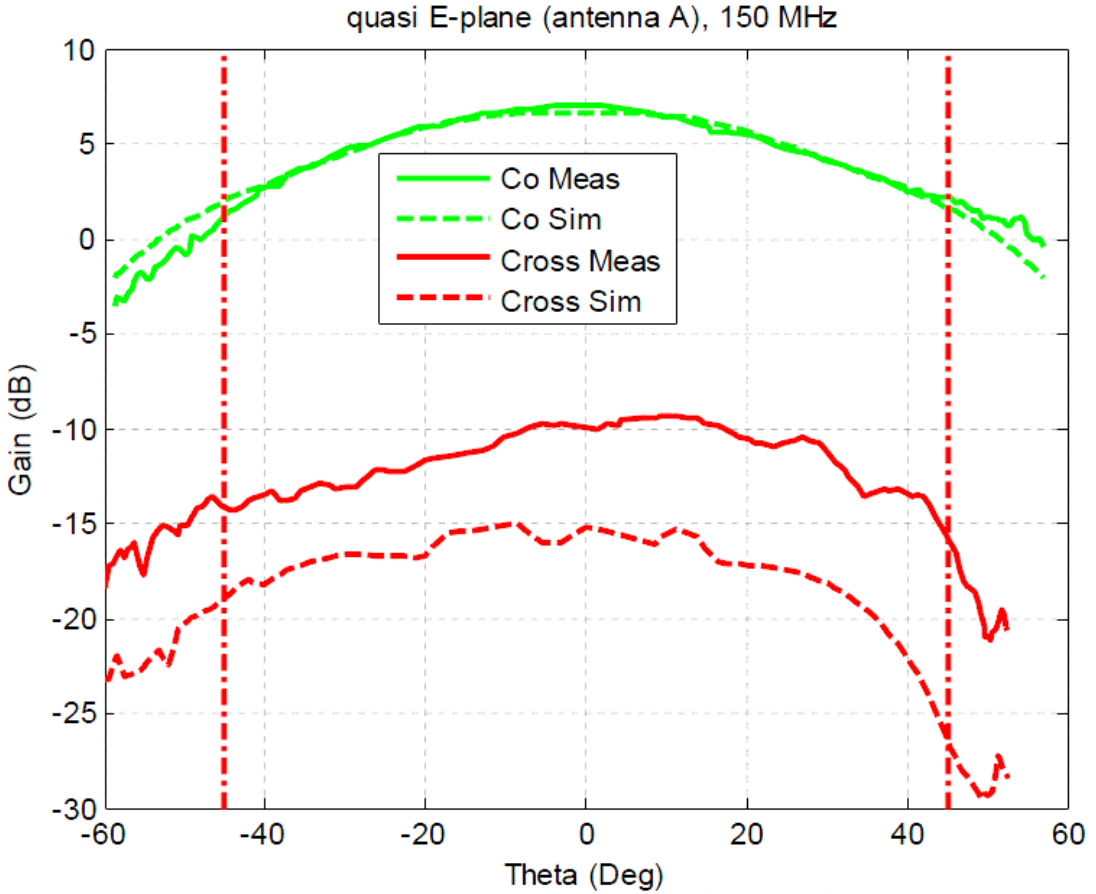
NOAA 3 sat: 137 MHz



- Also: Beam forming with LOFAR HBA, cross-correlation, LNA stability over large periods of time, etc.

- Next: Correlation of LOFAR with SKALA array?

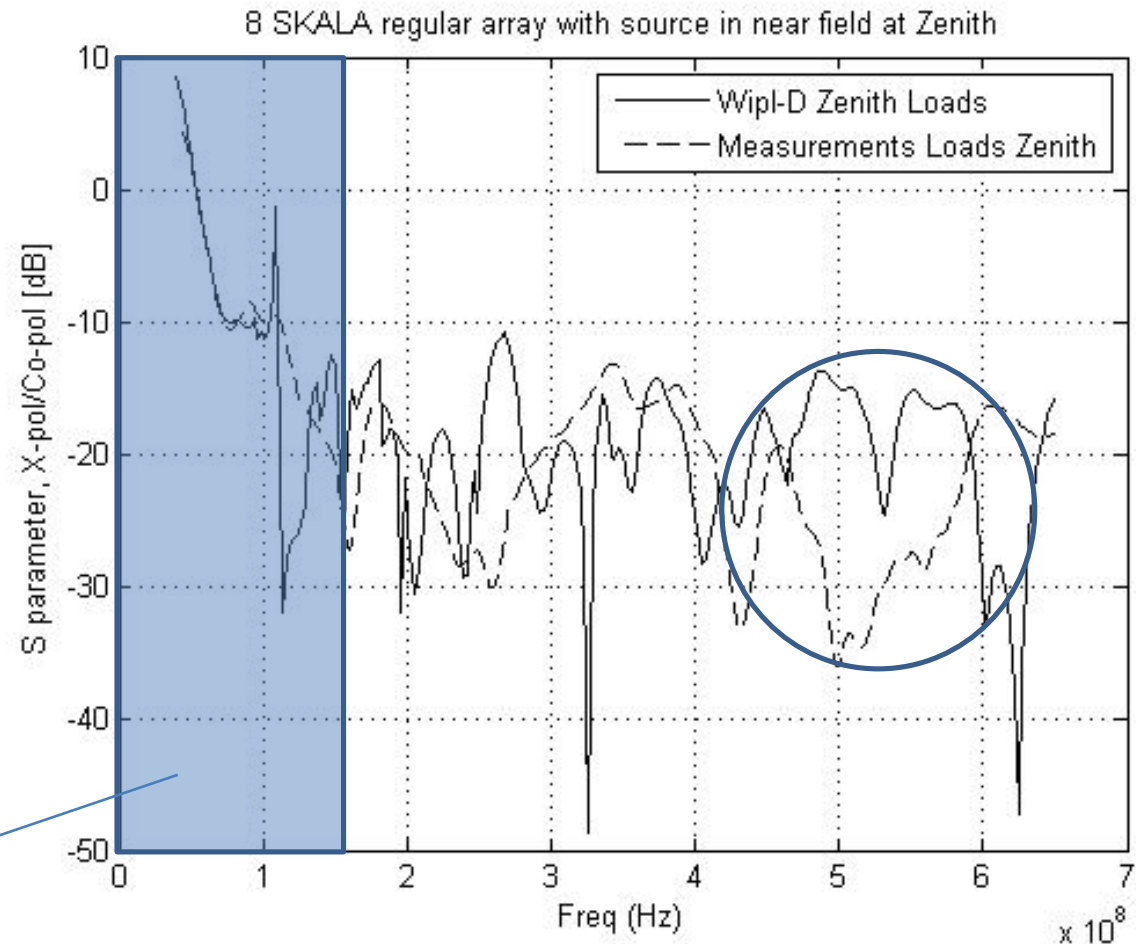
Measurements: Pattern (with Hexacopter - INAF)



Measurements: Near field patterns / Cross-polarization / IXR



Next step: Try with Celestial Sources (MWA, LOFAR).



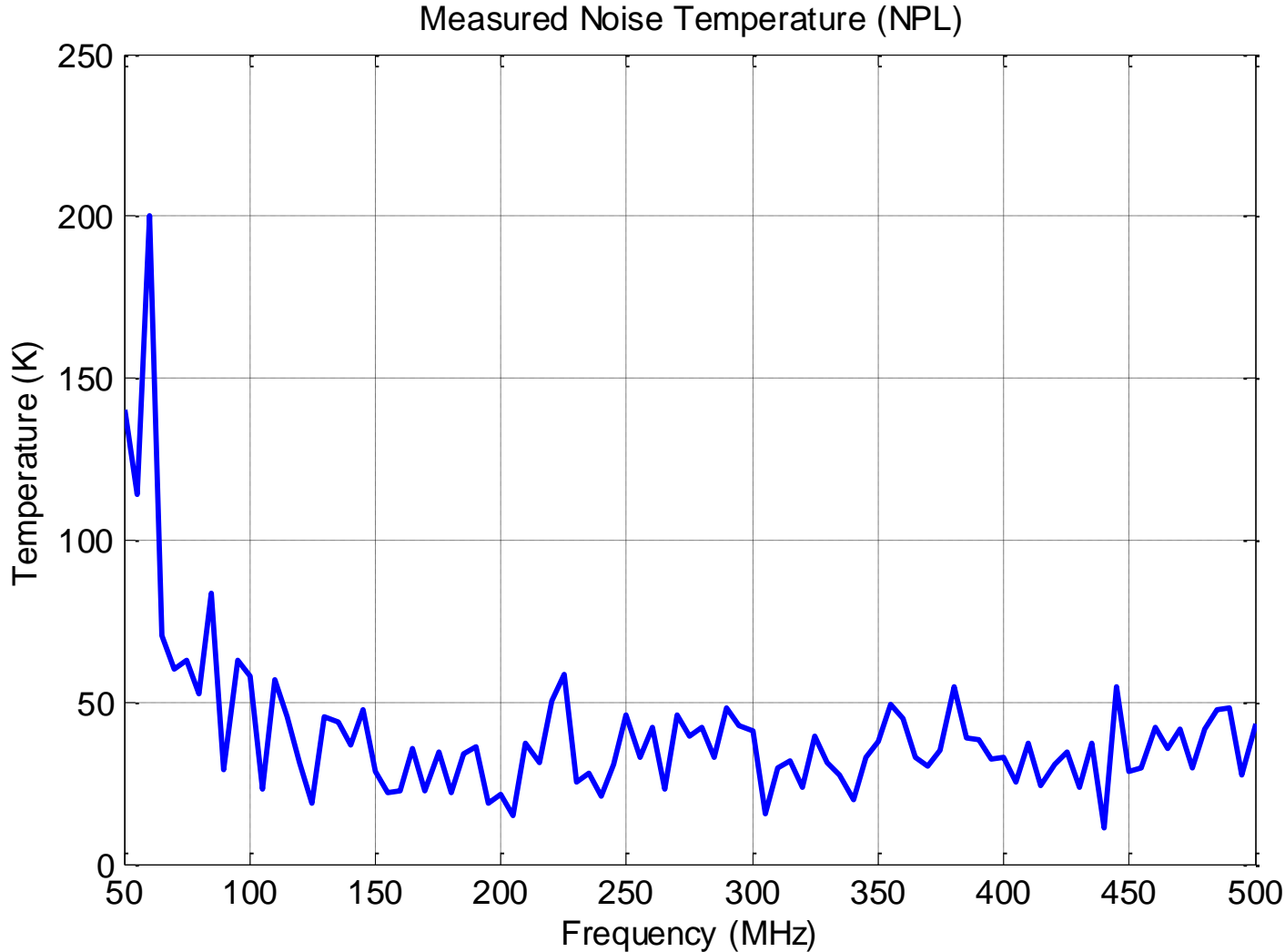
Near Field Scanner does not give meaningful measurements

Credit: B. Fiorelli, ASTRON.

Measurements: LNA

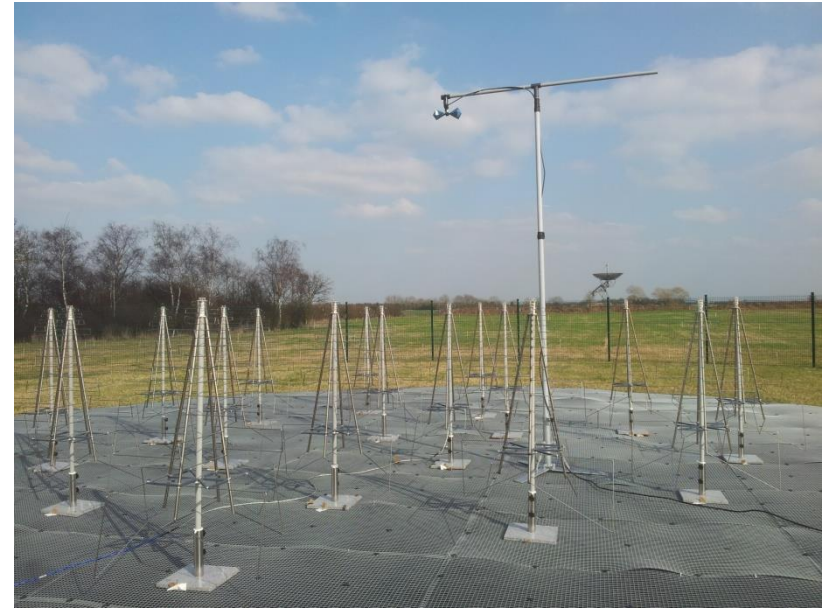


- 1st stage amplifier with Agilent noise analyser in reverberation chamber.



