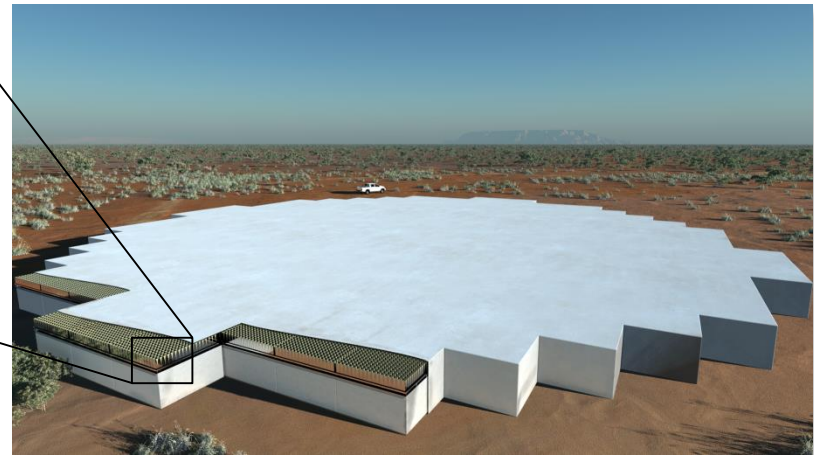


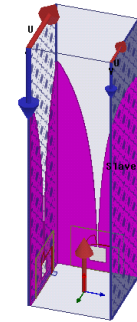
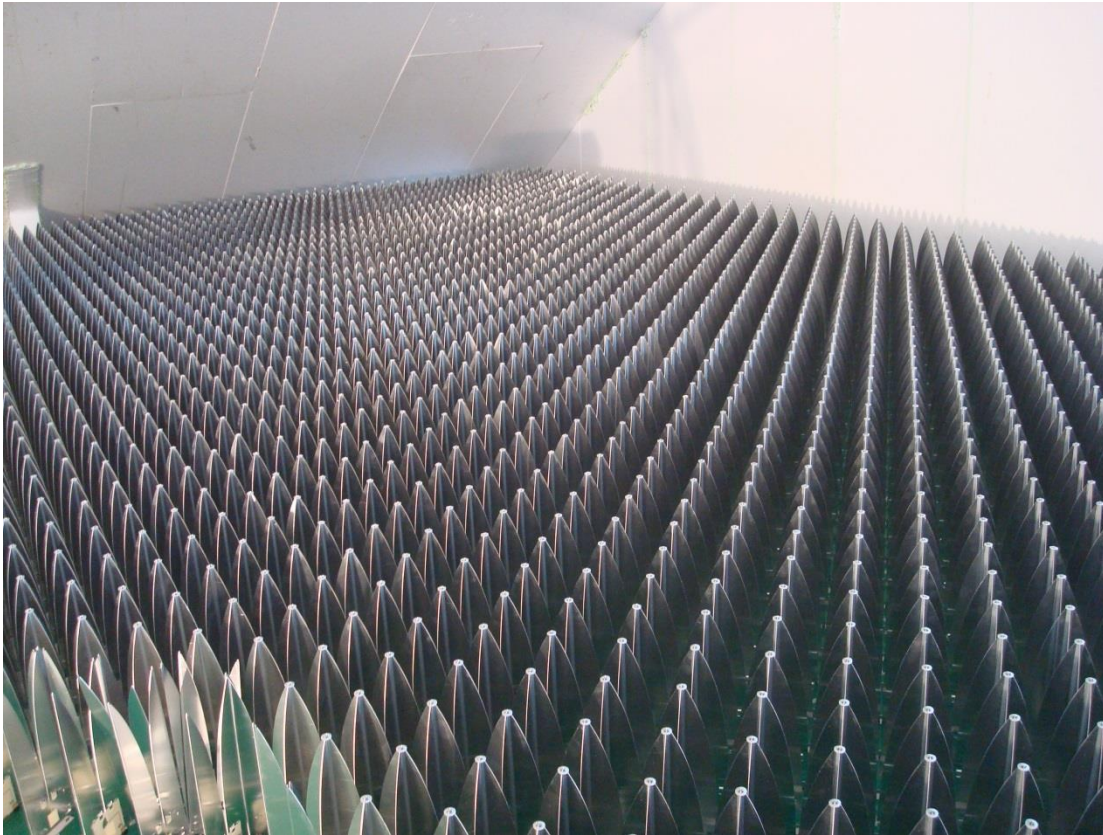
# Tile separation study for EMBRACE-like vivaldi dense array: polarimetry and sensitivity

