



Lectures on radio astronomy: 3

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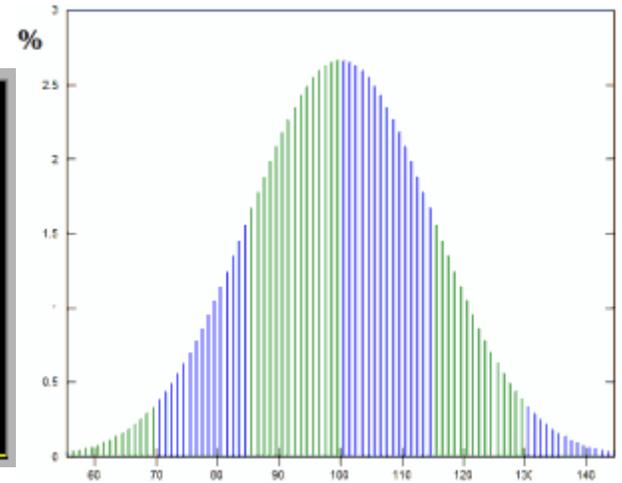
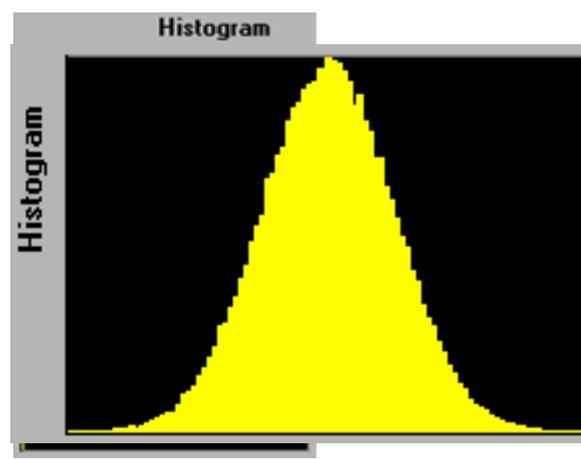
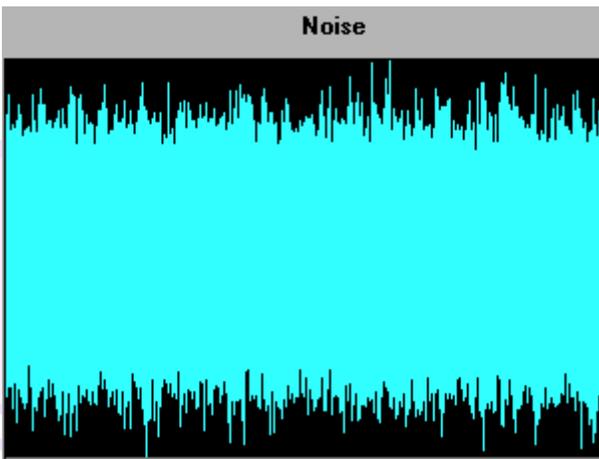
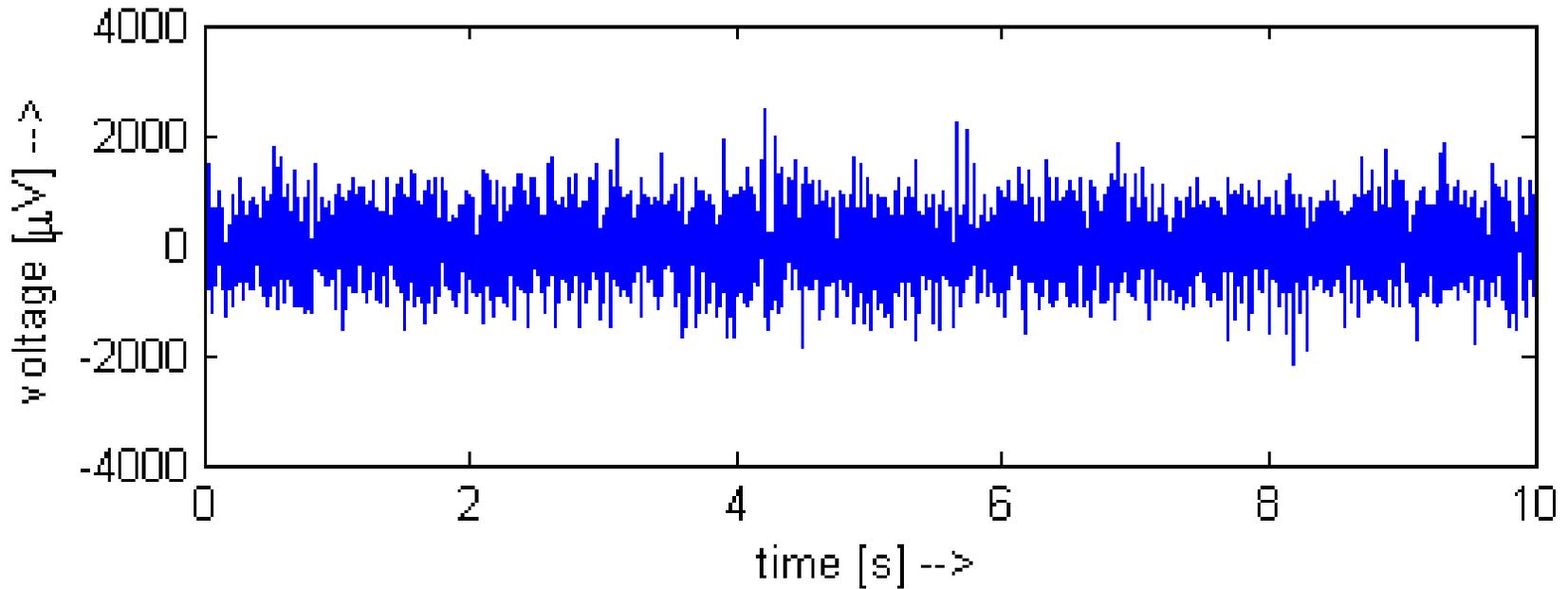
Receivers & noise

Signal we want (from sky) has unfortunate properties:

- Its statistical characteristics are just those of noise, indistinguishable from other background noise (from the ground, atmosphere, receiver, etc.)
 - It is usually much weaker than other sources (ground, receiver, etc.)
- ➔ Detecting it requires top technology, and a lot of clever tricks also

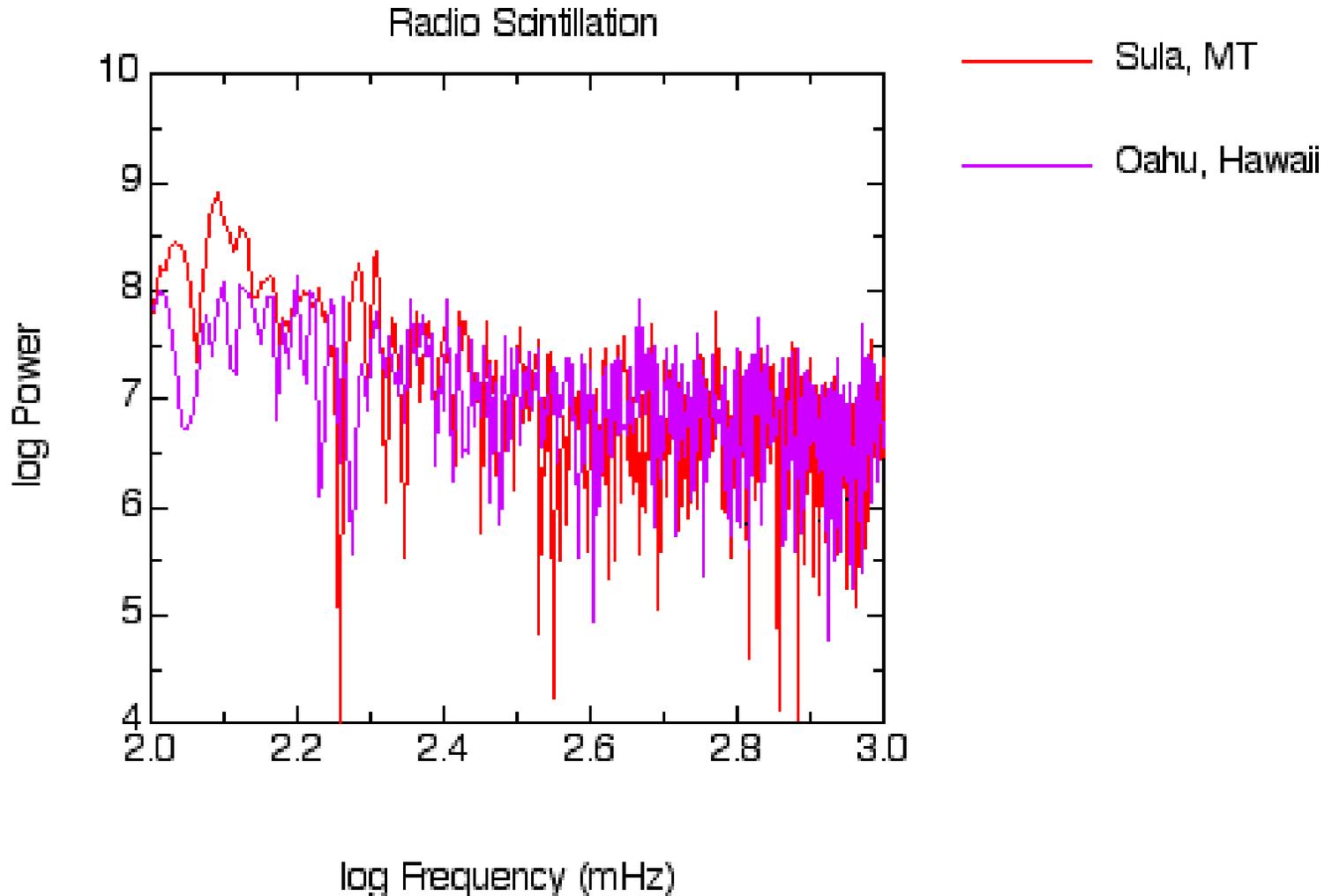
An example of noise

Noise



Noise from solar pulse (spectrum)

Log-Log Power Spectra Solar Pulse March 26, 2002 20:23Z



Telescope receiver system: essential elements –

- Sensitivity
- Tunable frequency
- Total (instantaneous) bandwidth
- Frequency channels/resolution
- Stability of output signal
- Dynamic range

Also useful are simplicity, ease of operation & maintenance, flexibility

Receiver sensitivity issues

- Choose low-noise components – nowadays often FET/HEMTs; can be cooled (even to <4 K) for less thermal noise
- Minimize effect of lossy components (cables, connectors, atmosphere, filters): loss of -0.1 dB ($= 2.3\%$, or factor 0.977) will add $2.3\% \times 290$ K $= 7$ K to system noise. So, short cables, cooled filters, etc. before amplifier

Troposphere significant for $\lambda < 10$ cm; solutions?