Test arrays

- AAVS0, and AAVS05:
16 dual-polarised SKALA elements.
- Aim: Test realistic SKA AA-low front-end technology in an array environment.
 - Cross check with simulations: mutual coupling, embedded element patterns and noise.
- Tests:
 - Mutual coupling.
 - Patterns (using near field probe, micro-copter, 2 element interferometer (alt-az mount), etc.).
 - Noise: Hot/cold pointing of the array.
 - RFI & satellites.
 - Imaging experiment.
 - Further tests to check software, calibration strategies, cross-polarization, cross-talk, tolerances, lightning modelling environmental, etc.



AAVS0 array under test



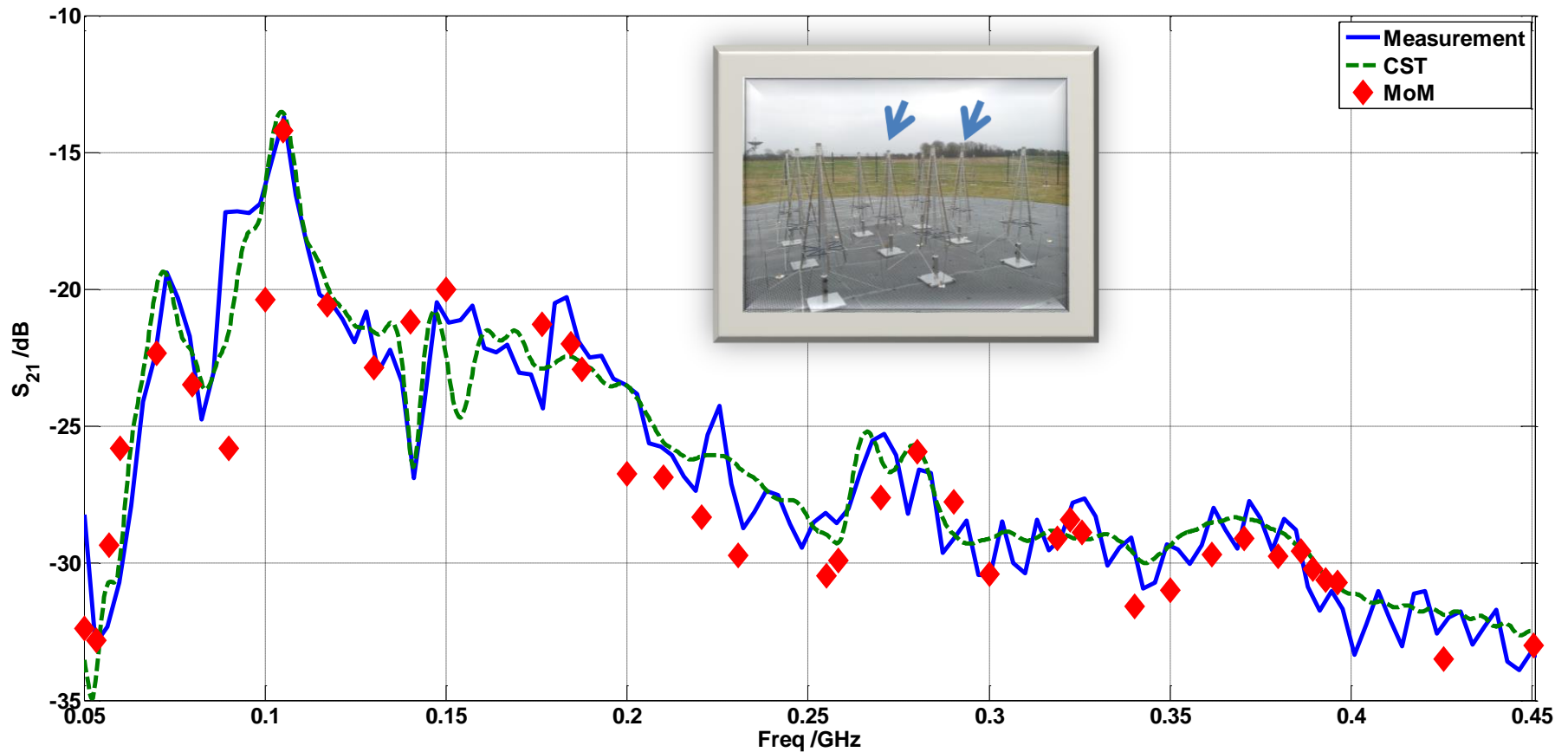
UNIBOARD
back end

AAVS0 test array at Lords Bridge

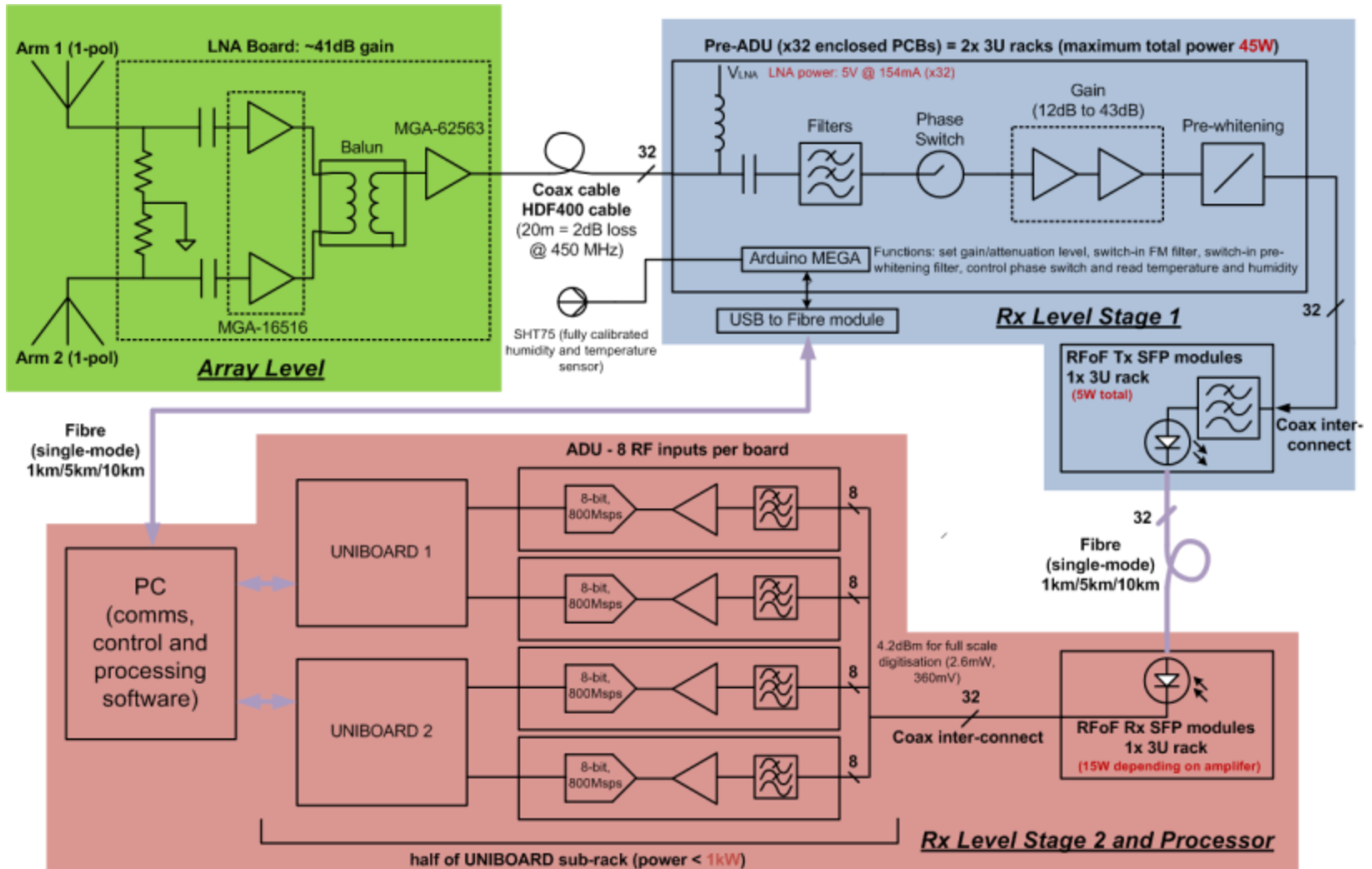


Test arrays

- Mutual coupling



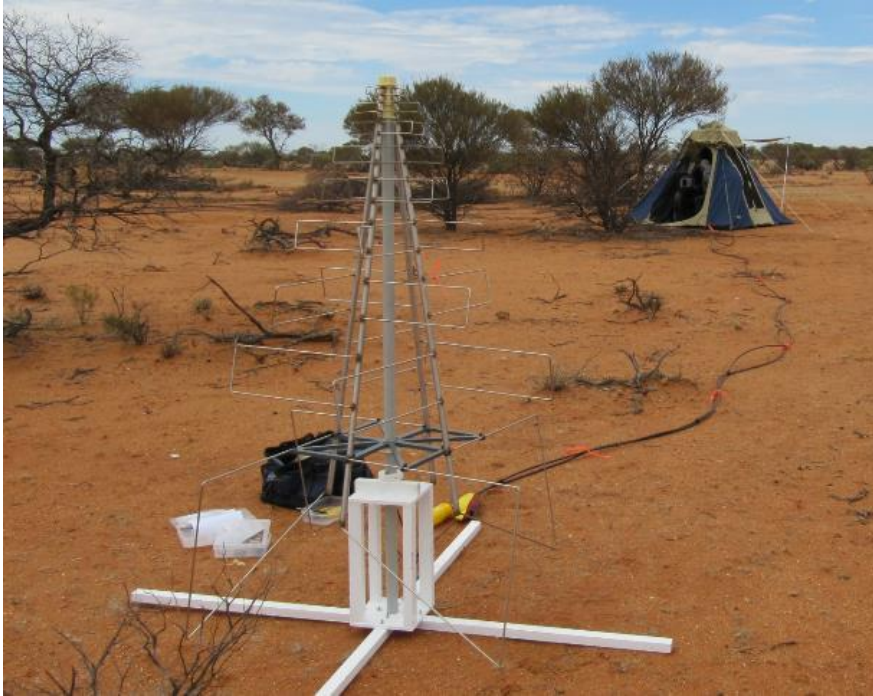
AAVSO



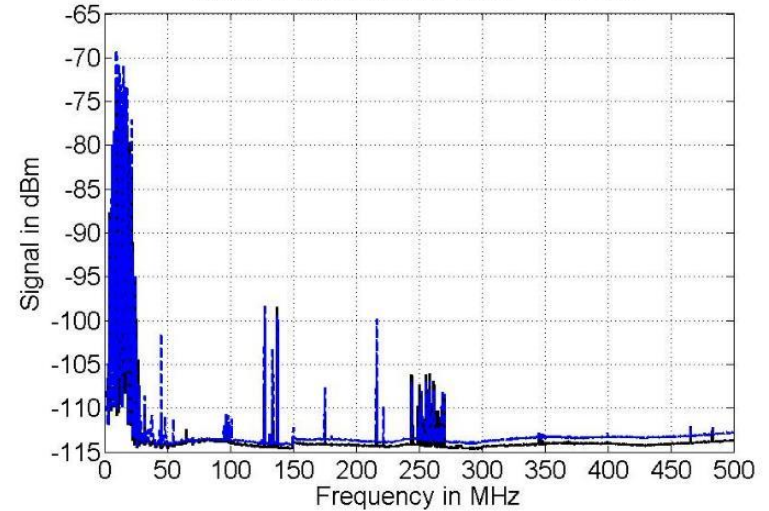
AAVS0.5 test array at MRO, Western Australia