*B. Fiorelli, M. Arts, E. van der Wal*



**MFAA**

Dense regular arrays



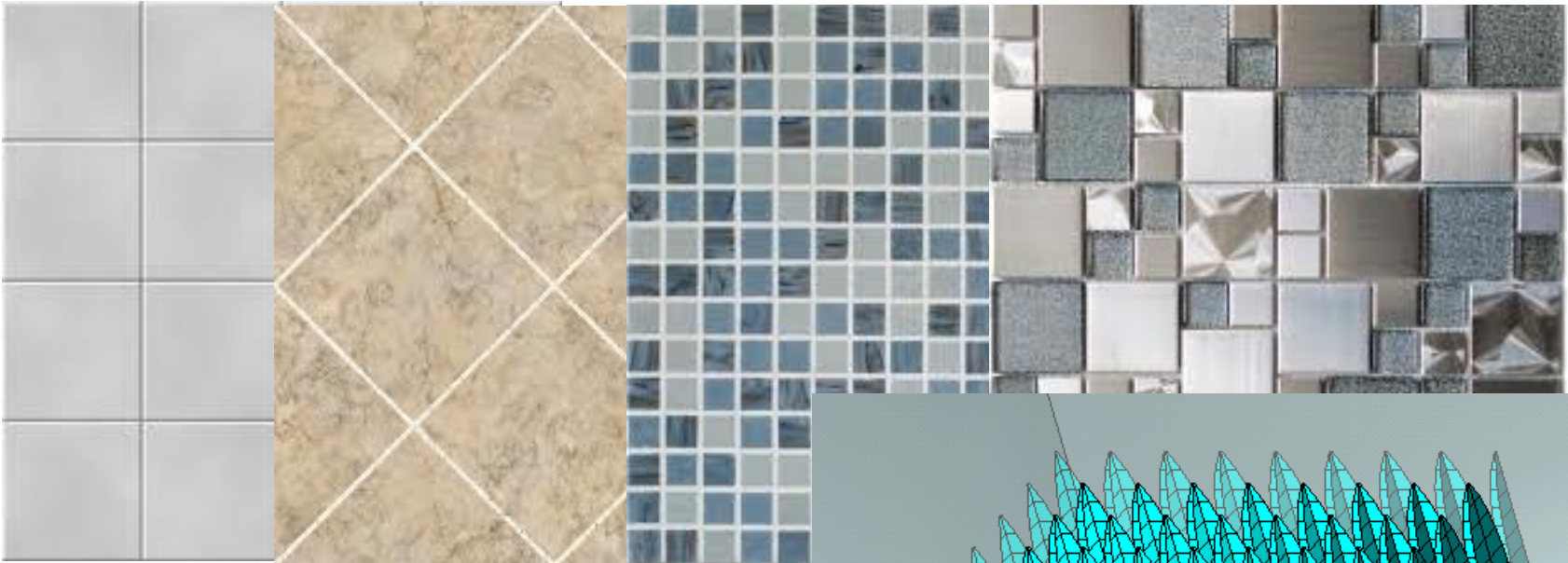
# Infinite Array + Station Edge Effect

## Finiteness of the array is an unavoidable

➡ Study the modular tiles edge effect



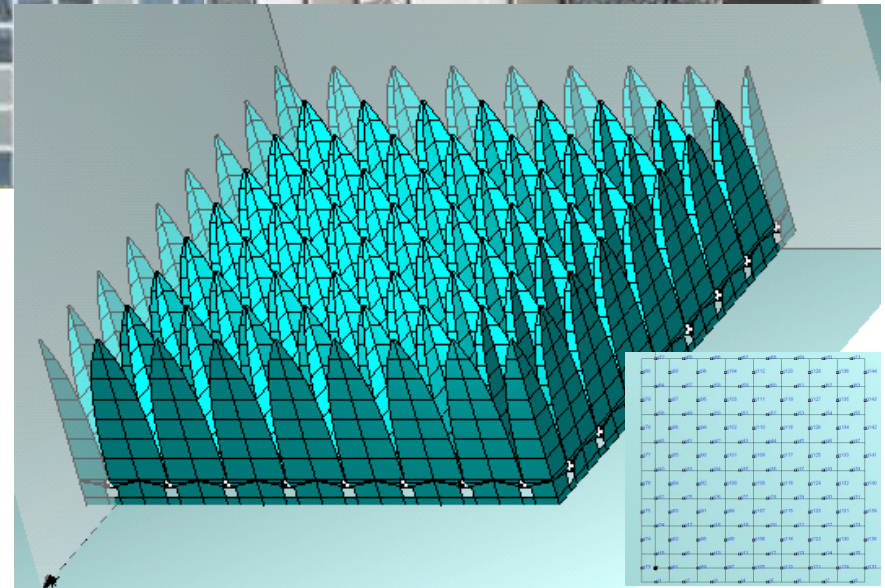
## What is a tile??



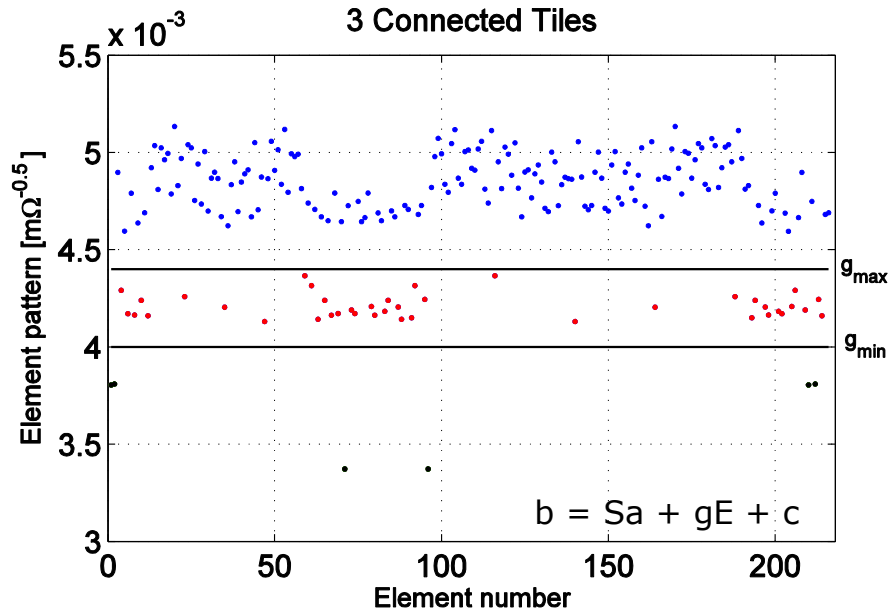
- Modular and regular
- Homogeneous performances



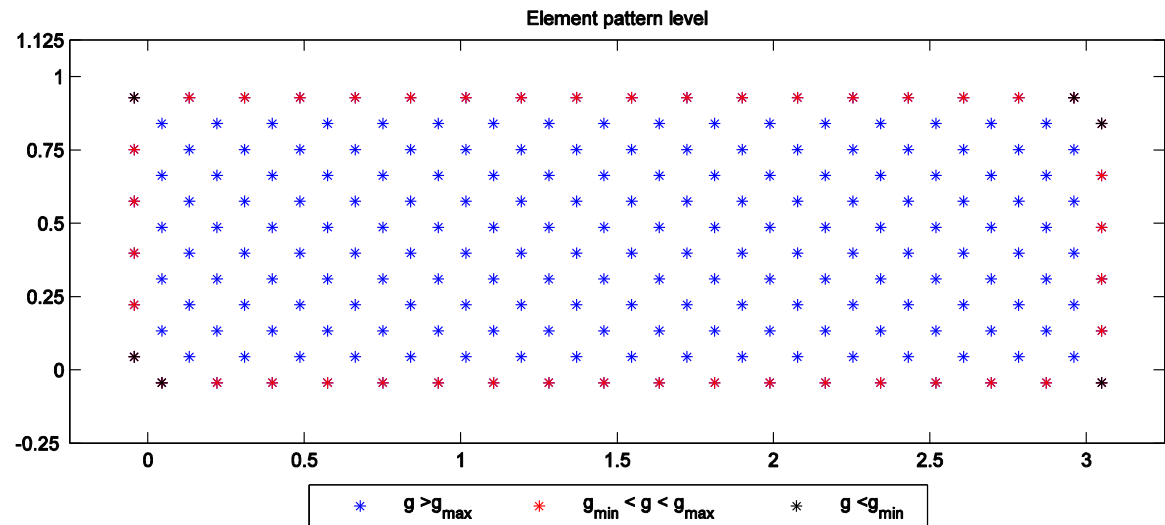
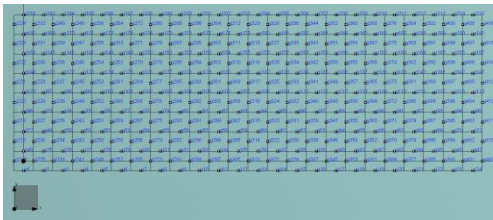
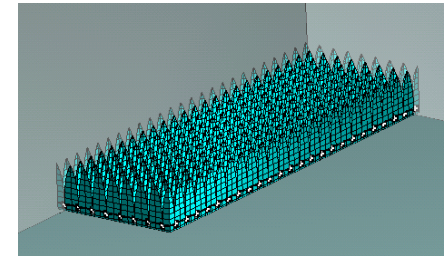
Station configuration