- Get above troposphere (mm telescopes are on mountains); go into space?
- Observe at high elevation. Atmospheric effect depends on thickness. Looking at zenith angle z ($z=0^\circ$ is straight up) increases thickness (and effect) by $\sec z$
- Observe from dry site – effect is mainly due to water vapor in troposphere
- Observe short λ when weather's good

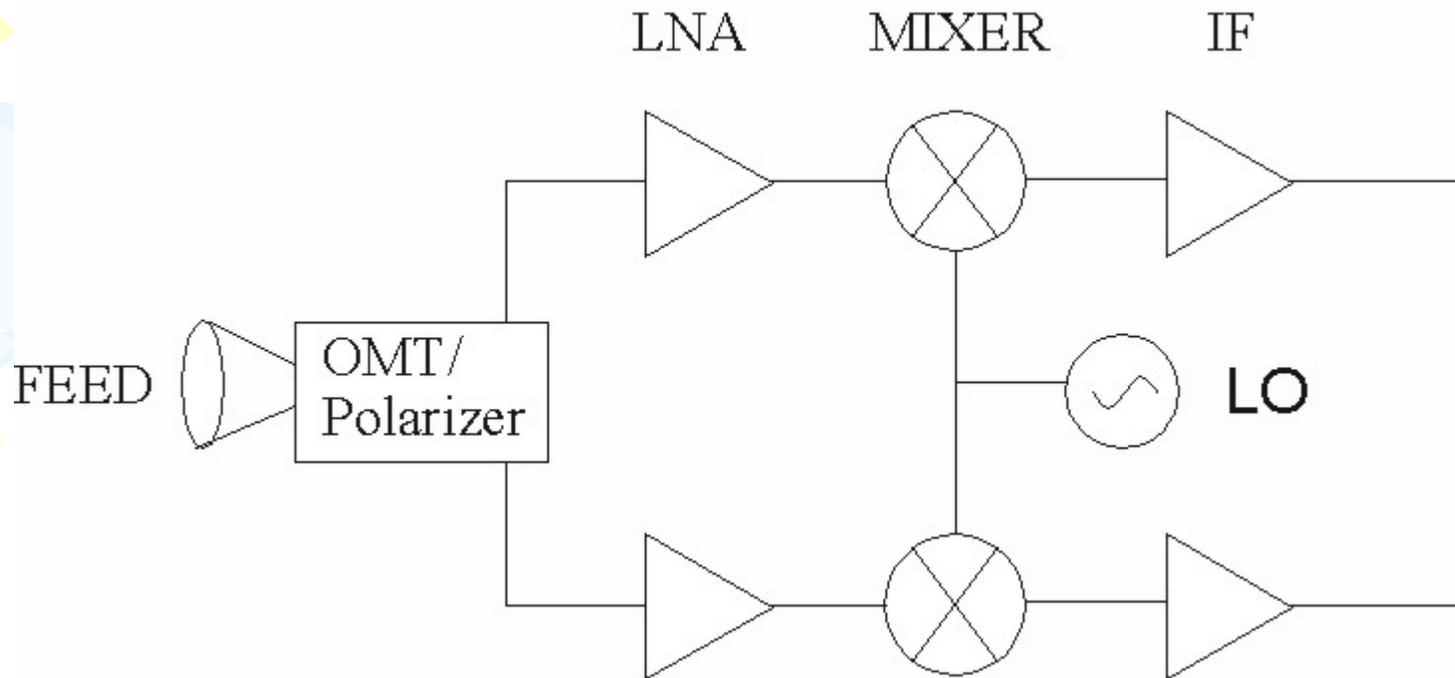
Telescopes like 15 m SEST:
high (2500 m) and dry site



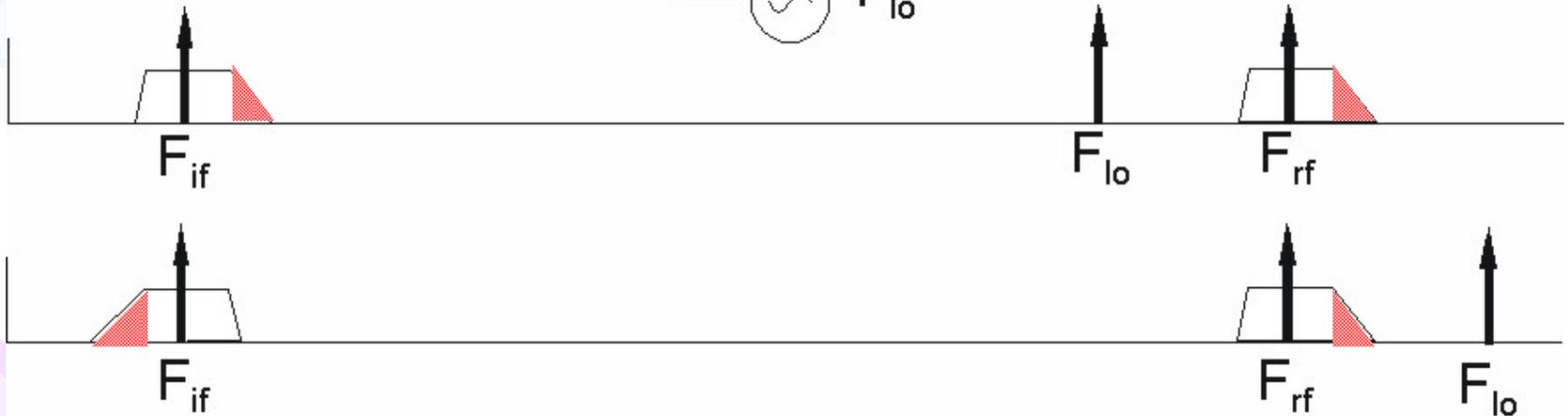
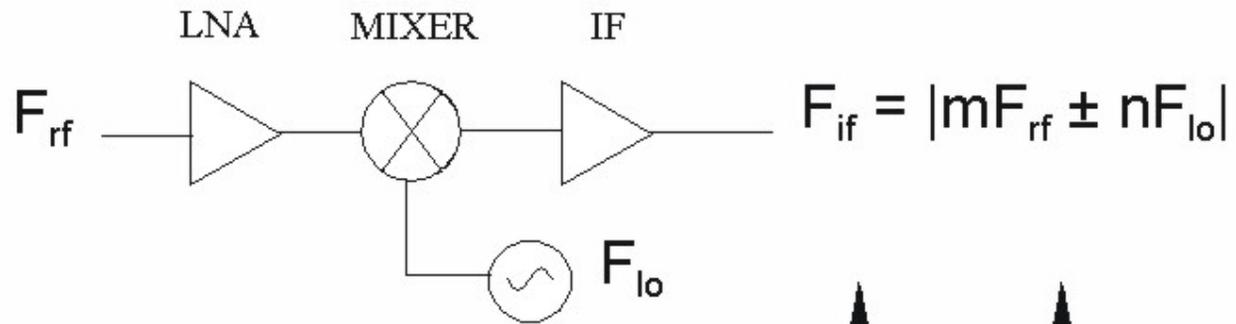
Frequency requirements of radio astronomy receivers

- Should be able to (quickly) tune to any frequency band
- Within that band, may want to have many channels over some range (line observations)
- For continuum, maximum possible bandwidth gives greatest sensitivity (includes more signal)

Structure of a typical superheterodyne receiver



Mixer used for frequency conversion of signal: $F_{rf} \Rightarrow F_{if}$



Mathematics of the super-heterodyne system

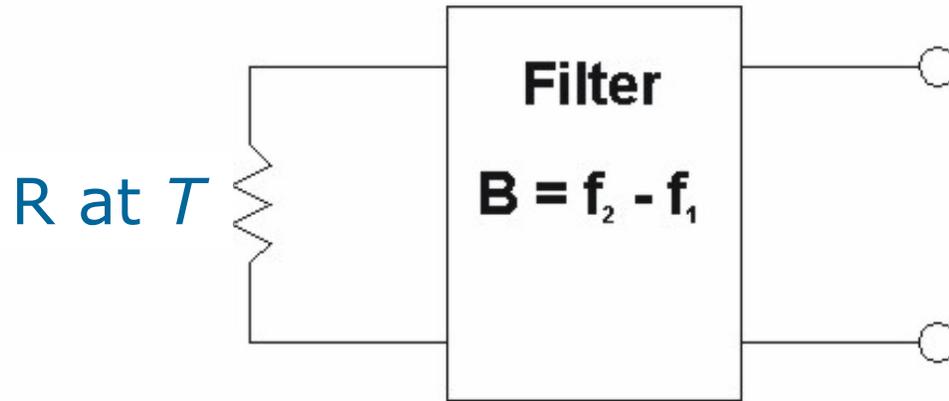
- Basic idea is to multiply together signals of two different frequencies
- From the trigonometric identity:
 $\sin f_1 \sin f_2 = \frac{1}{2} \cos(f_1 - f_2) - \frac{1}{2} \cos(f_1 + f_2)$
- The result of multiplying 2 sinusoidal signals together is signals at the sum and difference frequencies; the latter gives us an intermediate frequency:

$$f_{IF} = |f_{\text{sky}} - f_{LO}|$$

Features of the super-heterodyne system

- A local oscillator (LO) signal is mixed with sky signal: converts sky to intermediate frequency (f_{IF})
- In general, 2 sky frequencies (upper and lower sidebands) are produced; may not be desirable, so filter one out if not wanted
- The same IF system can be used for different antenna signals