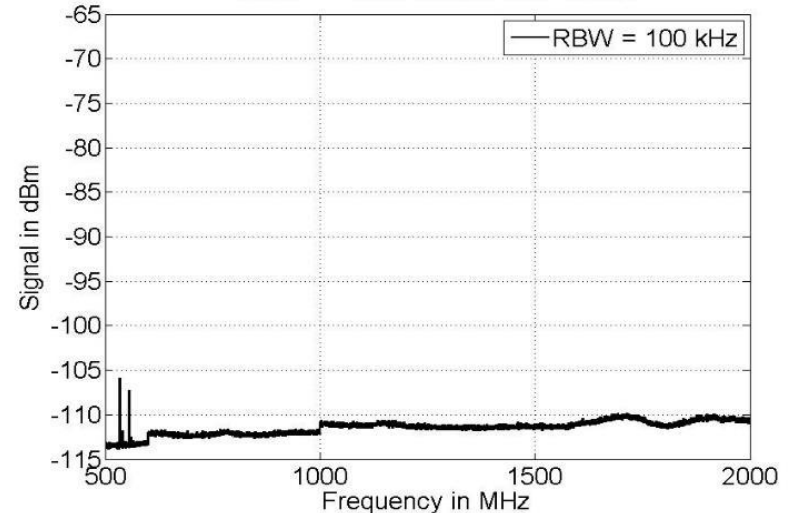
AAVS0.5: RFI Testing



Position 1 - 99% values:
black: N-S, blue: E-W; RBW = 100 KHz

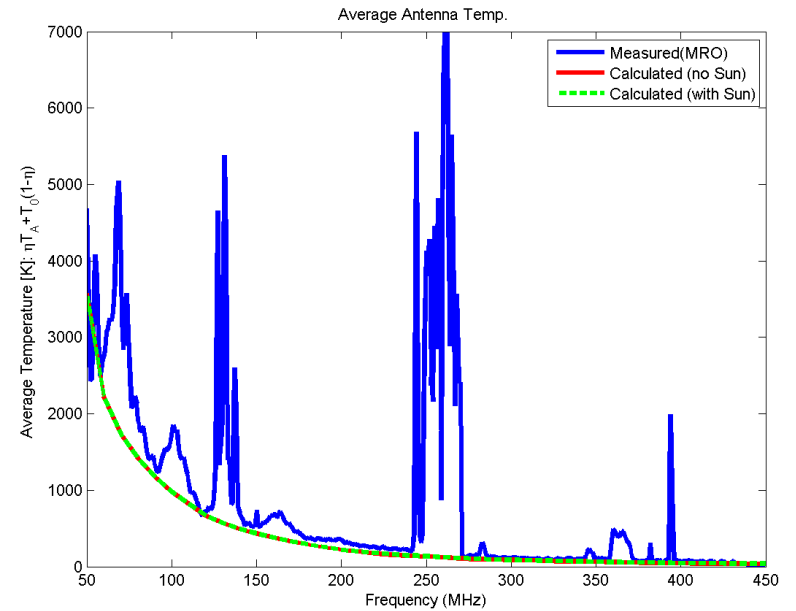
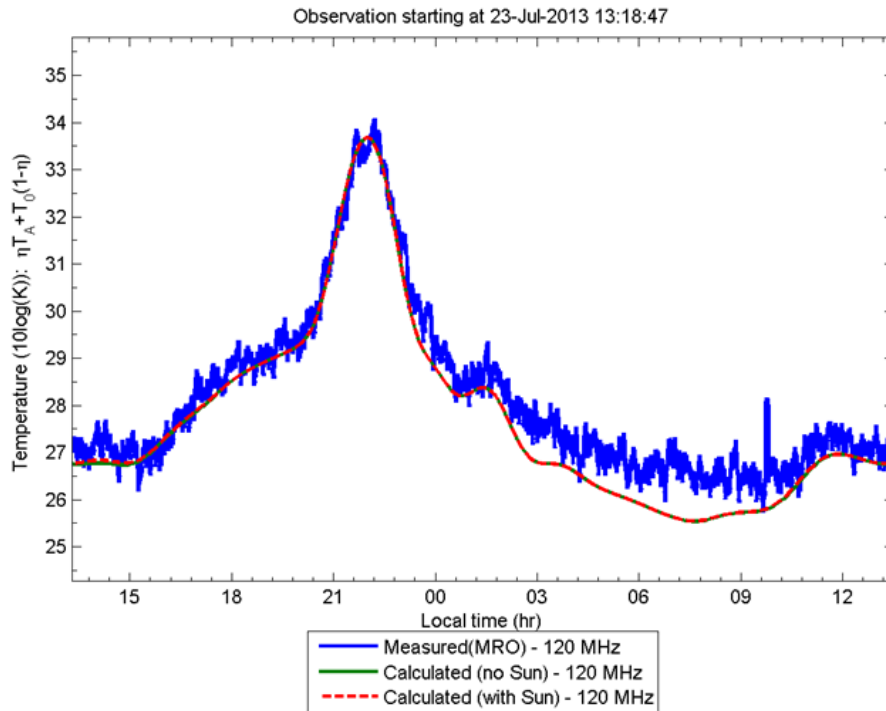


Position 1 - 99% values: North-South



- *Credit: A. Sutinjo, F. Schlagenhauser*

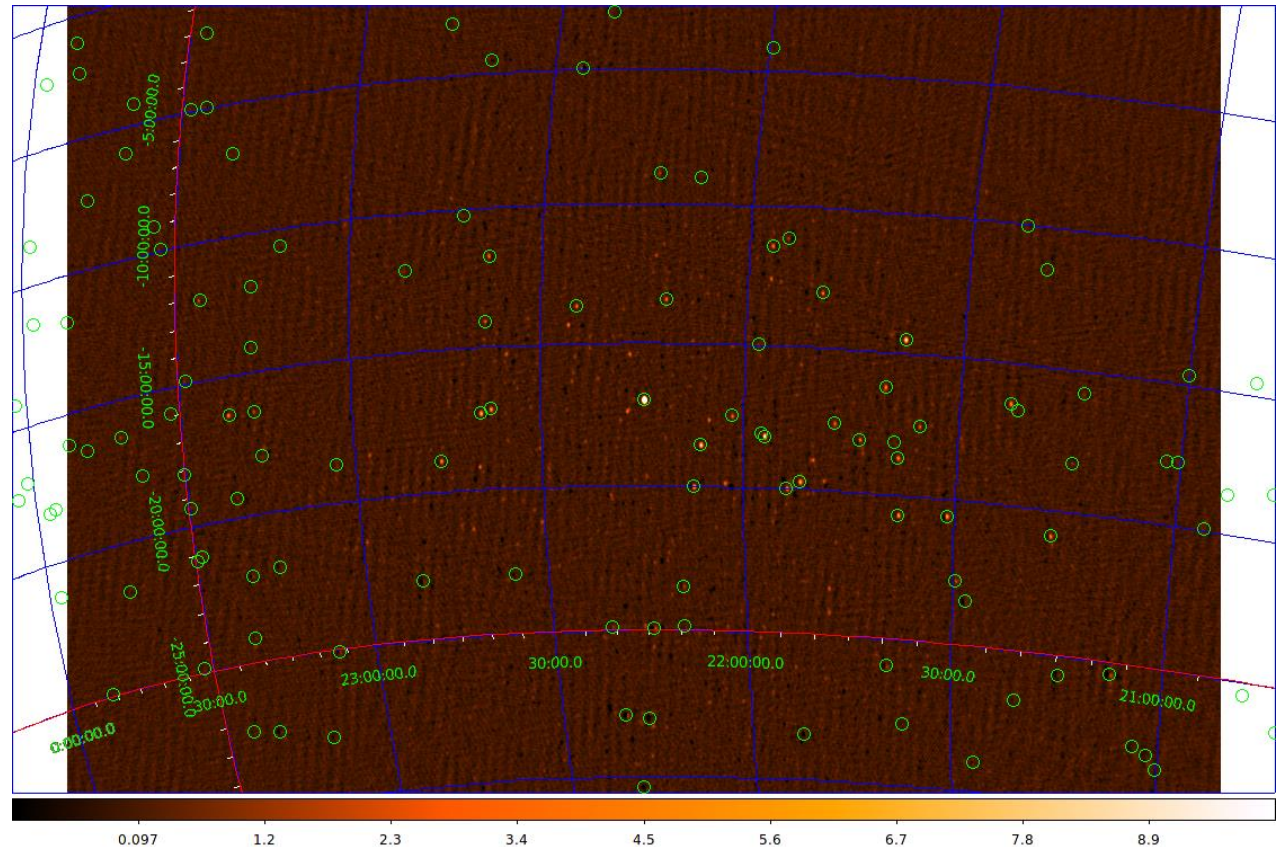
AAVS0.5: 24 hour drift-scan



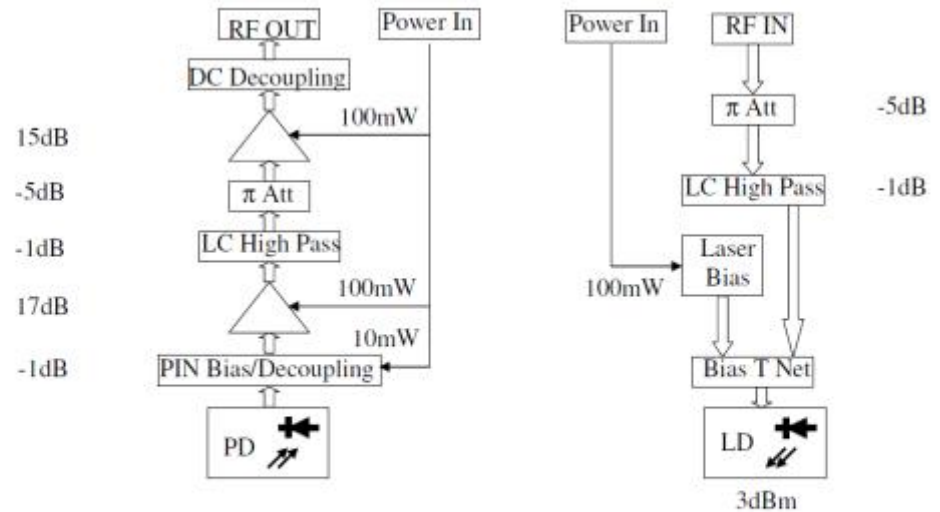
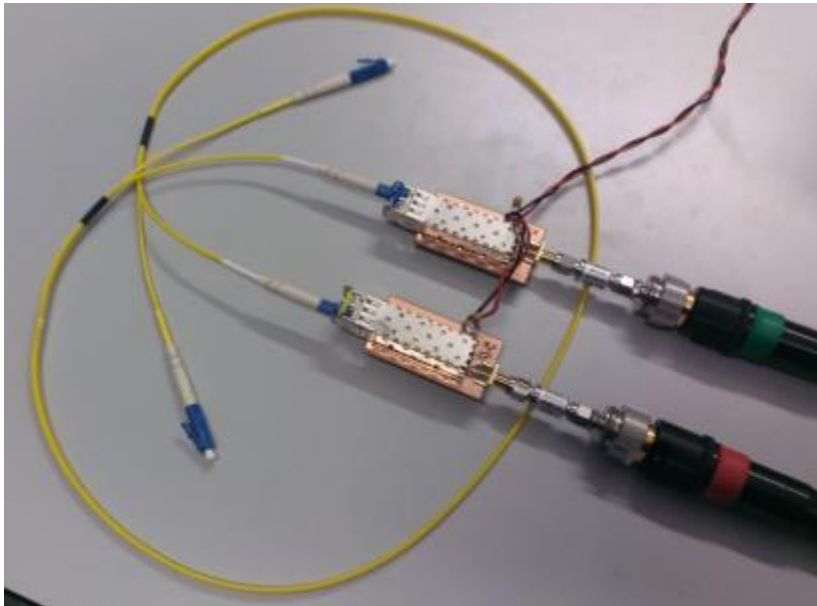
- *Credit: A. Sutinjo, P. Hall*