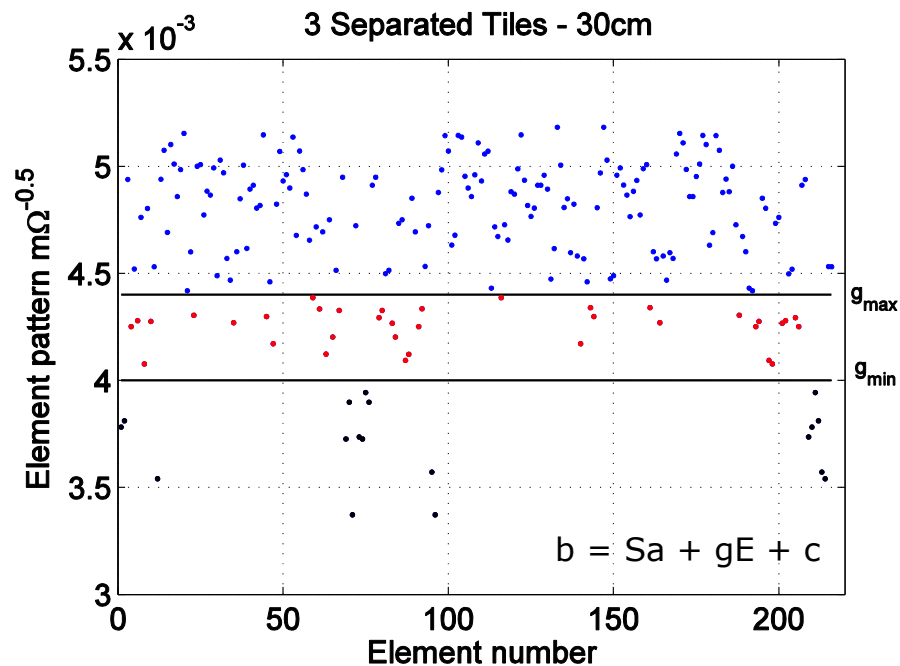


# What is a tile?

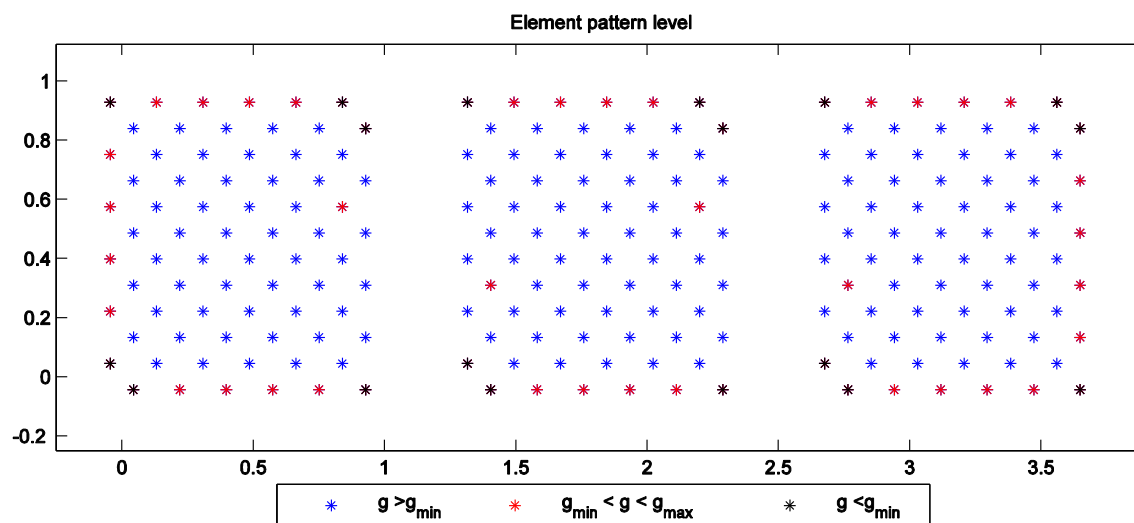
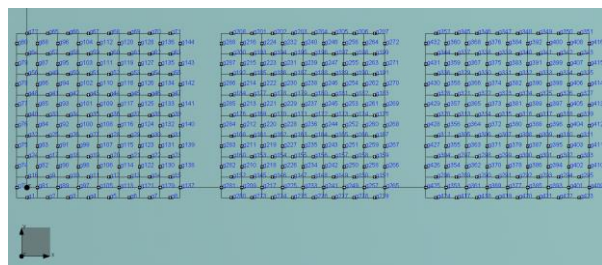
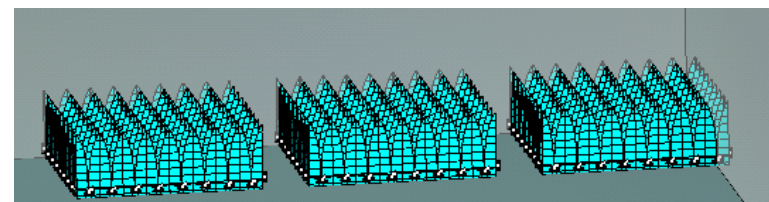


3 connected tiles



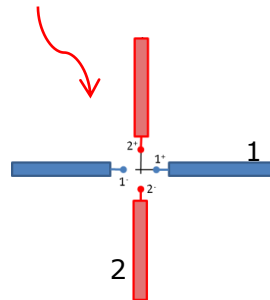


3 separated tiles



## Polarization Discrimination Ratios for Jones Polarimeters

$$\mathbf{E}^{\text{inc}} = E_x \hat{x} + E_y \hat{y}$$



$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} J_{1x} & J_{1y} \\ J_{2x} & J_{2y} \end{bmatrix} \begin{bmatrix} E_x \\ E_y \end{bmatrix}$$

Measured output

Incident field

Transfer function to be inverted

$$XPD_x = \frac{|J_{1x}|^2}{|J_{2x}|^2}$$

$$XPI_1 = \frac{|J_{1x}|^2}{|J_{1y}|^2}$$

- Raw cross-polarization
- Definition dependent on the coordinate system

## A new figure-of-merit for radio polarimeters

*Intrinsic cross-polarization ratio*

$$IXR = \left( \frac{\kappa(\mathbf{J}) + 1}{\kappa(\mathbf{J}) - 1} \right)^2$$

Related to the condition number of the Jones matrix

- Independent of the coordinate system
- Precision achievable inferring the input signal polarization state

$$\mathbf{e} = \mathbf{J}^{-1}\mathbf{f} \quad \frac{\|\Delta\mathbf{e}\|}{\|\mathbf{e}\|} \leq \left( 1 + \frac{2}{\sqrt{IXR}} + \dots \right) \left( \frac{\|\Delta\mathbf{J}\|}{\|\mathbf{J}\|} + \frac{\|\Delta\mathbf{f}\|}{\|\mathbf{f}\|} \right)$$