Power in noise signal: thermal voltage fluctuations

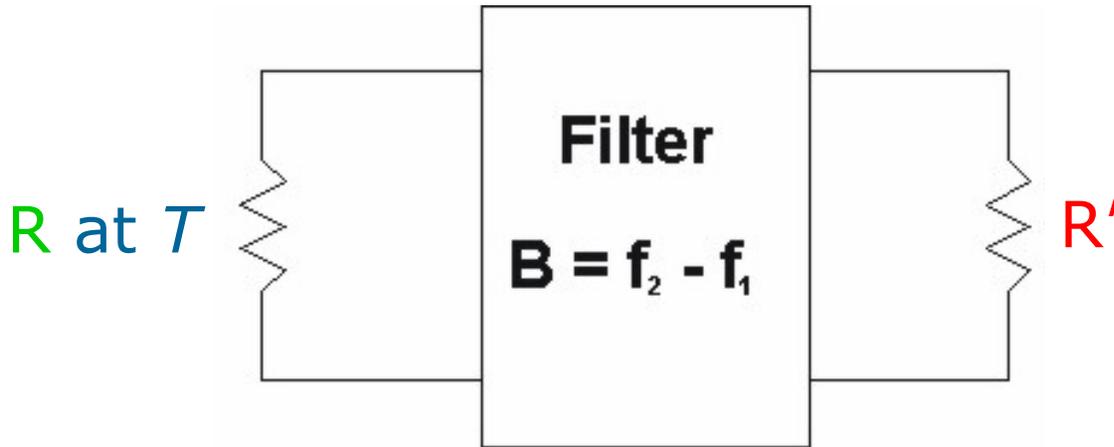


- After filtering, voltage at right-hand output can be written:

$$V_{\text{rms}}^2 = 4kTR \int x / (e^x - 1) df \quad ; \quad x = hf/kT$$

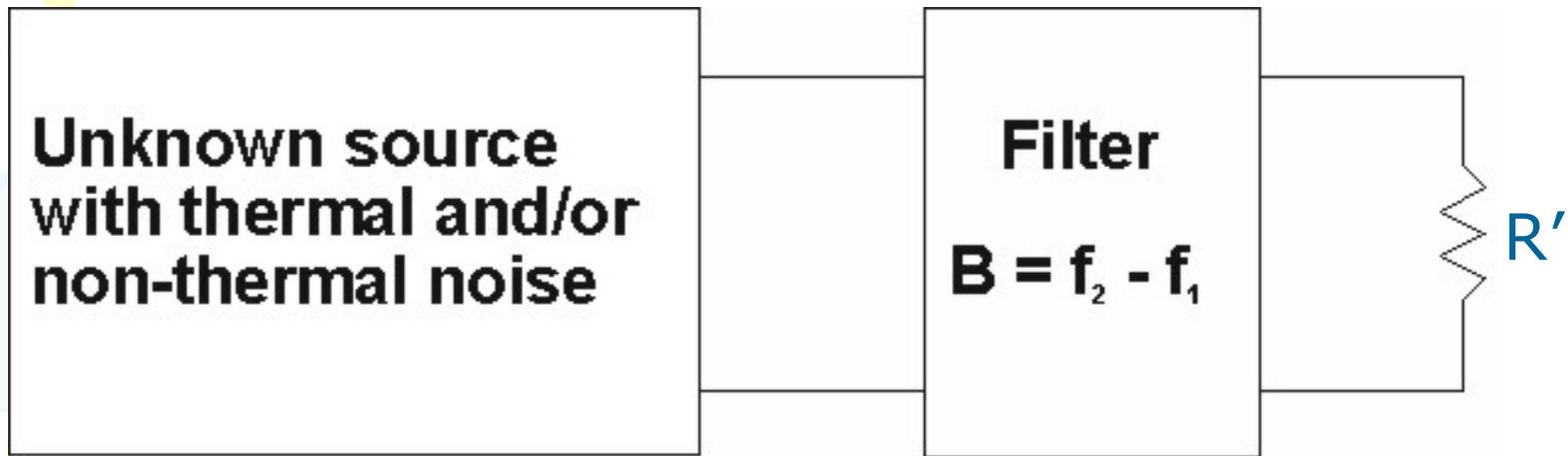
- For $x \ll 1$, $V_{\text{rms}}^2 = 4kTR (f_2 - f_1)$

Available noise power



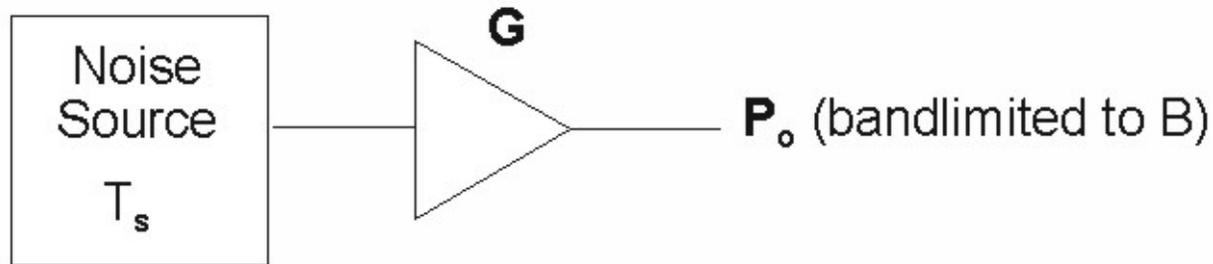
- The signal from resistor R , at temperature T , is filtered and limited to a bandwidth, B ($= f_2 - f_1$)
- The resulting signal in resistor R' has a power, $P_n = BkT$

In a similar way, we can determine equivalent noise



- In a similar setup, we filter the signal from an unknown source
- From the power in resistor R' , we can calculate: $T_s = P_n/kB$

What is the equivalent noise of the amplifier?