AAVS0.5: Correlation with MWA (first image)

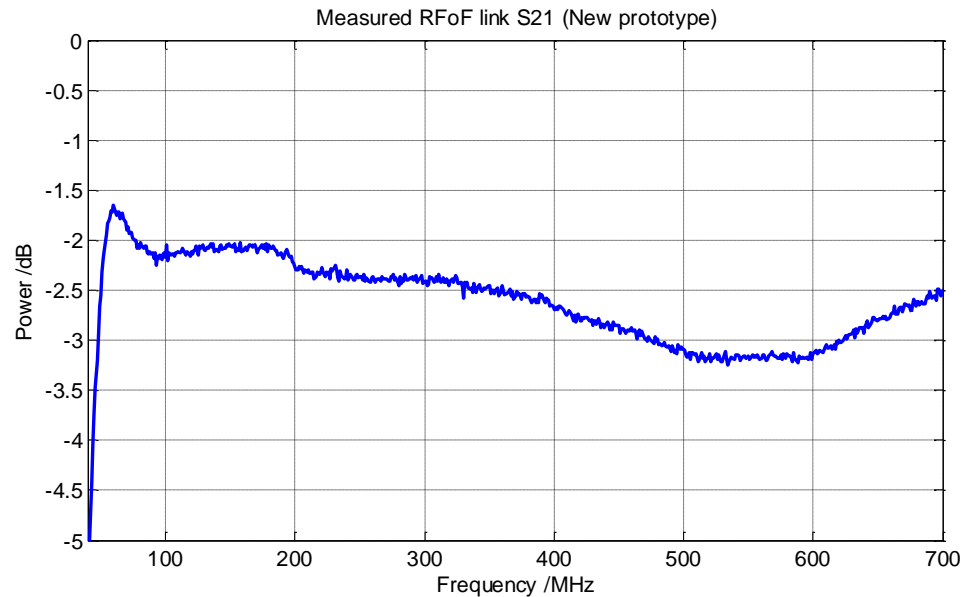
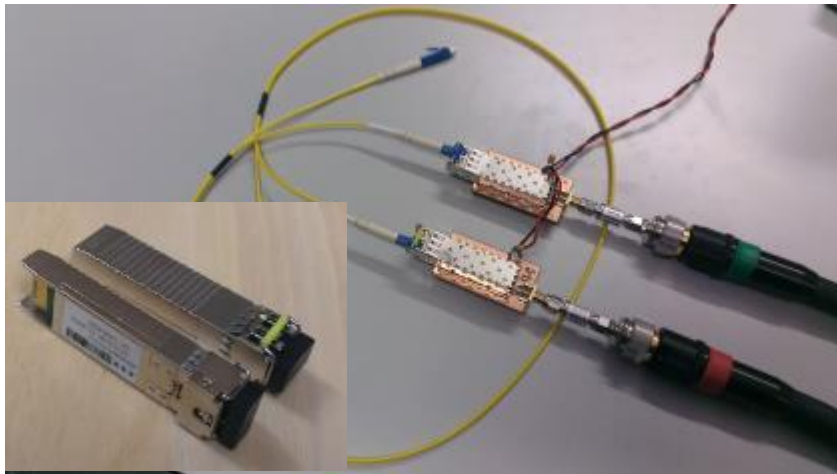
- 2 minute integration, wide-field snapshot, centred on 3C444
- AAVS 0.5 baselines only (but calibrated using whole MWA)



RFoF: 2nd prototype

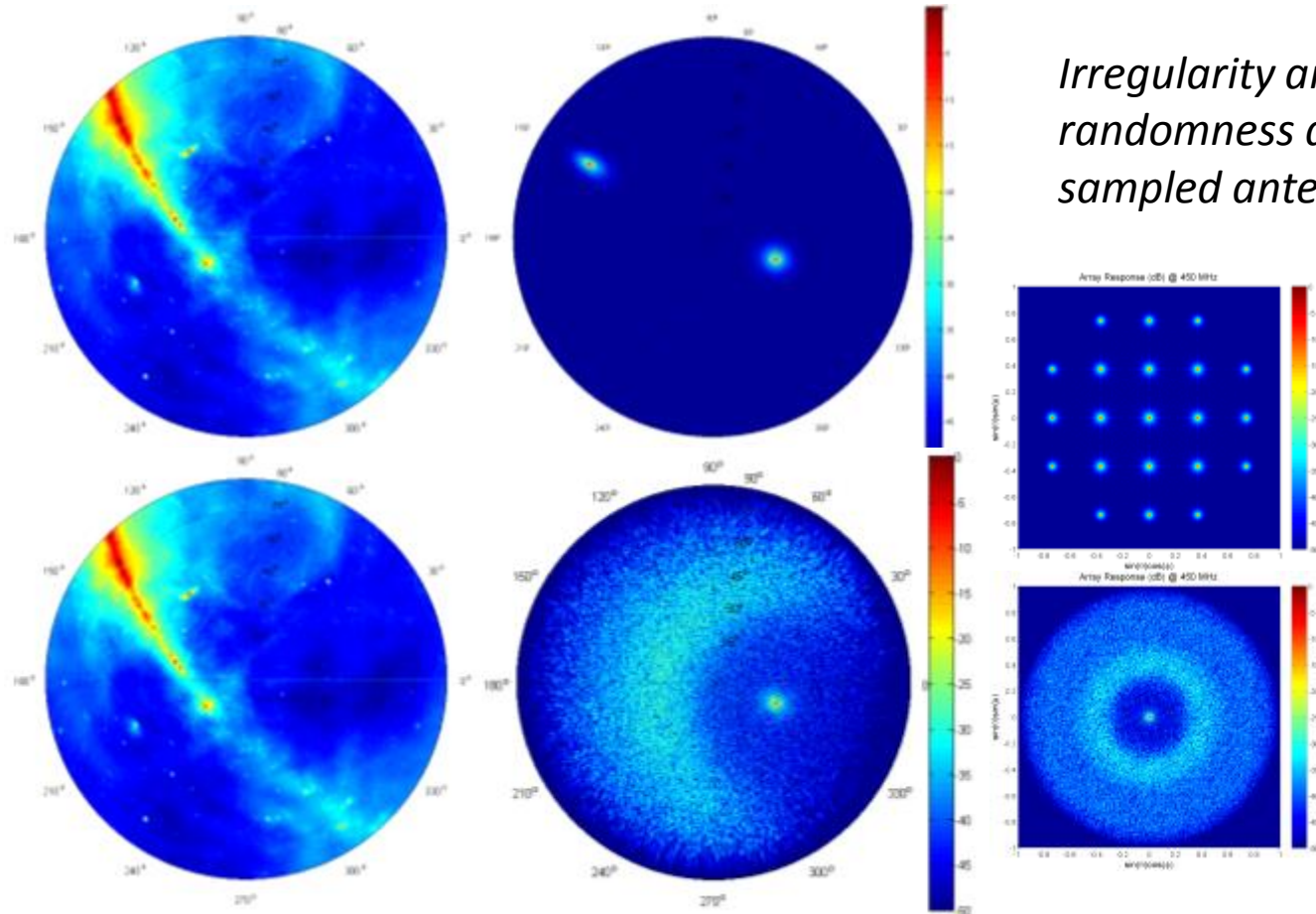


RFoF: 2nd prototype performance

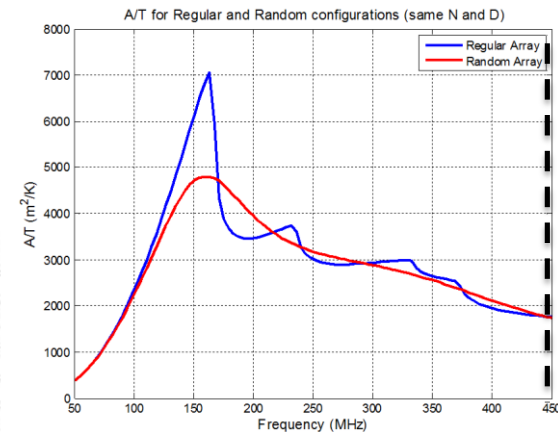
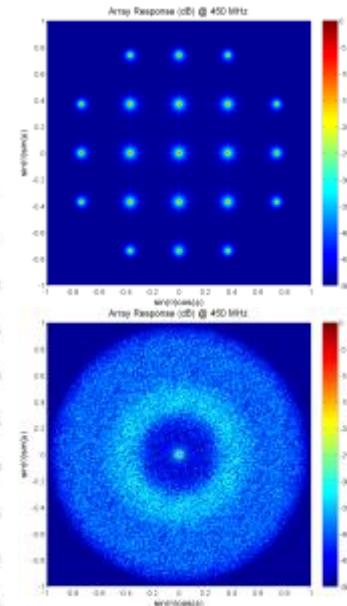


- Design BW: 50-700 MHz, -60dBm input, <2dB Passband ripple
- 1310nm, single mode G. 652/G. 655 fibre, LC/UPC connector
- Pros: Good link performance across SKA LFAA band, small footprint (SFP), low power (Tx: 5V@30mA, Rx: 5V@95mA)
- Cons: Temperamental connectors (not angled)

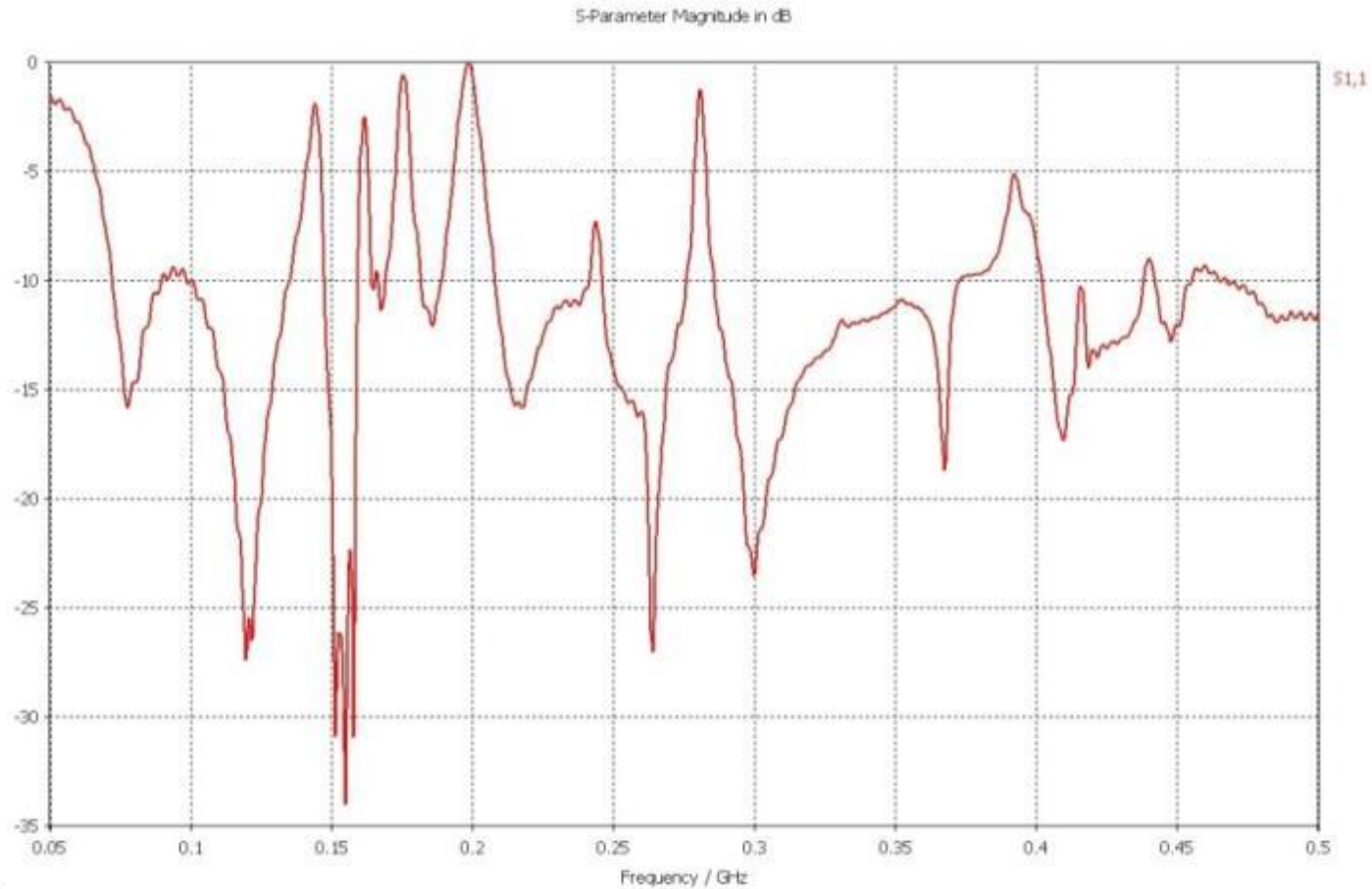
How configuration affects astronomical measurements