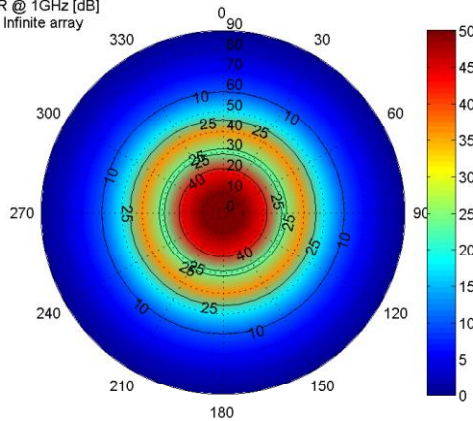
the total relative error of the fully calibrated polarimeter

Better polarimetric design: isolation and channel symmetry

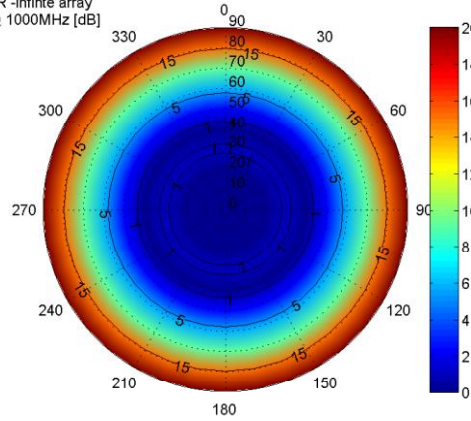


## IXR and Axial Ratio

IXR @ 1GHz [dB]  
Infinite array



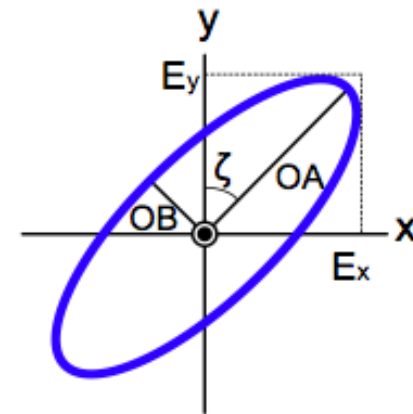
AR -infinite array  
@ 1000MHz [dB]