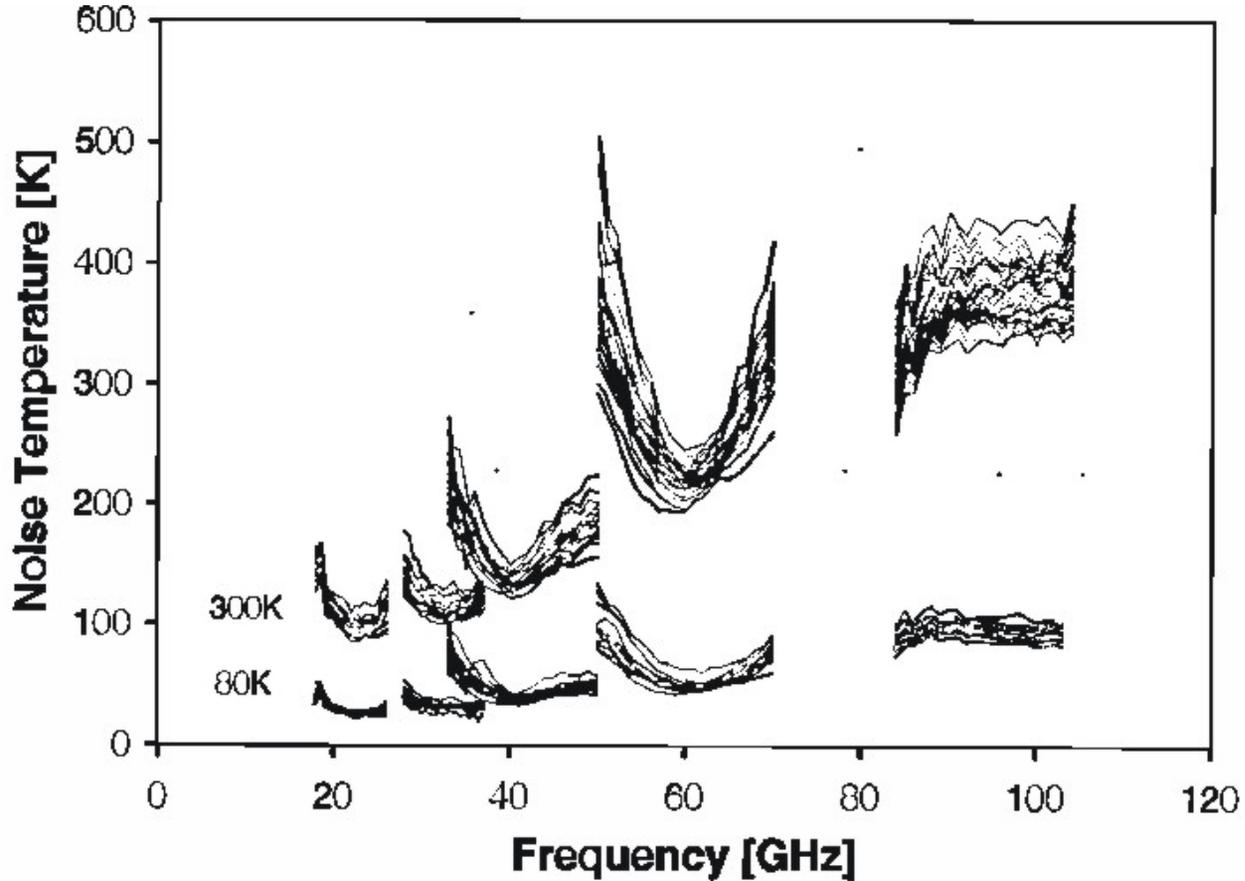
$$P_o = GkBT_s + K$$

Define $K = GkBT_e$

$$\text{Then, } P_o = GkB(T_s + T_e)$$

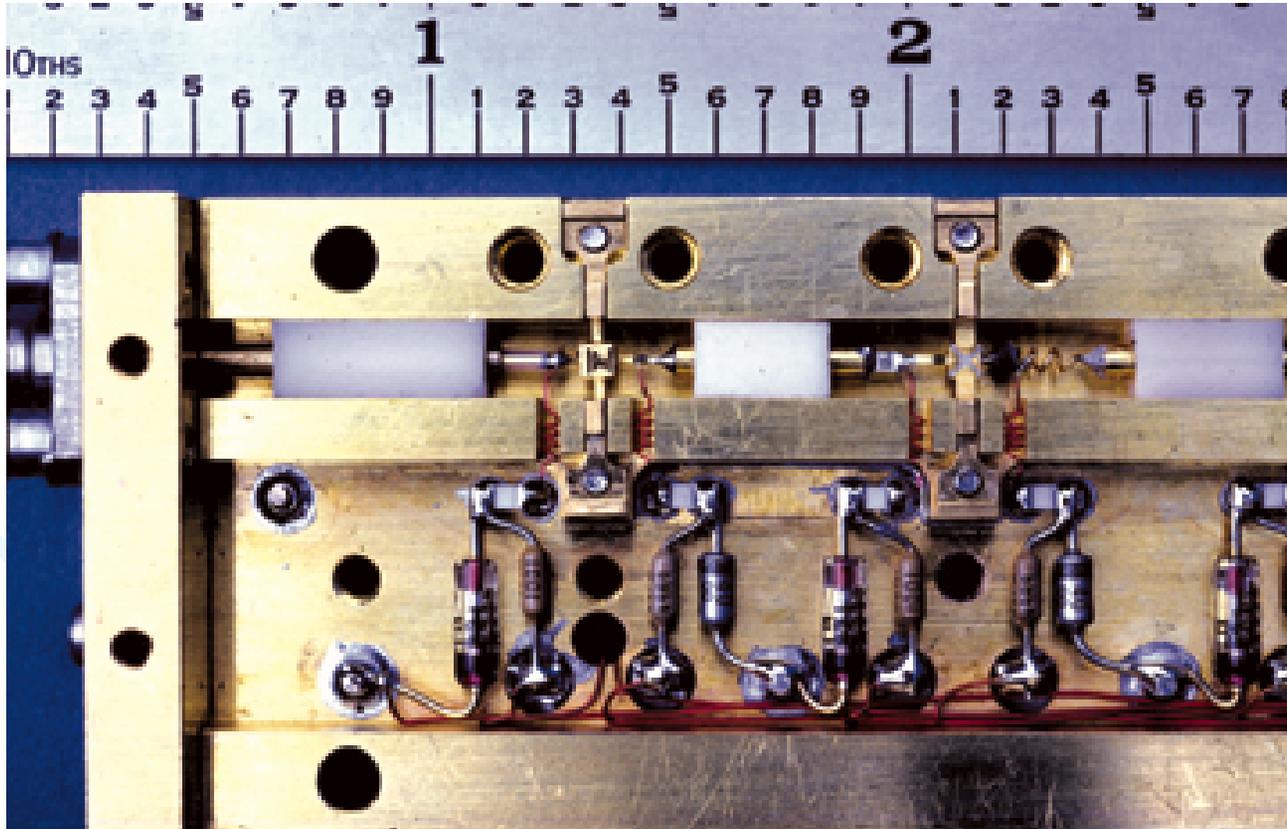
T_e is the amplifier *Equivalent Input Noise Temperature*

HFET noise temperature

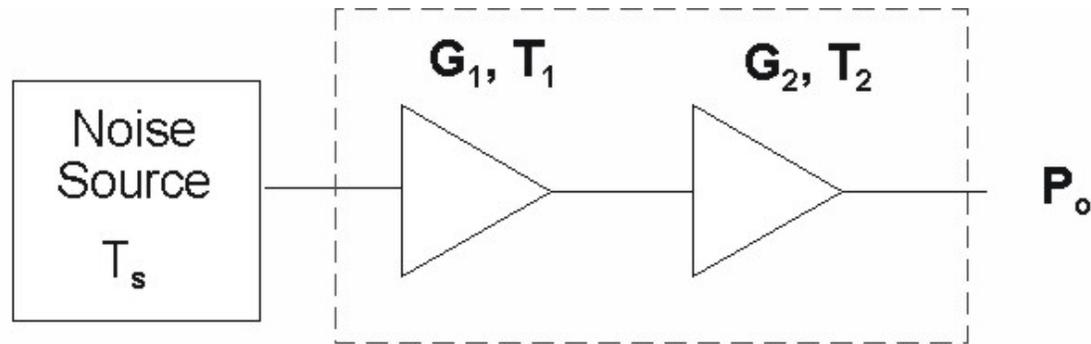


Data courtesy M. Pospieszalski of NRAO Central Development Laboratory

HFET (HEMT) Low Noise Amplifier (LNA)



What is the noise contribution of amplifiers in series?



$$P_o = G_1 G_2 k B T_s + G_1 G_2 k B T_1 + G_2 k B T_2$$

or,

$$P_o = G_1 G_2 k B (T_s + (T_1 + T_2 / G_1))$$

So, Amplifier Cascade has equivalent noise $T_1 + T_2 / G_1$

Example of receiver temperature calculation

Receiver system, 3 amplifiers: 1, 2 & 3

- $T_1 = 50 \text{ K}$, $G_1 = 20 \text{ dB}$ ($= 100\times$)

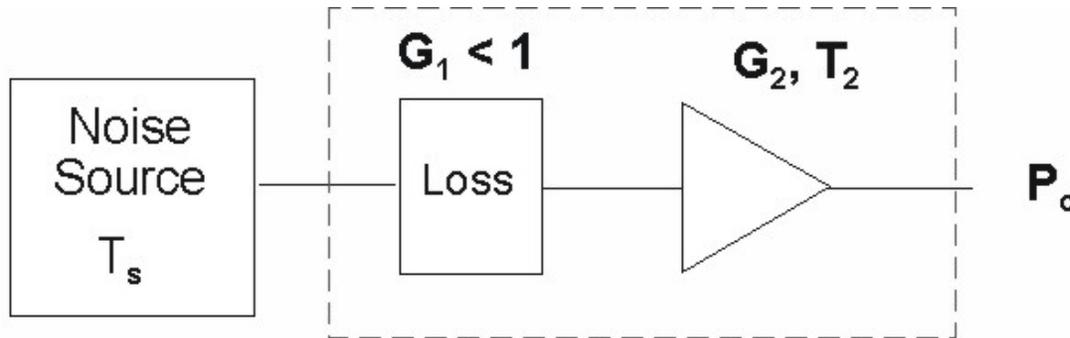
- $T_2 = 300 \text{ K}$, $G_2 = 10 \text{ dB}$ ($= 10\times$)

- $T_3 = 500 \text{ K}$

$$T_N = 50 \text{ K} + 300 \text{ K}/100 + 500 \text{ K}/(10\times 100)$$
$$= 50 \text{ K} + 3 \text{ K} + 0.5 \text{ K} = 53.5 \text{ K}$$

So we see, 1st amplifier has greatest effect.

Noise contribution of input loss



Let $L = 1/G_1$, then for ohmic loss at physical temperature T_o , the effective noise temperature of the loss is $(L-1)T_o$.

Effective noise temperature of the loss - amplifier cascade

is: $(L-1)T_o + LT_2$.

The lesson, when designing a receiver, is...