Irregularity and in particular randomness are vital for under-sampled antenna arrays

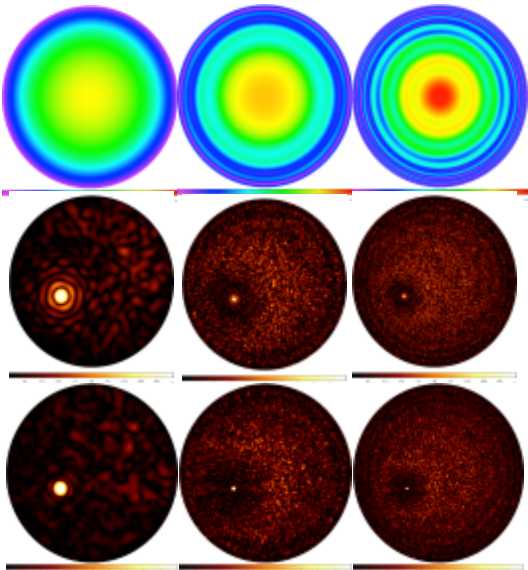
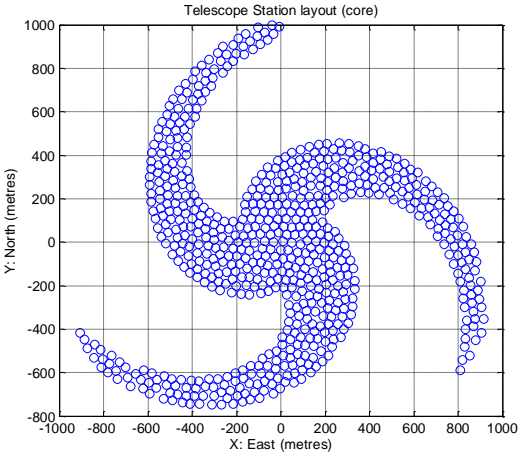


Effects of mutual coupling in regular arrays

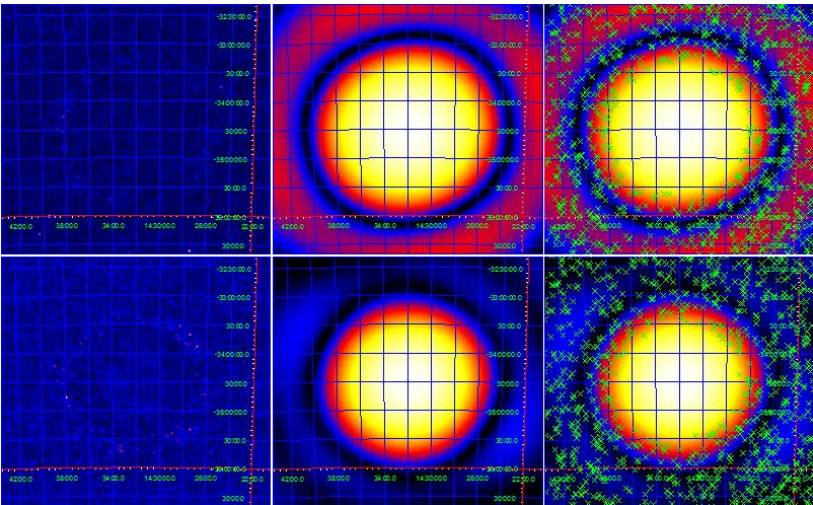
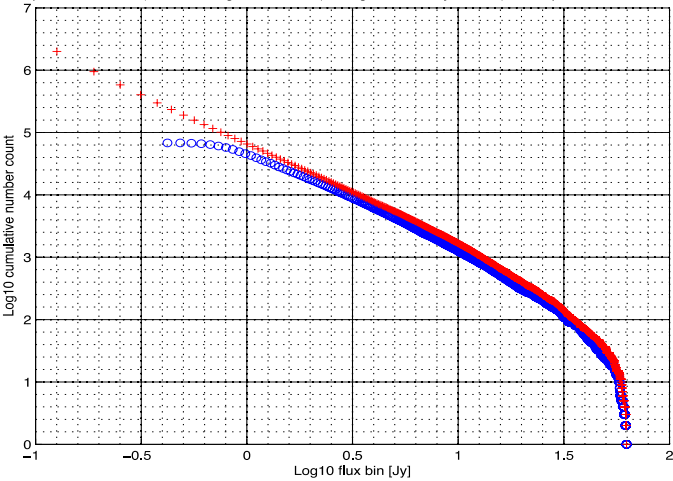


Simulations and Calibration for SKA-low

OSKAR2 simulations

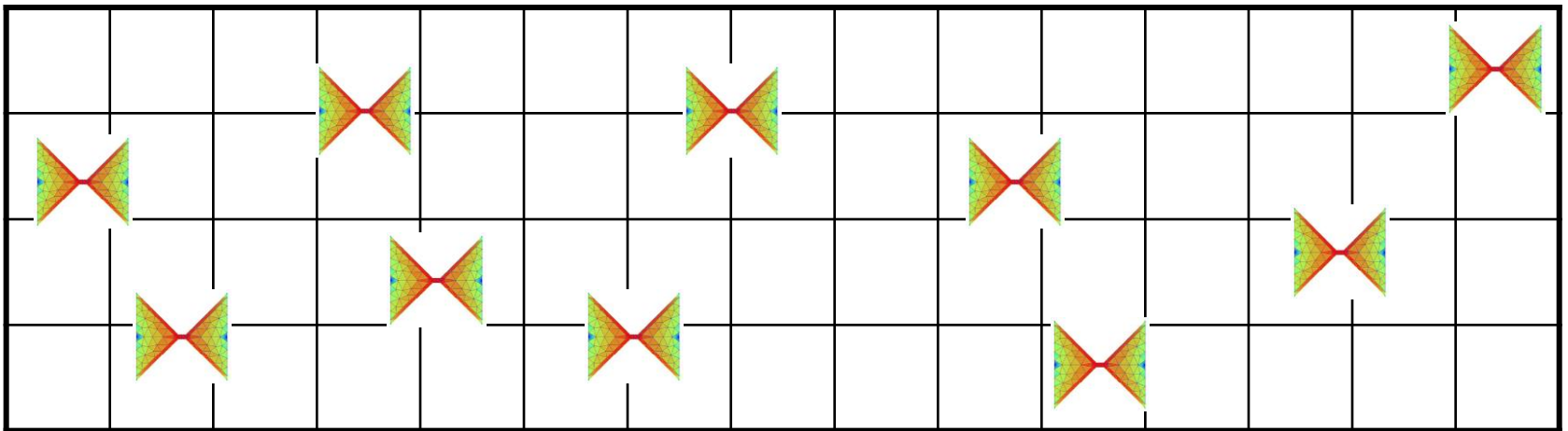


Comparison of VLSS (minus 50 brightest sources) with generated sky model (broken power law; 2M sources)



MoM-MBF simulation of large irregular arrays

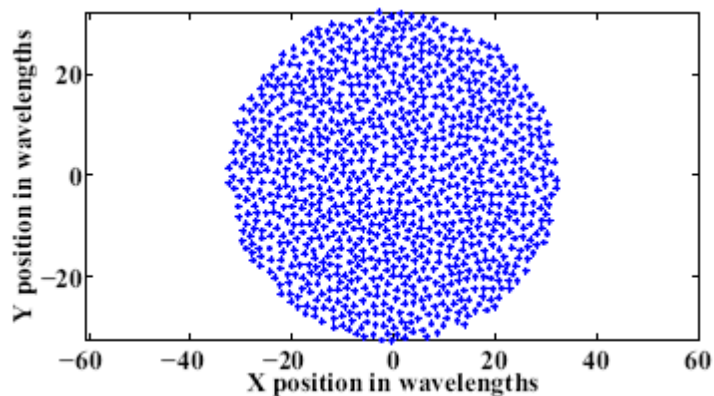
- Based on **Method of Moments + MBFs** (CBFs) and the interpolation technique presented in [1], where the computation of interactions between MBFs is carried out by **interpolating exact data obtained on a simple grid**.



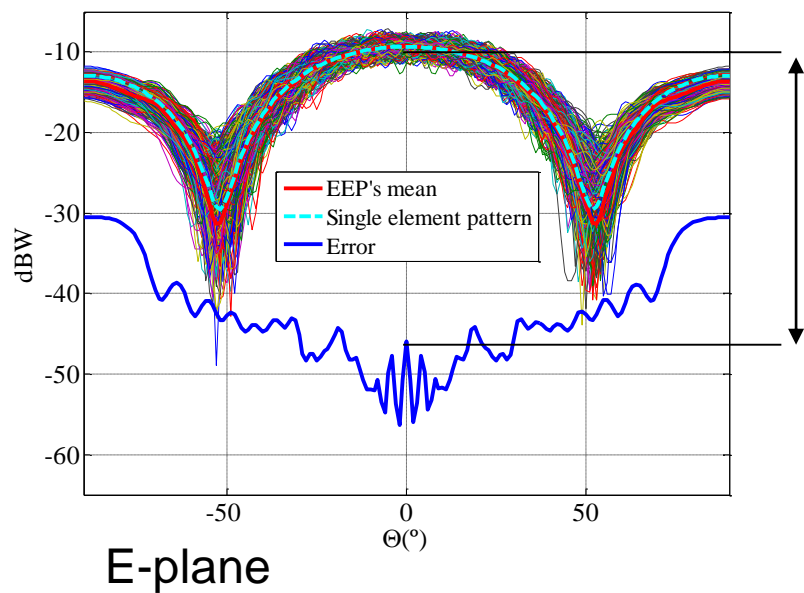
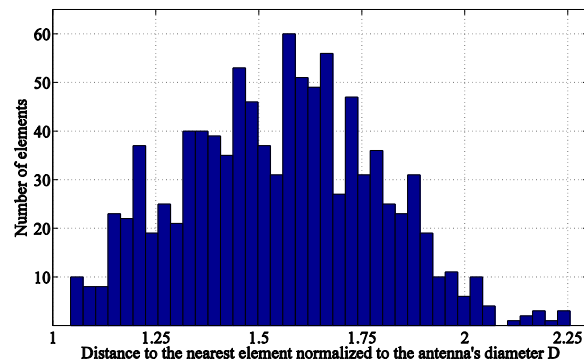
[1] David Gonzalez-Ovejero, Christophe Craeye, "Interpolatory Macro Basis Functions Analysis of Non-Periodic Arrays," IEEE Trans. Antennas Propag., vol.59, no.8, pp.3117,3122, Aug. 2011