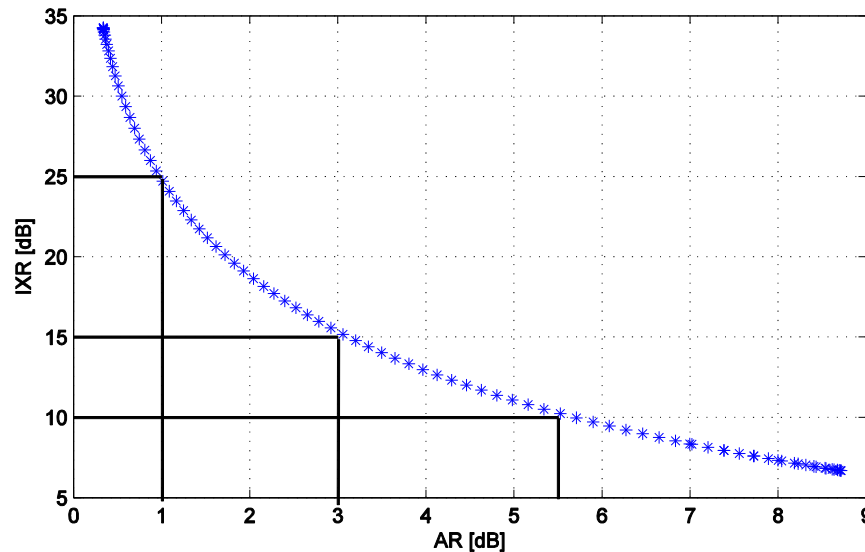
Intrinsic cross-polarization ratio

$$IXR = \left( \frac{\kappa(J) + 1}{\kappa(J) - 1} \right)^2$$

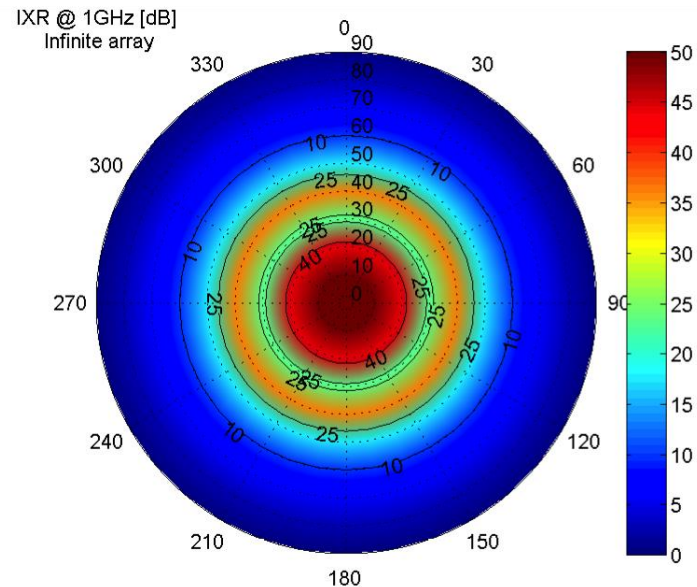
Axial ratio



$$AR = \frac{OA}{OB} = \kappa(J)$$

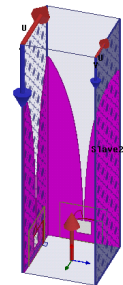


## Infinite Array as reference



### IXR levels:

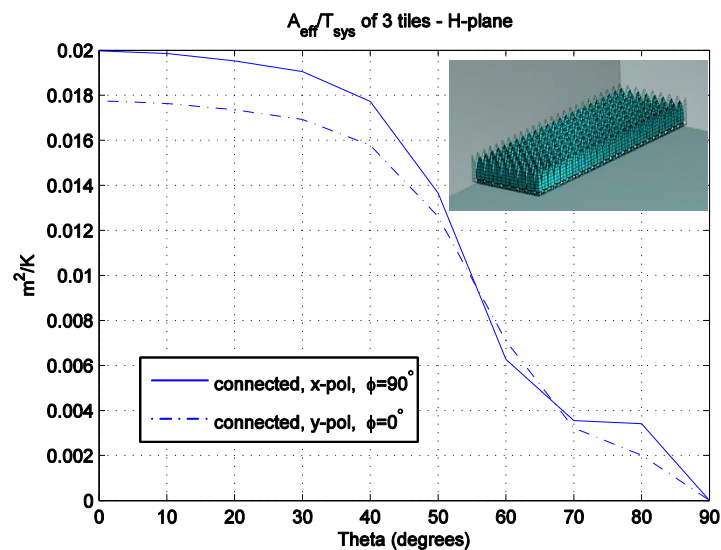
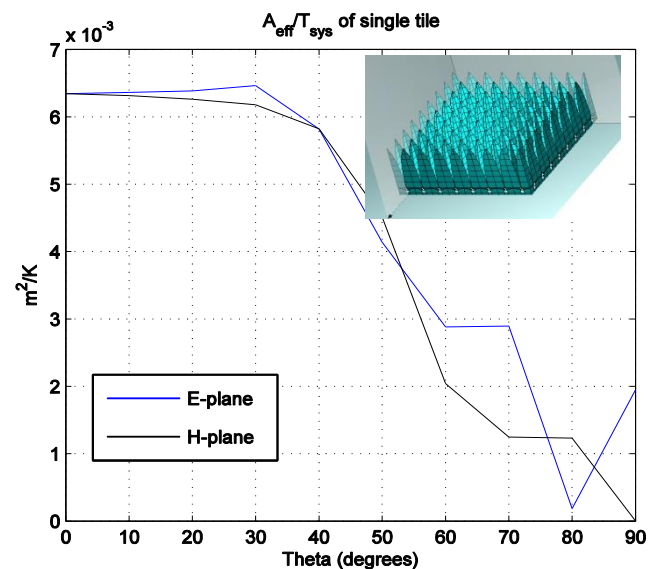
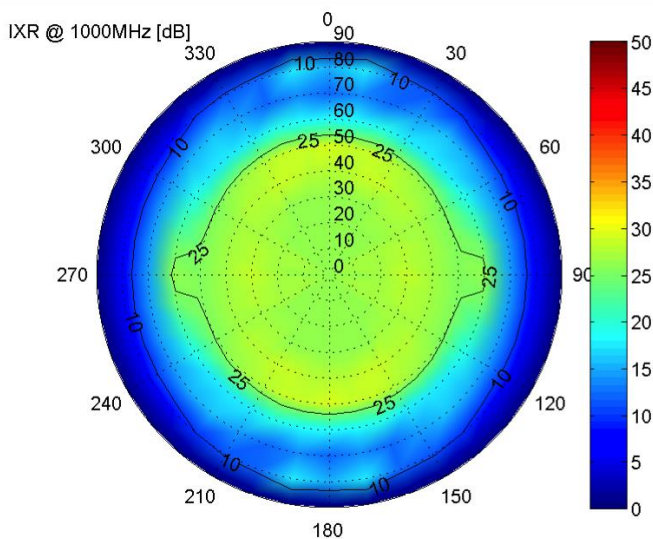
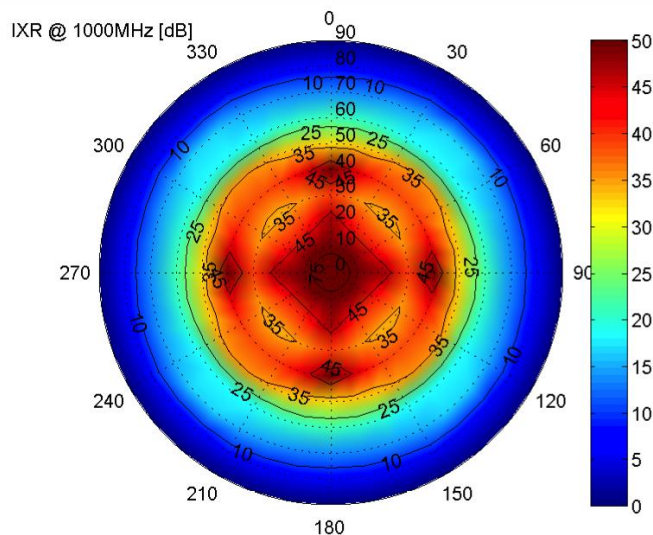
10dB up to 60 degrees,  
25 dB up to 45 degrees,  
40 dB up to 20 degrees.

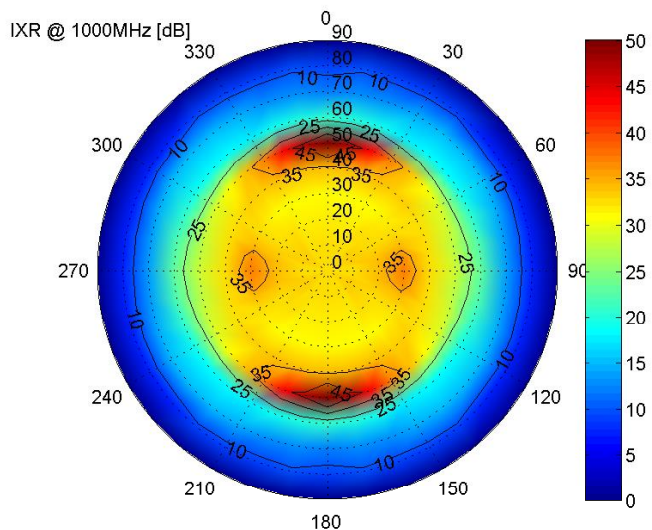


Analysis based on:

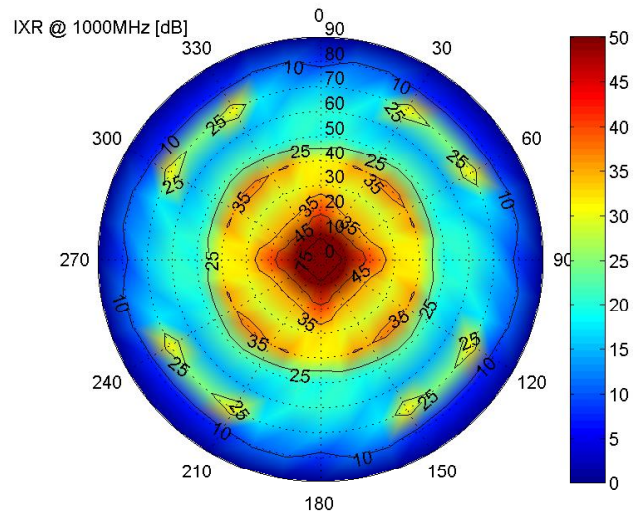
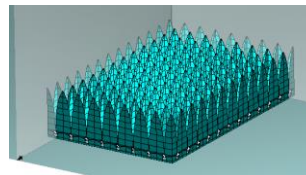
- Polarization,
- Sensitivity.