- Put a low noise amplifier (LNA) with high gain ($G \geq 20$ dB) at front
- Avoid any losses before the LNA (so, keep cables short, or use waveguide; avoid filters if possible, or cool them; keep atmospheric loss low – choose a good site)
- Noise from lossy element after LNA gets divided by LNA gain (G_1)

Final noise determined by T_N , bandwidth, duration

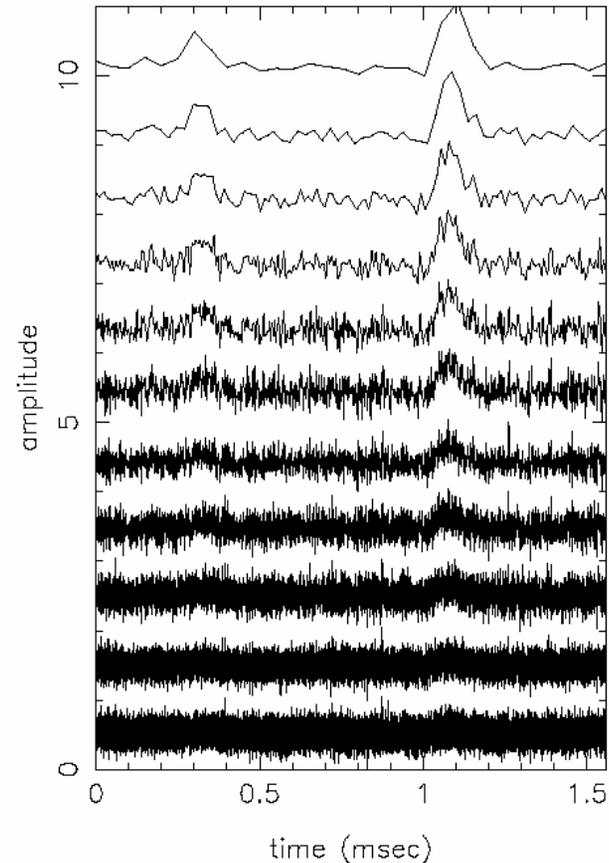
$$\sigma = \frac{T_N}{\sqrt{\Delta f \times \tau}}, \text{ where } \Delta f \text{ is bandwidth,}$$

and τ is integration time

σ is the final (rms) noise, to be compared with source signal strength

Here is an example of time integration in practice

- Observation of pulse from ms pulsar PSR1937+21
- Integration time increases by $2\times$ each step from bottom
- See pulse better, lose some detail
- [frequency smoothing gives similar result]

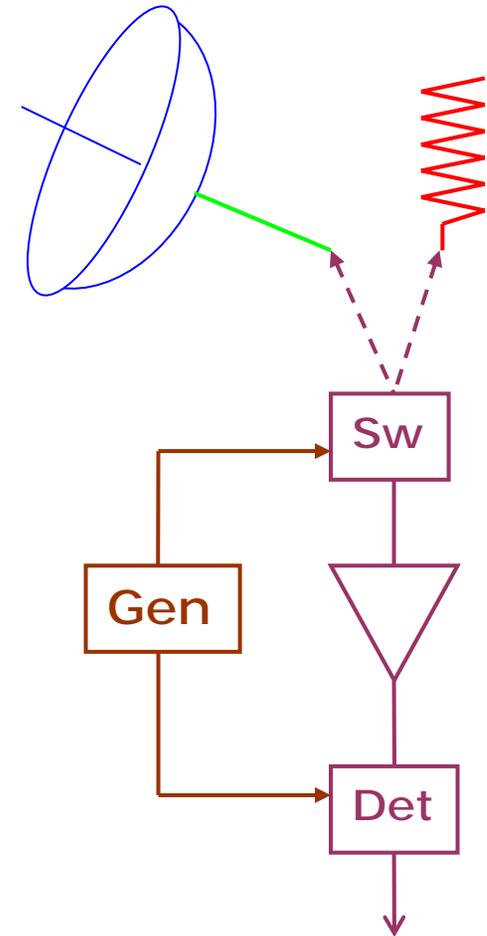


Having sensitivity is useless if stability is poor

- Amplifiers with high gain tend to be less stable
- To keep output stable, often add feedback loop: automatic gain control (AGC)
- Physicist Robert Dicke invented technique: switch to reference noise source, to monitor receiver.

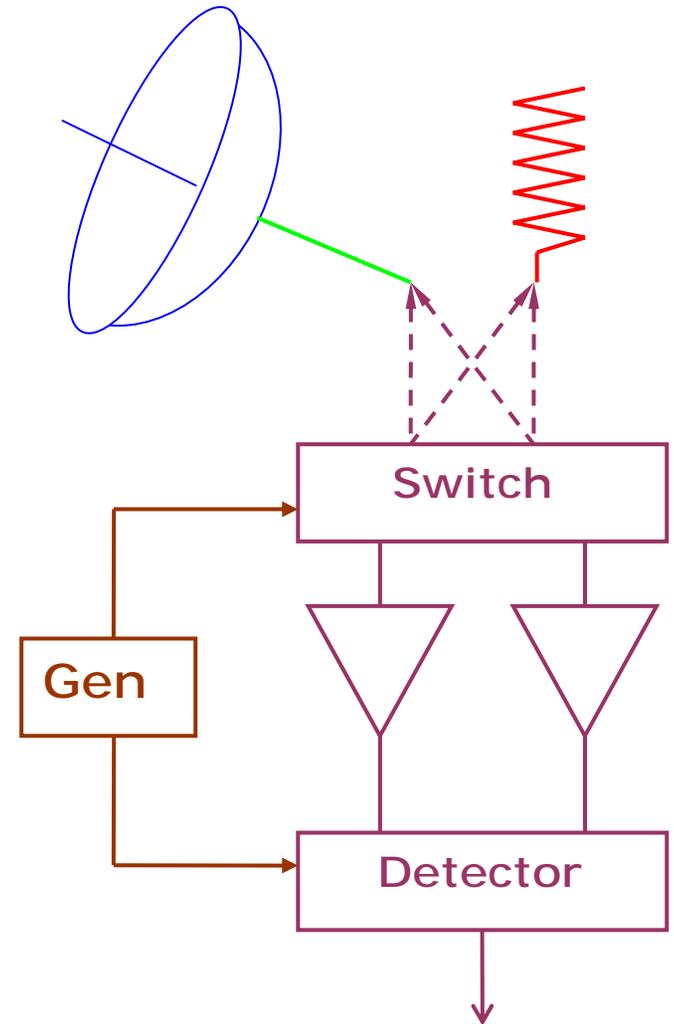
Example of a simple Dicke switch radio telescope

- Generate switching frequency, faster than system drift
- Demodulate at same frequency after detection
- Disadvantage is not all time spent on source: lose some observing time



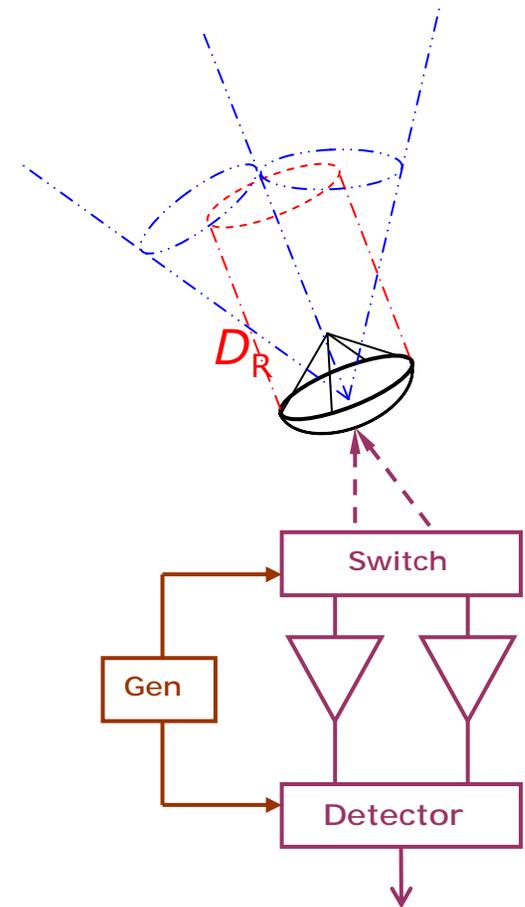
Avoid loss of observing time with two receivers

- Always observing sky and reference
- At end, average two difference signals
- Always need stable reference
- This system costs more (2 channels)