Mutual coupling in irregular arrays

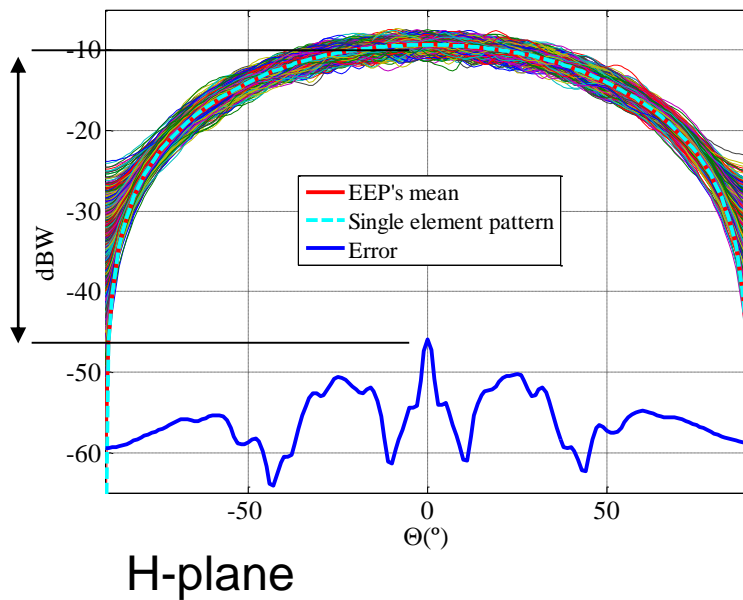
$$e = 10 \log_{10} \left(\left| E_{mean}^{\rightarrow}(\theta, \phi) - E_{single}^{\rightarrow}(\theta, \phi) \right|^2 \right)$$