## 1 to 3 Embrace-like tiles

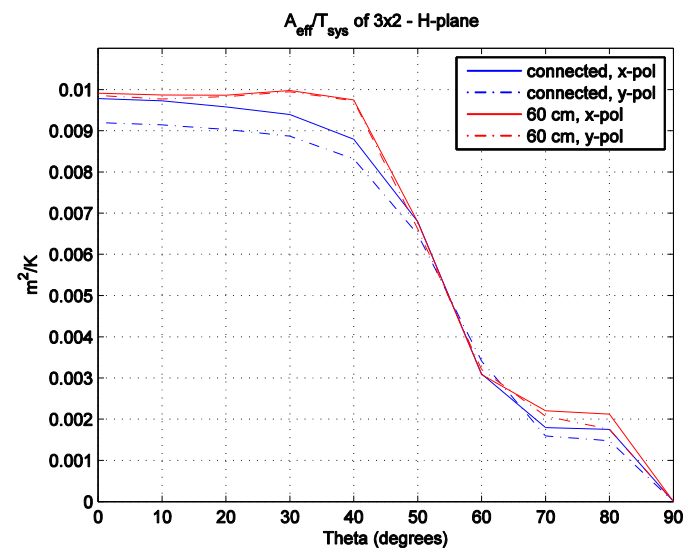
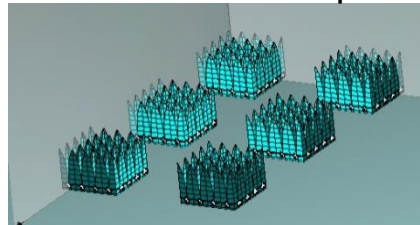




3x2 - No interspacing

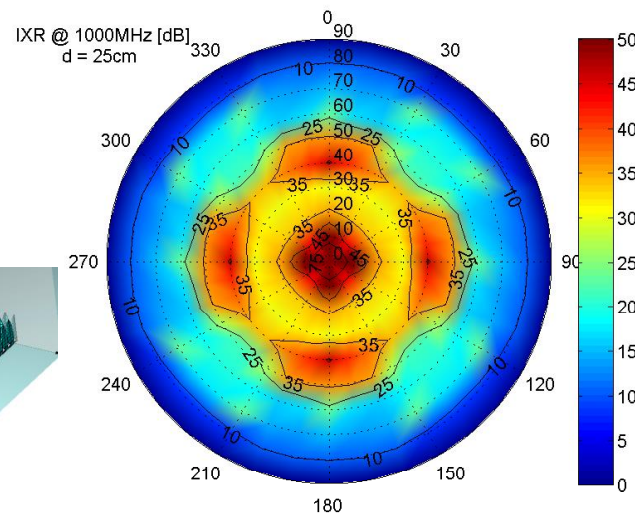
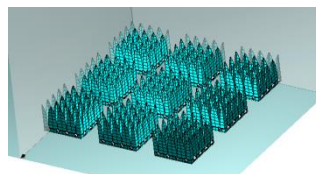
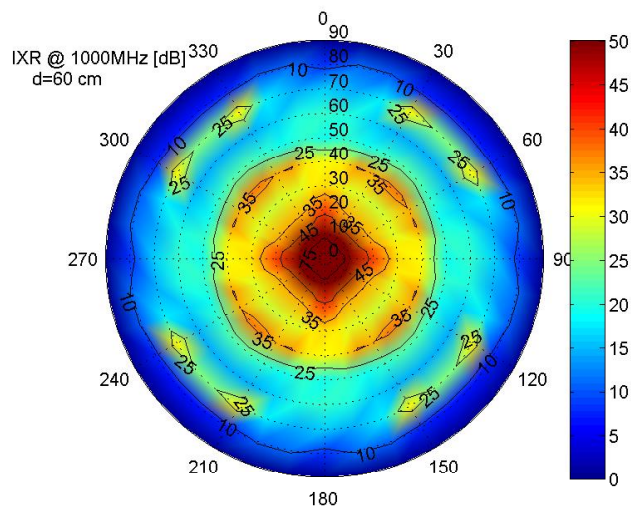
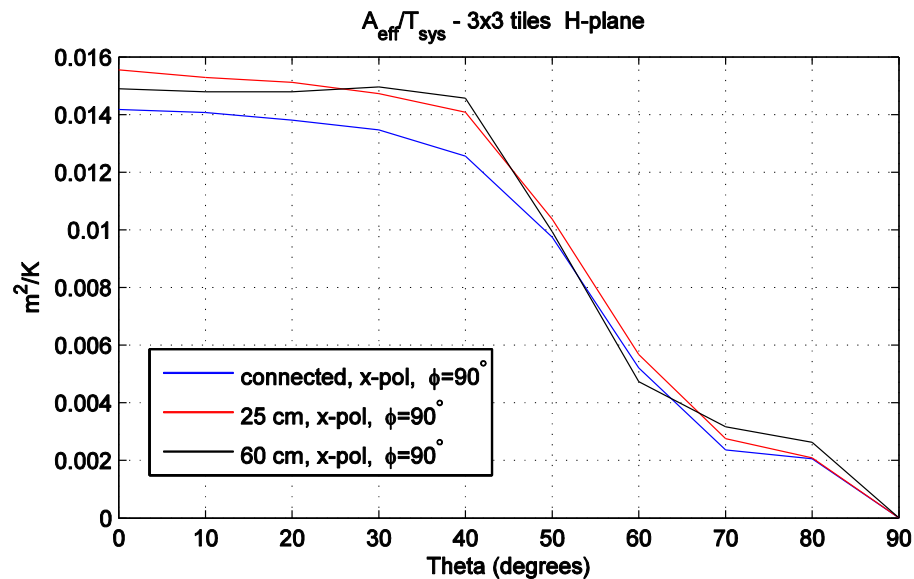
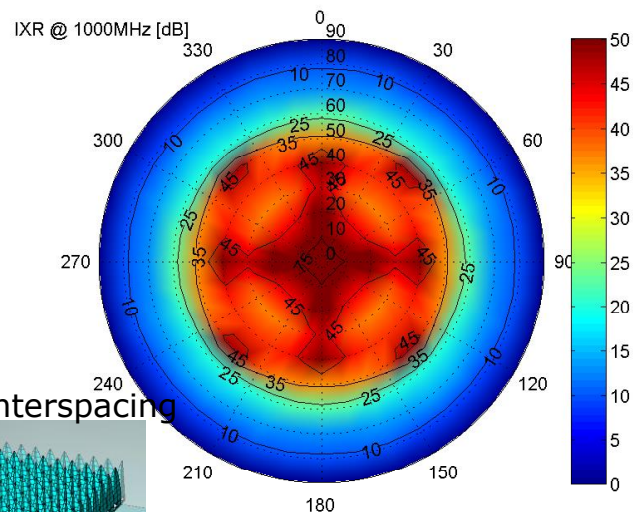