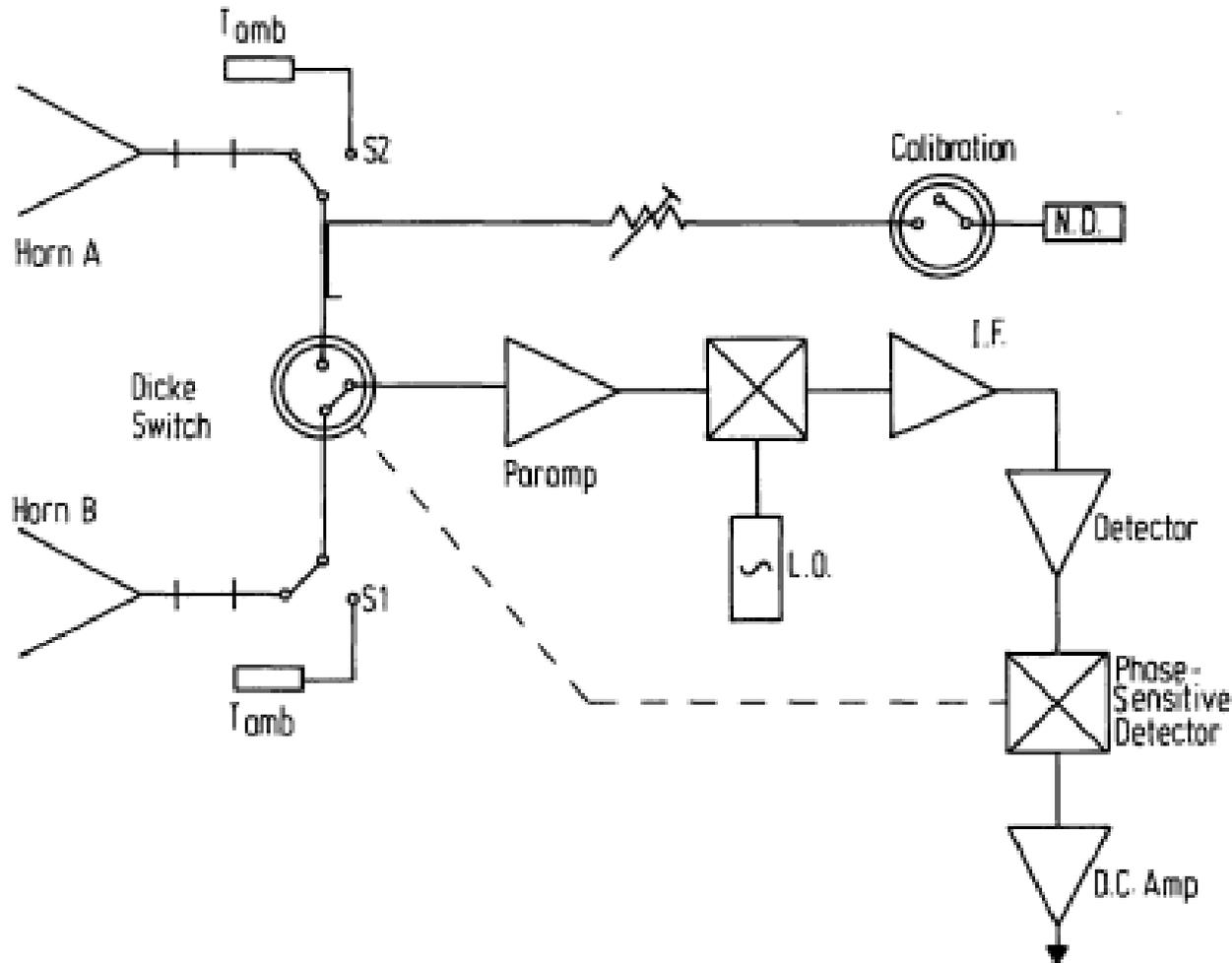


Dicke's technique widely used, in different ways

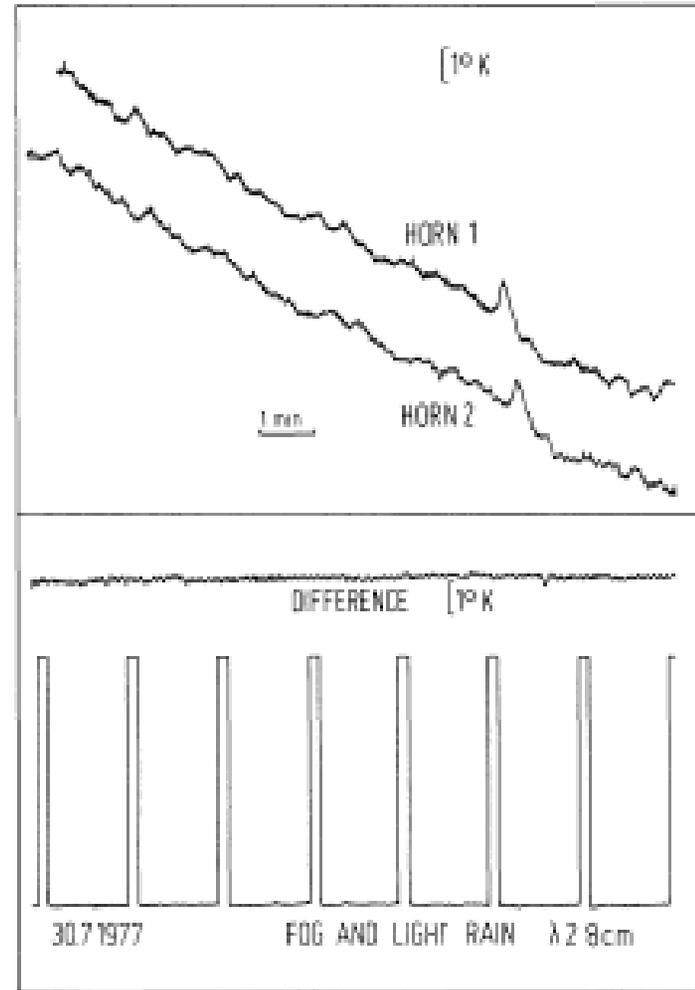
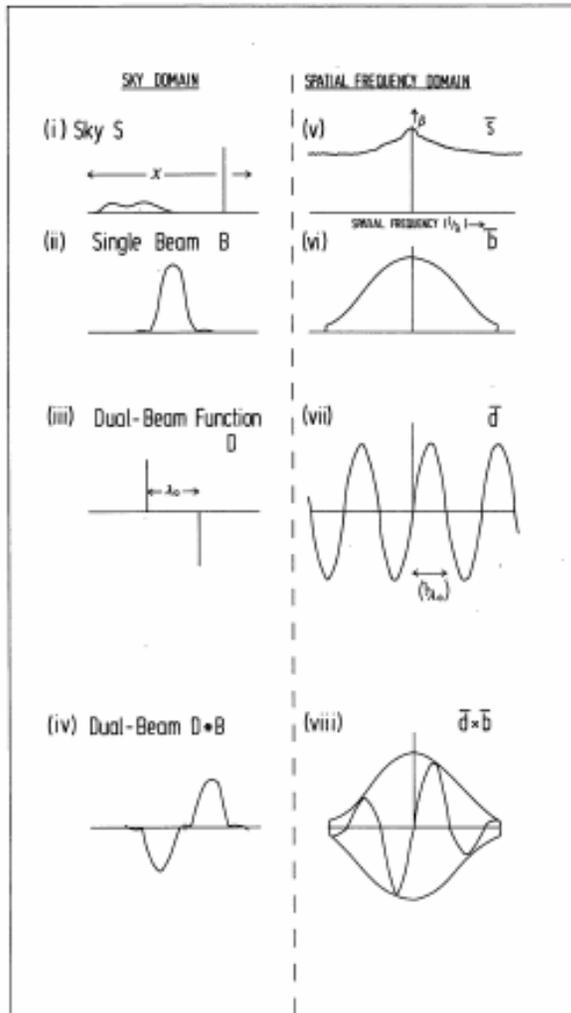
- For example, with two receivers, we can make two beams
- We can point one beam at source, other on empty sky.
- Using Dicke's switch, one beam becomes reference – can “switch out” effect of atmosphere.



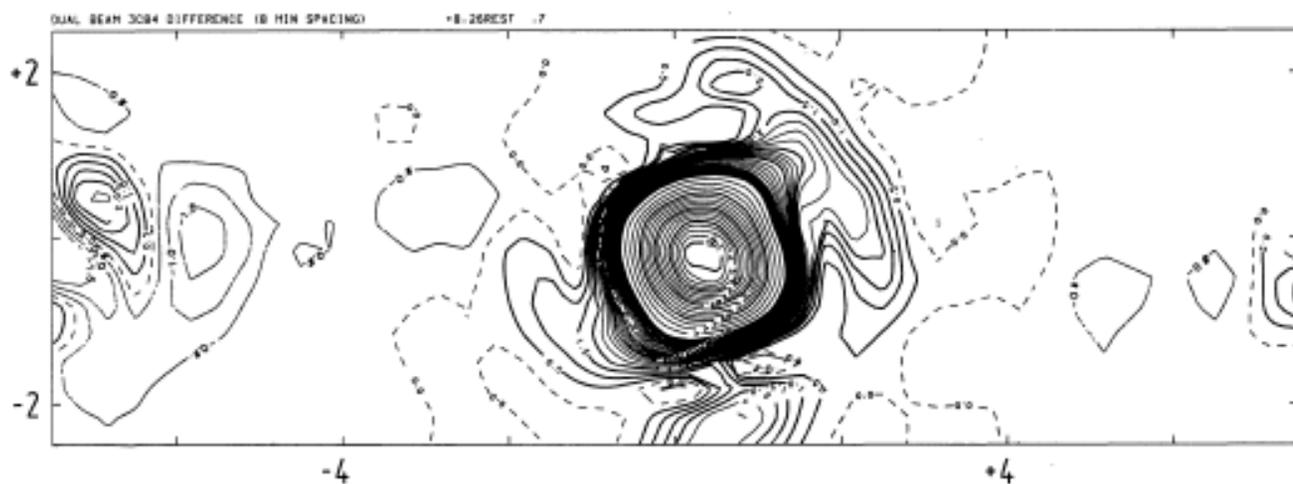
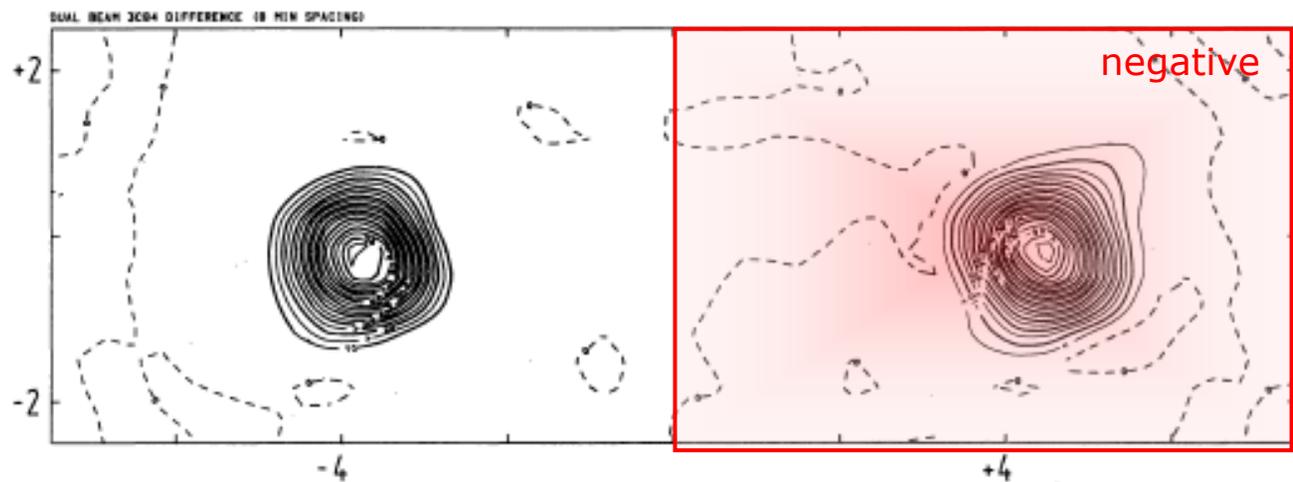
Effelsberg $\lambda 2.8$ cm system (Emerson et al., 1979)