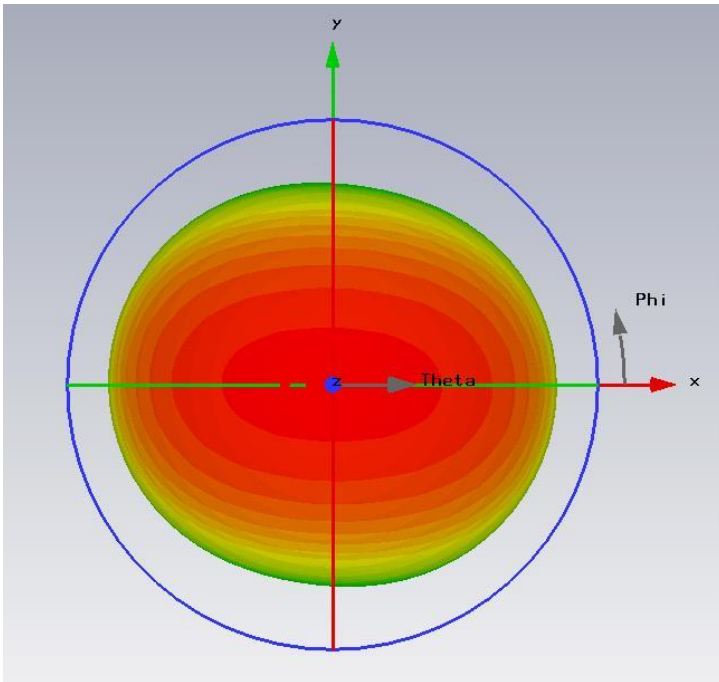
Random configuration



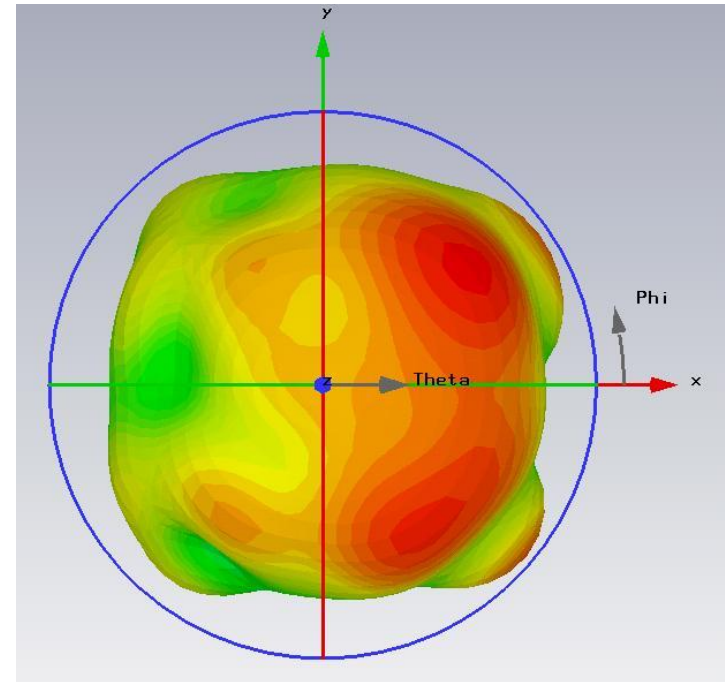
~ 35 dB



$$\text{Station_Beam} = \text{Array_Factor} \times \text{Average_EEP}$$

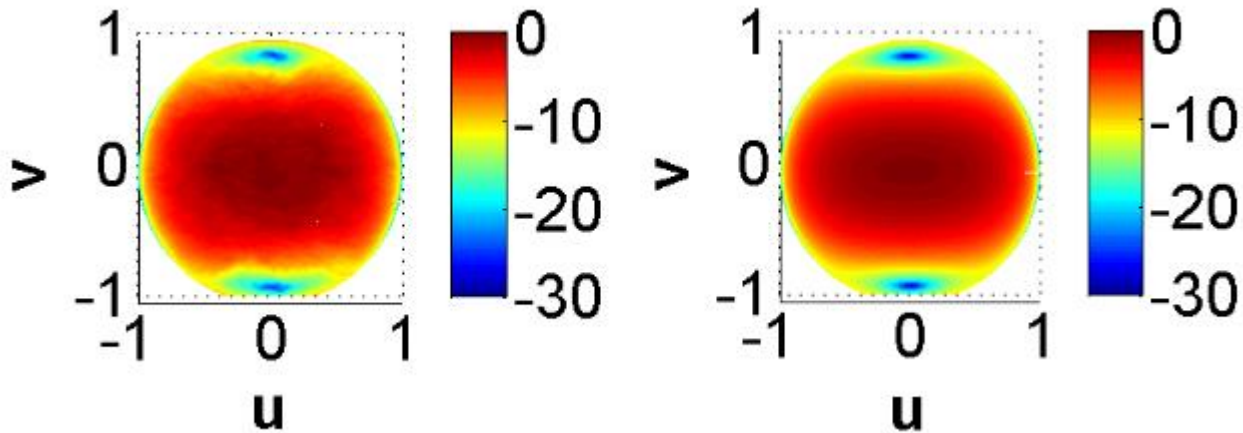


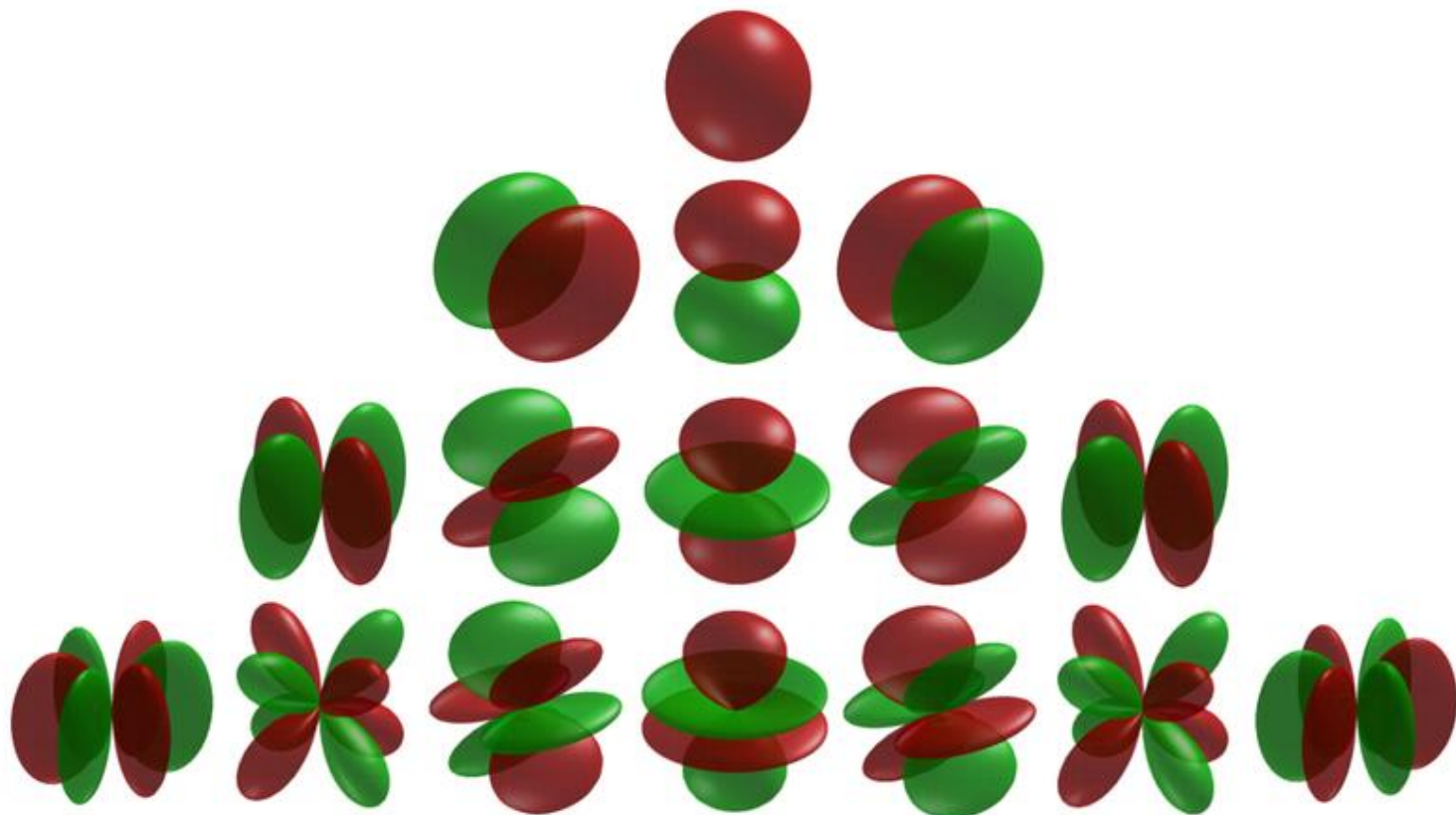
Average Embedded Element Pattern



Pattern of a given element

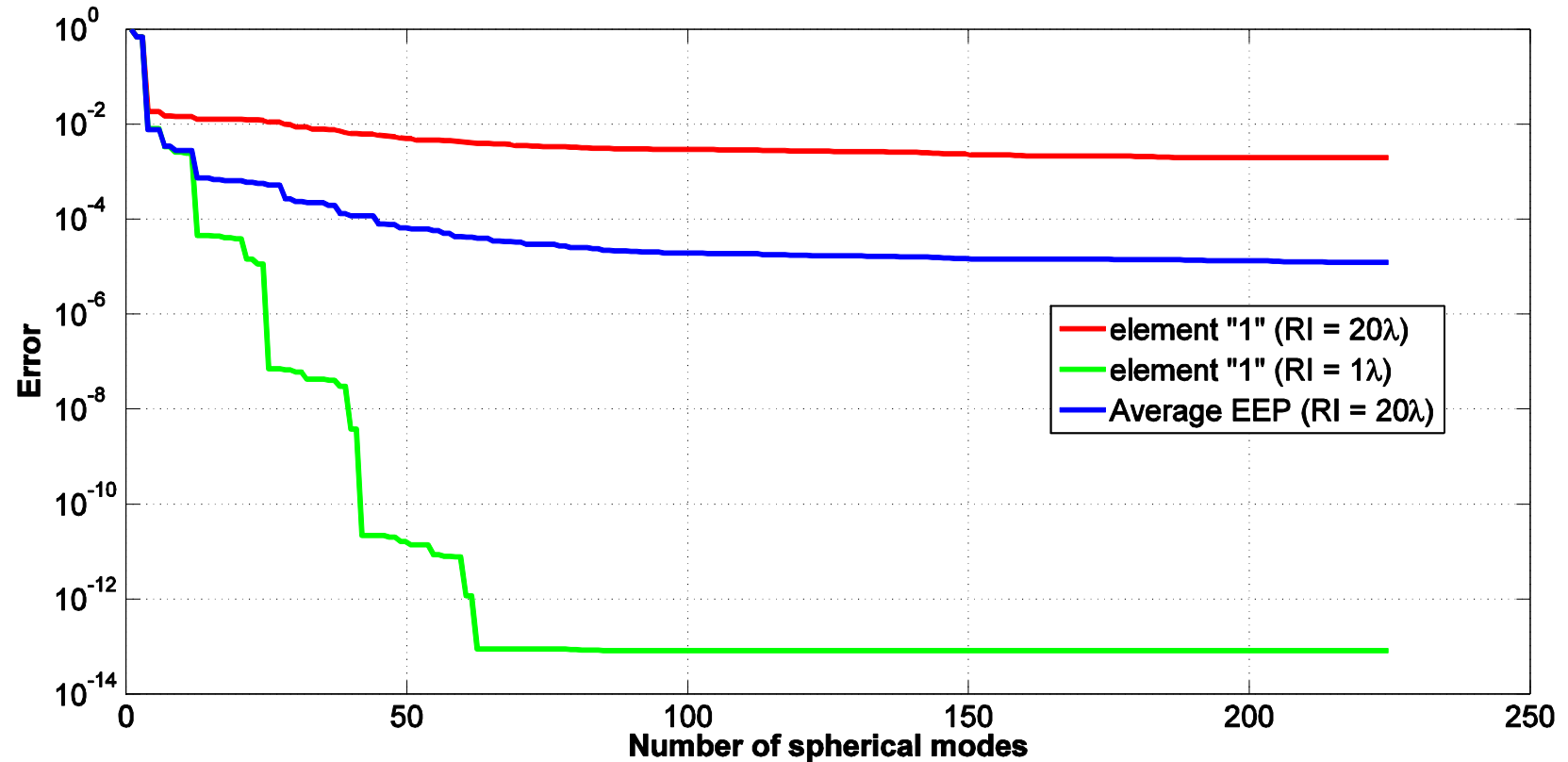
Beam Models for pattern prediction/calibration (inspired by Jan Noordam and the 3GC workshops)



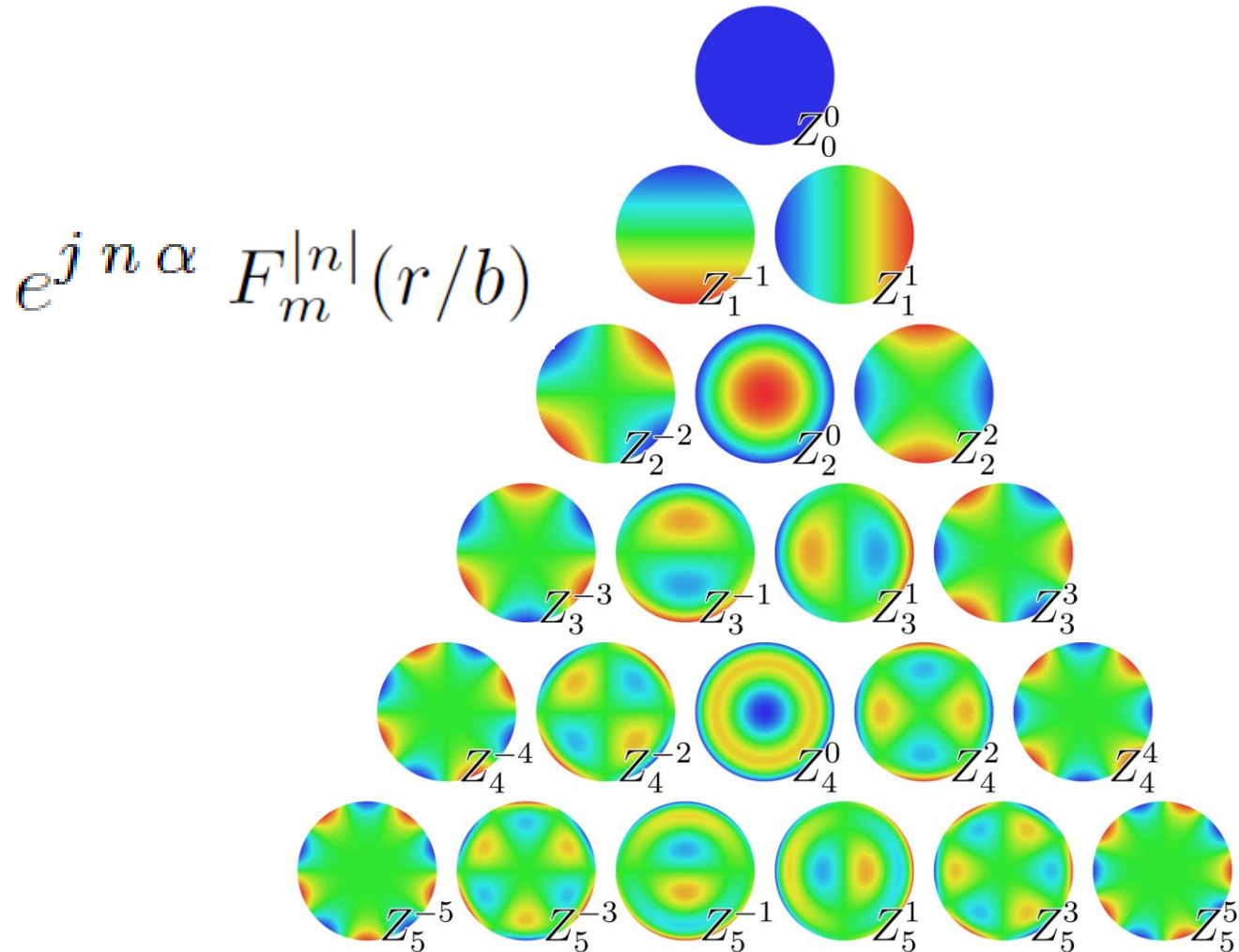


Spherical Harmonics

Average Embedded Element Pattern

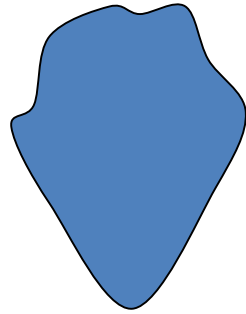


Zernike functions



Picture from Wikipedia

Array factorisation



$$\vec{J}_{ns} \simeq \sum_{p=1}^P C_{nsp} \vec{J}_p^{\circ}$$



Antenna index

| | | | | |
|-------|-----------|-----------|-----------|--|
| MBF 1 | C_{111} | C_{211} | C_{311} | Coefficients for IDENTICAL current distribution |
| MBF 2 | C_{112} | C_{212} | C_{322} | |
| ... | | | | |

$$\vec{F}_s \simeq \sum_{p=1}^P \sum_{n=1}^N \left(\sum_{s=1}^N A_s C_{nsp} \right) e^{j k \hat{u} \cdot \vec{r}_n} \vec{F}_p^{\circ}$$

$\vec{F}_p^{\circ} \rightarrow \mathbf{AF}_p$

Zernike representation of deficiencies in the pattern including mutual coupling

$$\overline{F_{rec}}(\theta, \phi) = \sum_{m=1}^t \alpha_m \sum_{i=1}^n \overline{f}_i(\theta, \phi) e^{-j(\varphi_i - \varphi_{i,0})} Z_m$$

- Basis functions = EEPs.
 - They can be pre-computed accurately.
 - They are smooth and can be stored with low resolution.
- The variations wrt the simulated response are mapped using Zernike polynomials.
 - They are generic and flexible.
 - We can optimize the number of coefficients needed according to the number of sky sources available.
- The weights for the “predicted” pattern can be found from the combination of basis functions.

Low Order Beam Models for Calibration

Zernike representation of deficiencies in the pattern including mutual coupling

$$\overline{F}_{rec}(\theta, \phi) = \sum_{m=1}^{\tau} \alpha_m \sum_{i=1}^n \overline{f}_i(\theta, \phi) e^{-j(\varphi_i - \varphi_{i,0})} Z_m$$

- The **Embedded Element Patterns** (EEPs) define the “expected” array pattern.
- The variations with respect to the simulated response are mapped using **Zernike polynomials**.*
- The **weights** for the “reconstructed” pattern can be found from the combination of basis functions and a least squares estimation from a few measured points.

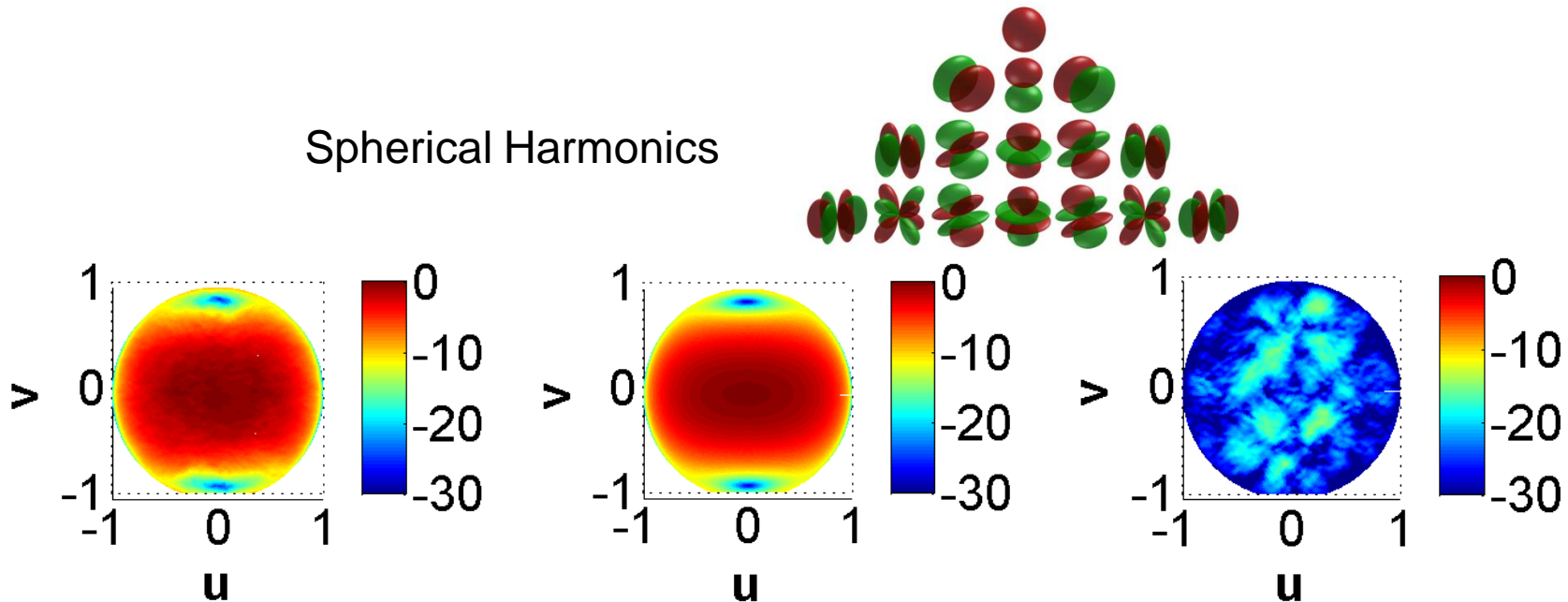
*Before: C. Craeye et al. (2012): $AP = \sum_k AF_k x MBF_k$

Use of pre-computed EEPs

$$\begin{aligned} \overline{F}_{rec}(\theta, \phi) \\ = \sum_{m=1}^t \alpha_m \sum_{i=1}^n \overline{f}_i(\theta, \phi) e^{-j(\varphi_i - \varphi_{i,0})} Z_m \end{aligned}$$

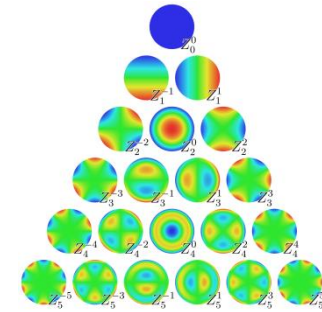
- They can be pre-computed accurately.
- They are smooth and can be stored with low resolution (enough for main beam and first few side-lobes). Better simulated EEPs mean less Zernike polynomials needed.