3x2 – 60cm interspacing





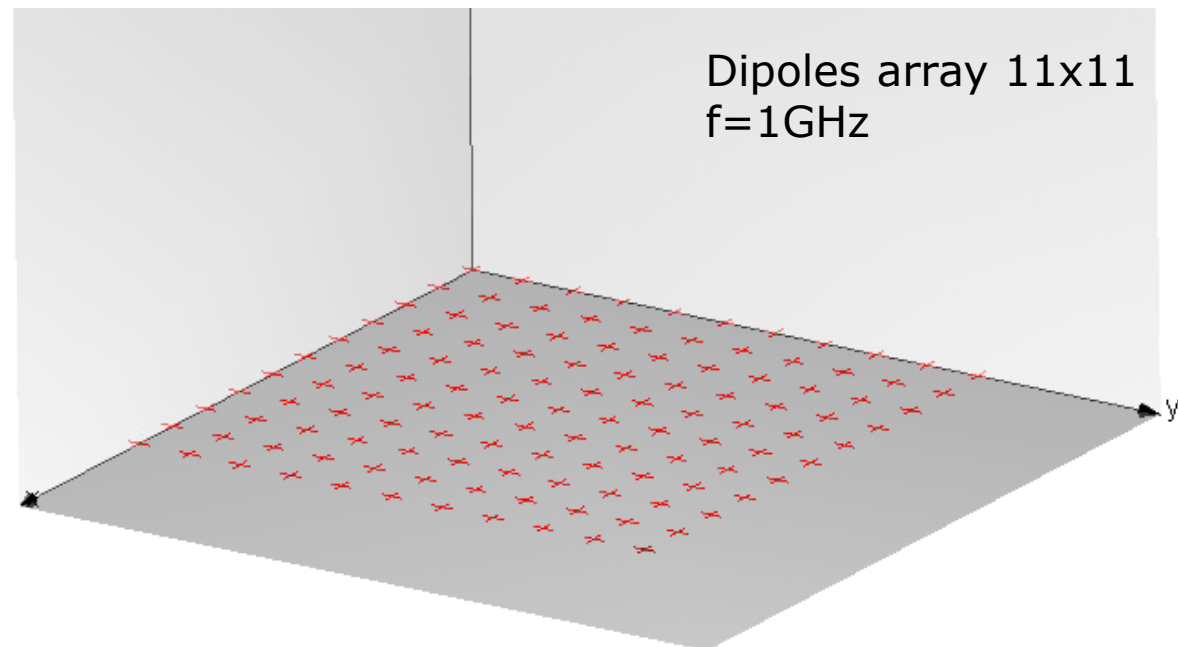
# Tile separation – 3x3



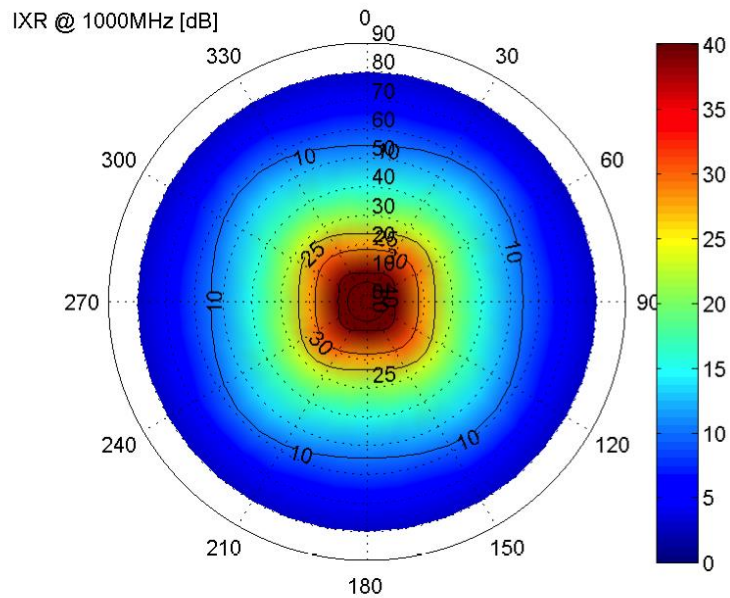


Previous study on array sparseness:  
Which is the level of sparseness allowing the single element analysis?

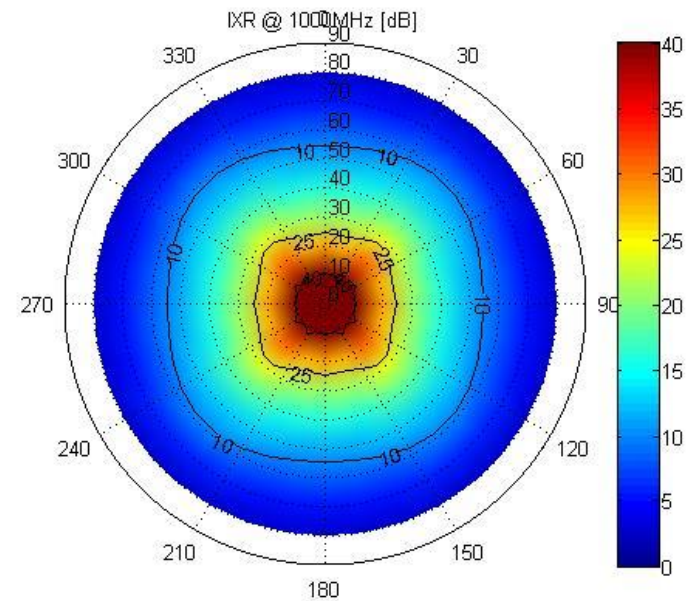
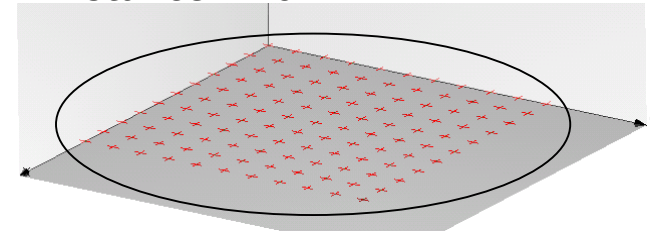
Worse case: regular array