What dual-beam measures & example of data (in fog)



Observation of strong source 3C84: data & result

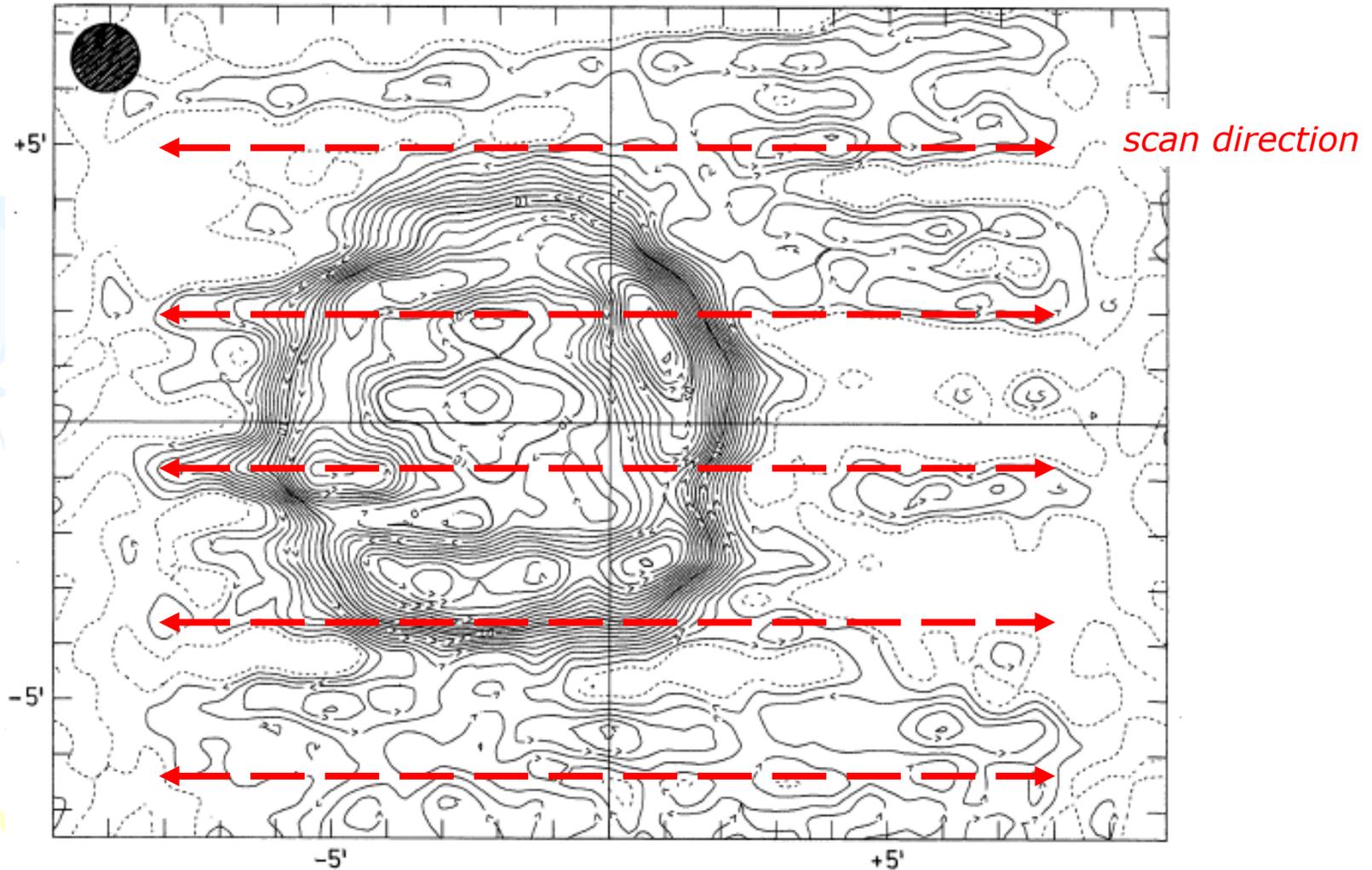


Technique can also be used for mapping extended sources

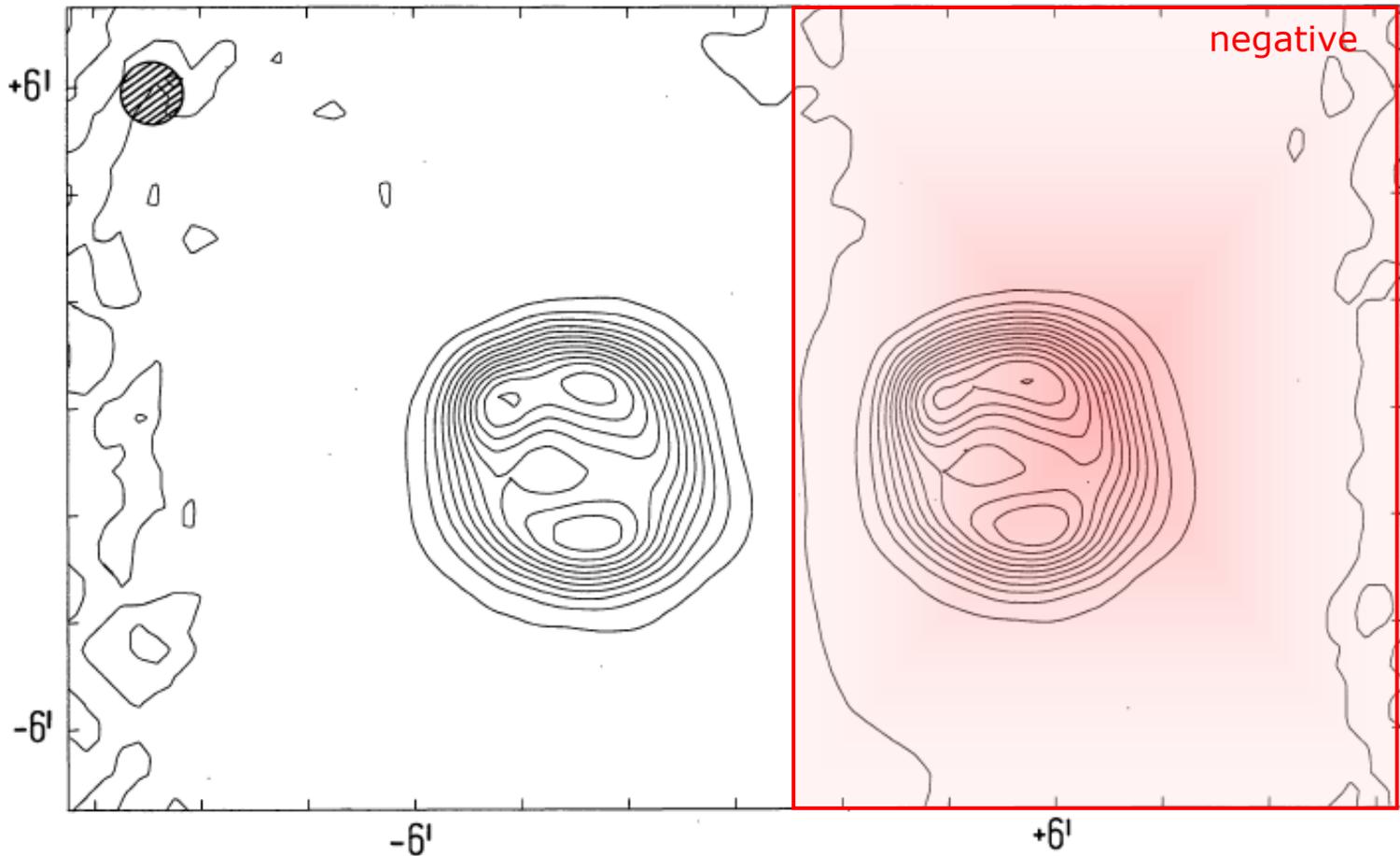
- For Effelsberg dish (100 m diameter) observing at $\lambda=2.8$ cm
- Rayleigh distance:
 $D_R \approx D^2/\lambda = 100^2/0.028 = 360$ km
- Troposphere (where water is) is at 2-3 km altitude, so should be same in both beams