Spherical Harmonics

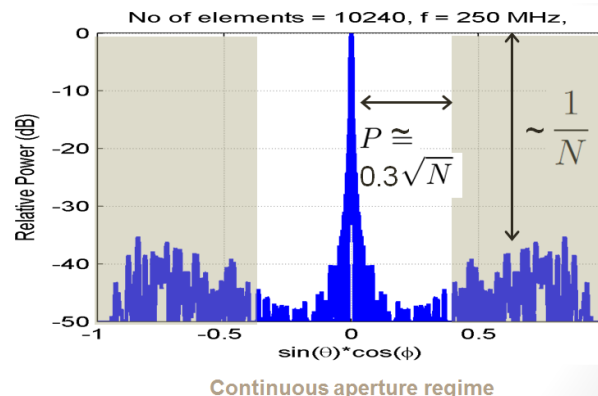
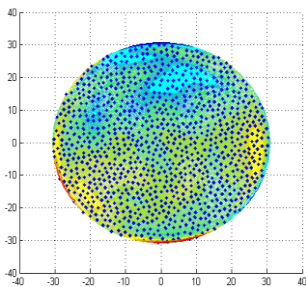


Use of Zernike polynomials

$$\overline{F_{rec}}(\theta, \phi) = \sum_{m=1}^t \alpha_m \sum_{i=1}^n \overline{f}_i(\theta, \phi) e^{-j(\varphi_i - \varphi_{i,0})} Z_m$$



- It is inspired from radiation from apertures, but including effects of mutual coupling. In here, the Zernike polynomials map the divergences in the main beam and first side-lobes!
- They are generic and flexible.
- We can optimize the number of coefficients needed according to the number of available measurement points.



Similar to theory of ~circular apertures:

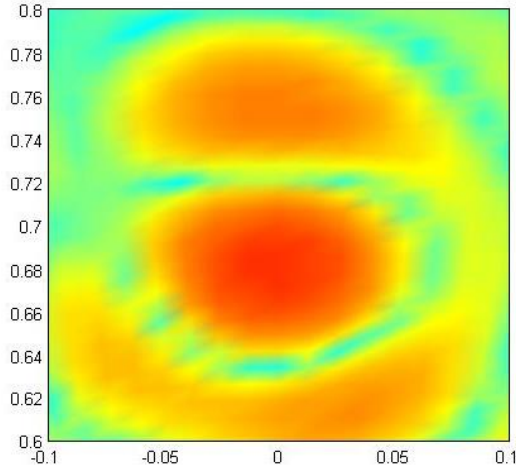
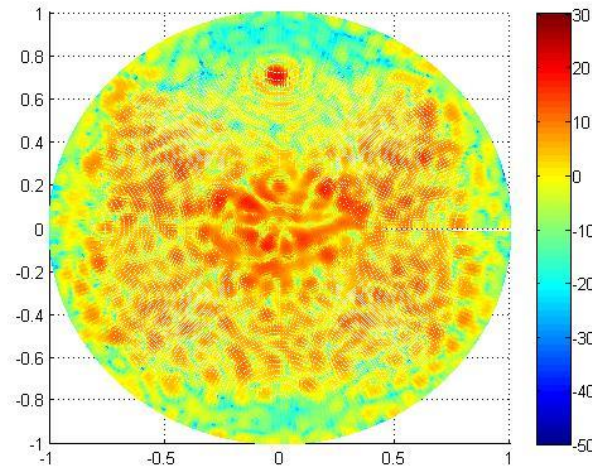
Y. Rahmat-Samii and V. Galindo-Israel, "Shaped reflector antenna analysis using the Jacobi-Bessel series," IEEE Trans. Antennas Propagat., Vol. 28, no.4, pp. 425-435, Jul. 1980.

Summarizing...

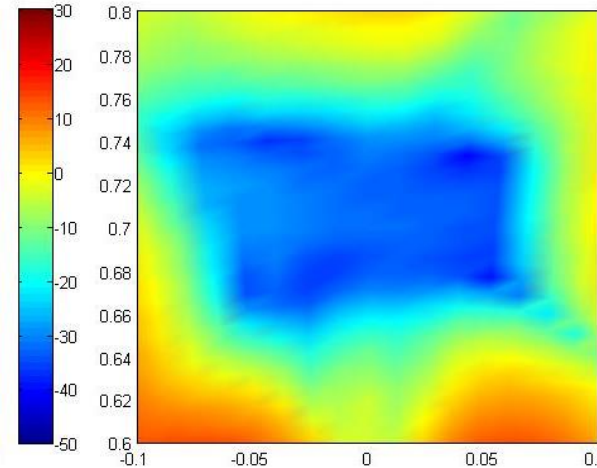
- The array pattern is modeled with (approximately) computed embedded element patterns.
- Each pattern is multiplied by a constant with smooth variation over the array (Zernike function)
- Zernike coefficients are estimated in least-squares sense based on observations.

Tests: Pointing error (2 deg.) - scanning

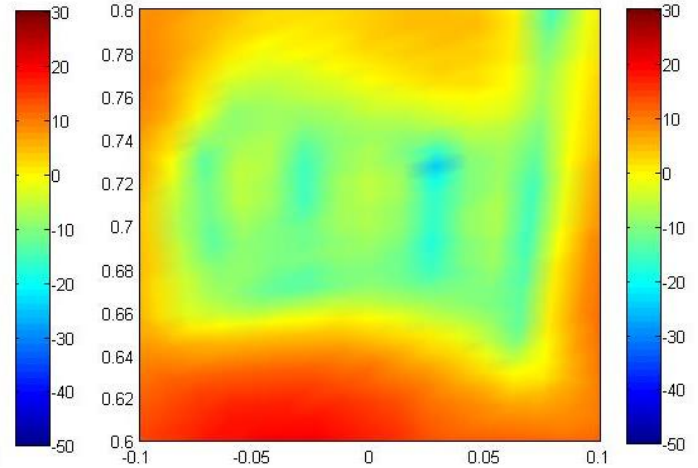
Scan:
 $\Theta = 45 \text{ deg.}$
 $\Phi = 90 \text{ deg.}$



Error Rec. - Actual



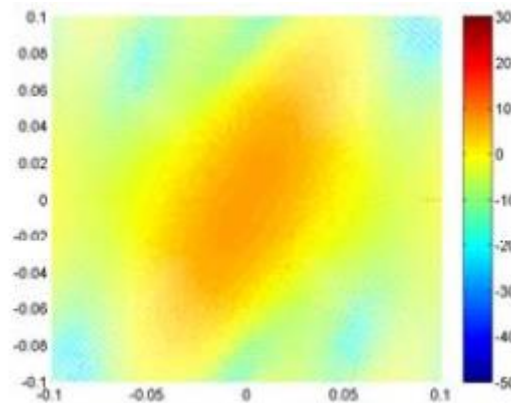
$t = 36, w = 81$



$t = 15, w = 16$

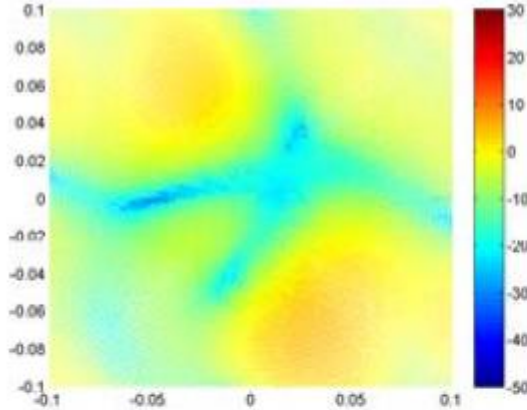
* t : number of Zernike polynomials / w : number of measured points.

Tests: Dead elements (10%)

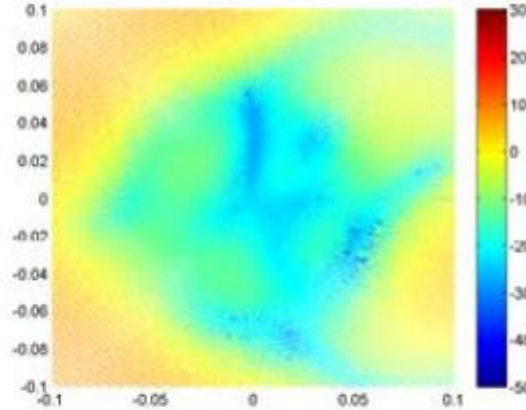


Error Rec. - Actual

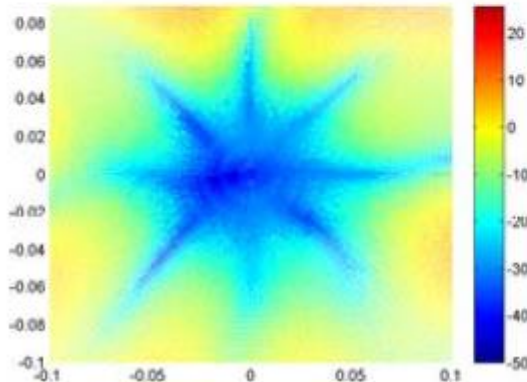
$t = 3$



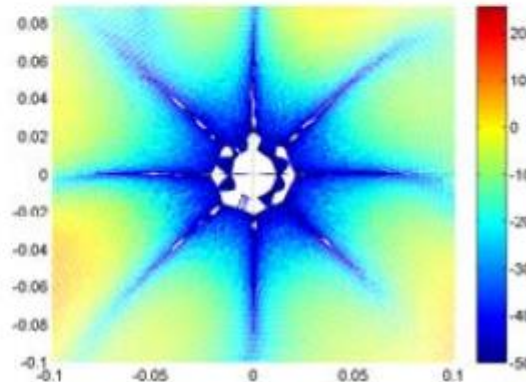
$t = 10$



$t = 21$



$t = 36$



* t : number of Zernike polynomials / w : number of measured points = 57.

Conclusions and Future Work

- The LFAA array will have a major demonstrator in Western Australia (AAVS1 with approx. 512 elements) by mid 2015. End of 2016 is the end of the pre-construction phase.
- Front-end technologies are being developed to meet the SKA budget and deployment/mechanical/environmental limits.
- Accurate beam models for calibration are essential and already exist. Use of UAV systems and demonstrator arrays are key for these developments.

Thank you