Single element

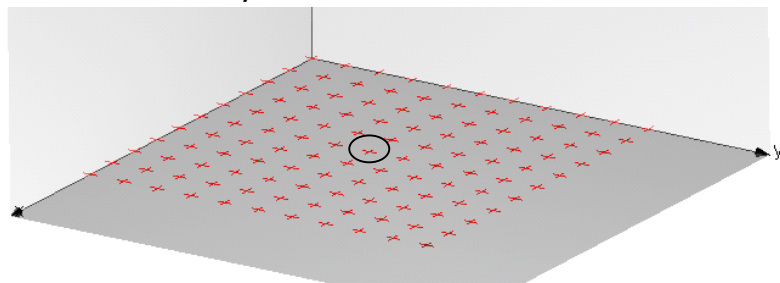


Whole array  
Distance:  $10\lambda$



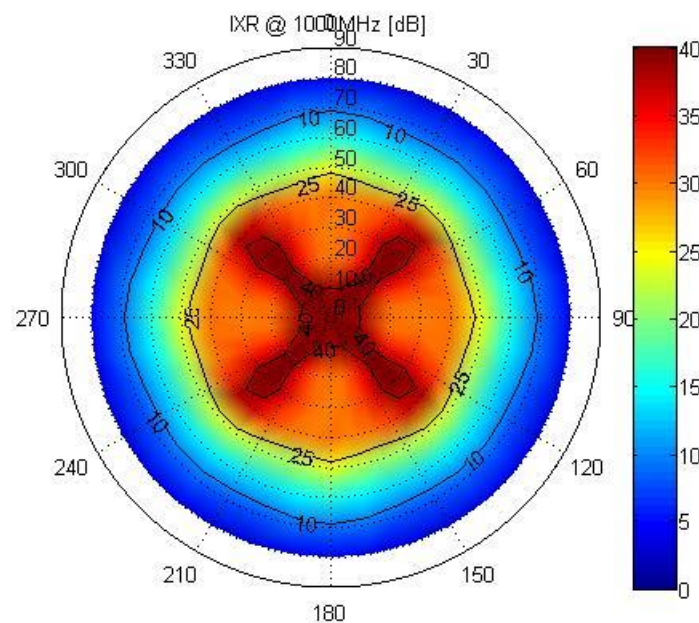
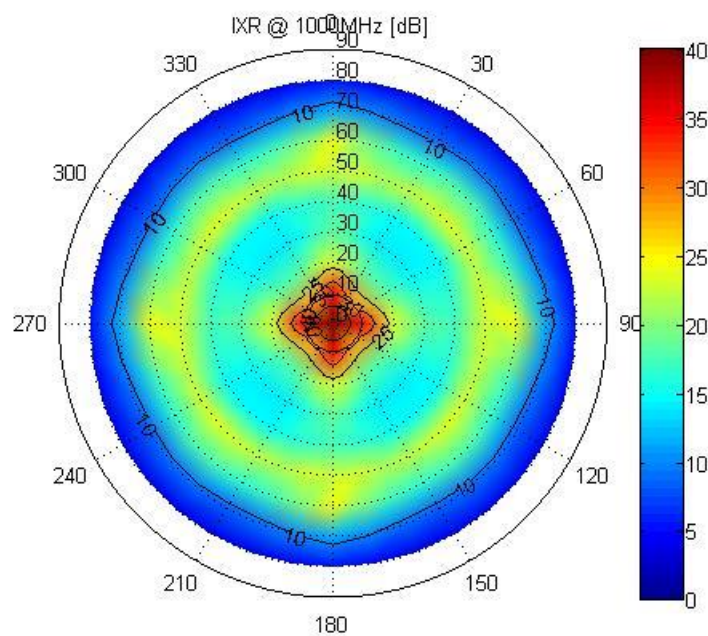
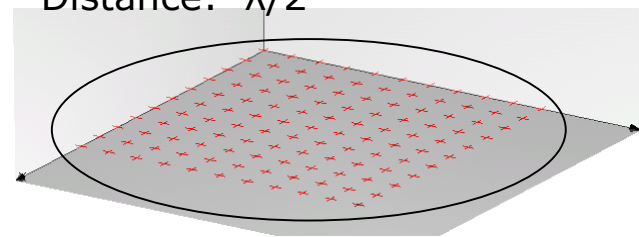
Central embedded element

Distance:  $\lambda/2$

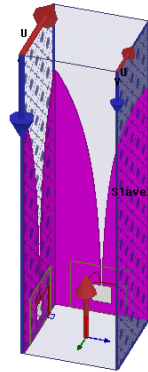


Whole array

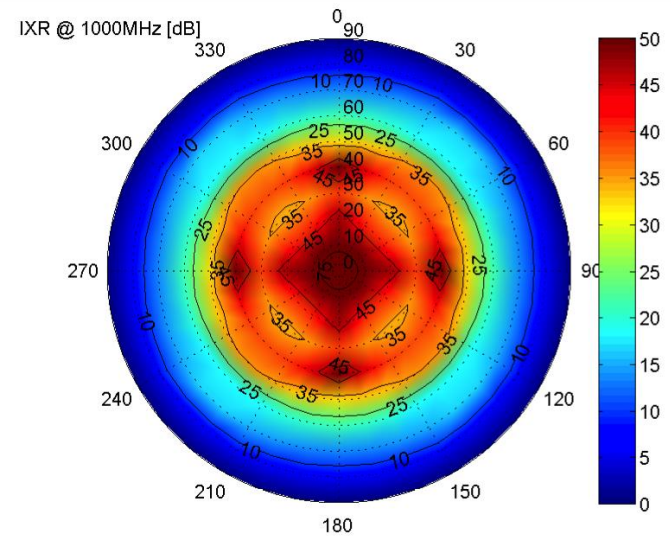
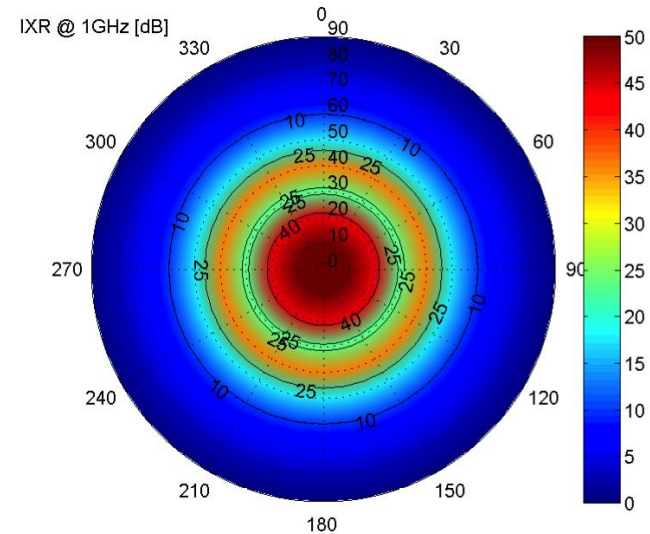
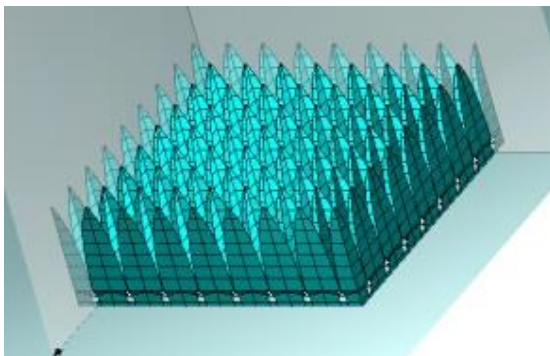
Distance:  $\lambda/2$



Infinite array



144 elements array



## Conclusions

- Asymmetry of the tiles configuration degrades the polarization performances.
- Mutual coupling and finiteness of the array improve the polarization performances at higher scanning angles ( $\Theta > 30^\circ$ ).
- When symmetry is preserved, the improvement is present at every scanning angle, including the region close to zenith.
- Tiles separation doesn't degrade the polarization performances and sensitivity of the finite array (up to  $2\lambda$ ).

## Future work

- Study: Tile sizing, Tile separation sizing, Station configuration.
- Further studies are required to evaluate the reliability of the infinite array approximation as function of the array size.



Thank you.