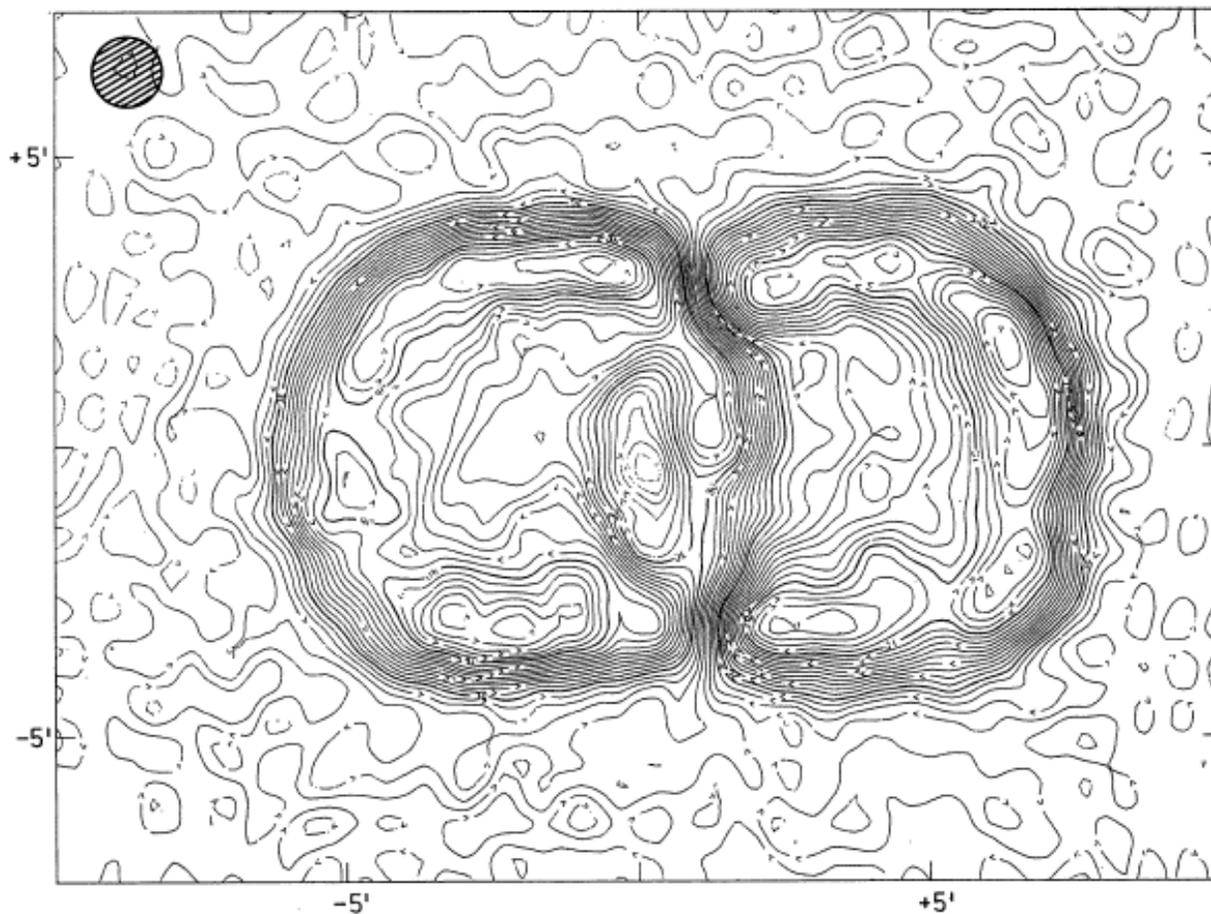
Single-beam map of 3C10, showing effects of atmosphere



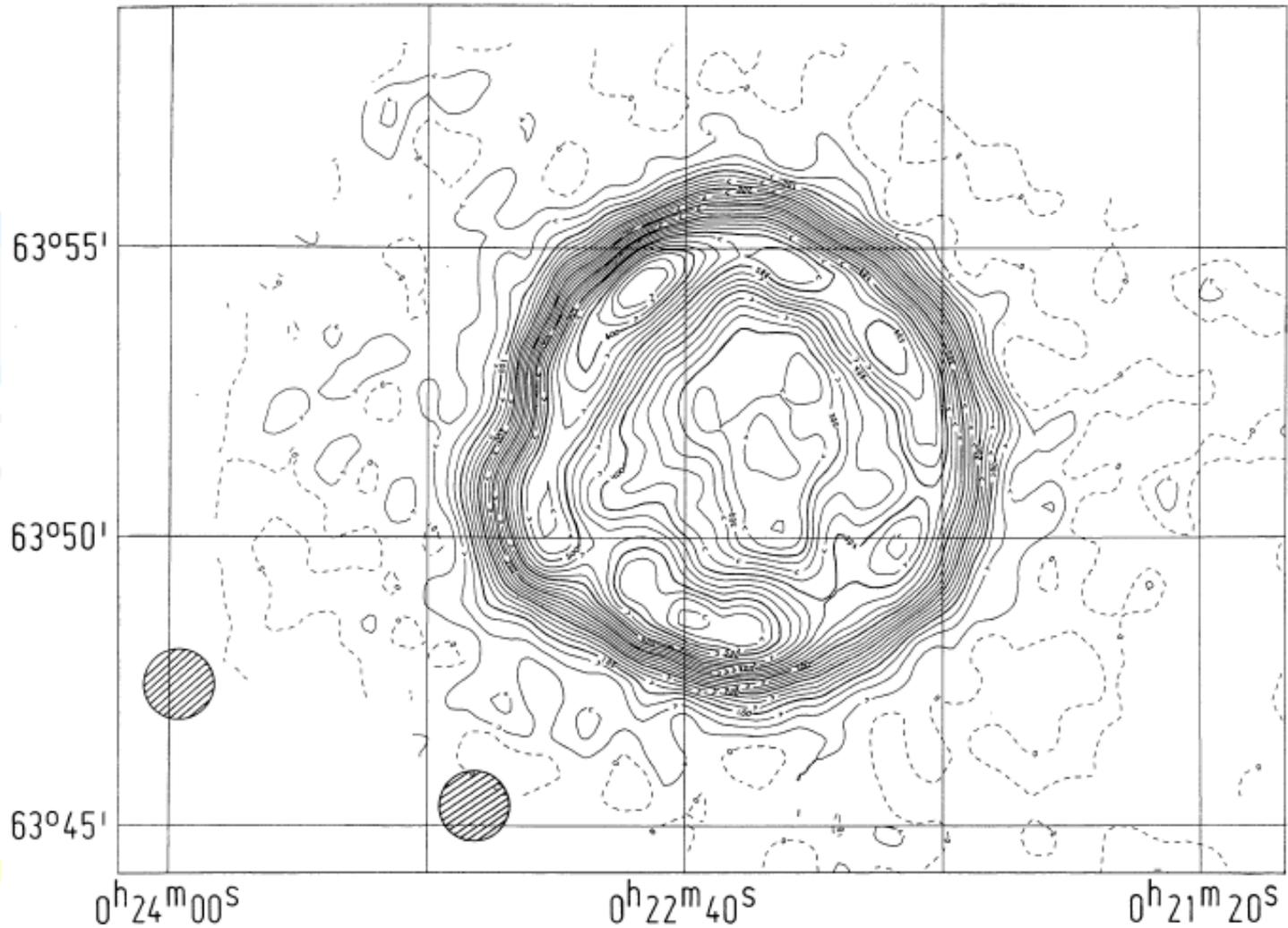
Cas A, beam separation = $8.2'$
arc: 2 images well separated



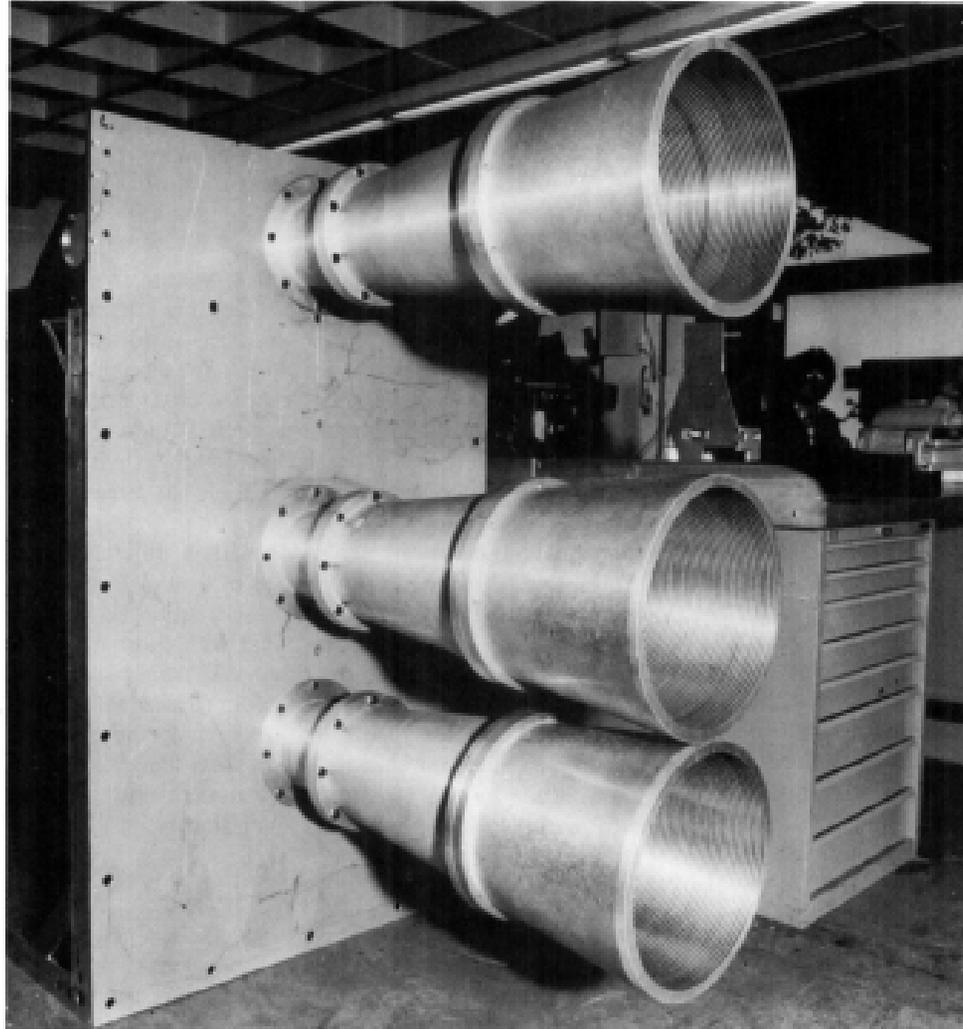
Images not always separated: 3C10, 5.5' arc beam distance



3C10, final map separates and averages two images



Triple-horn system: 3 beams are even better



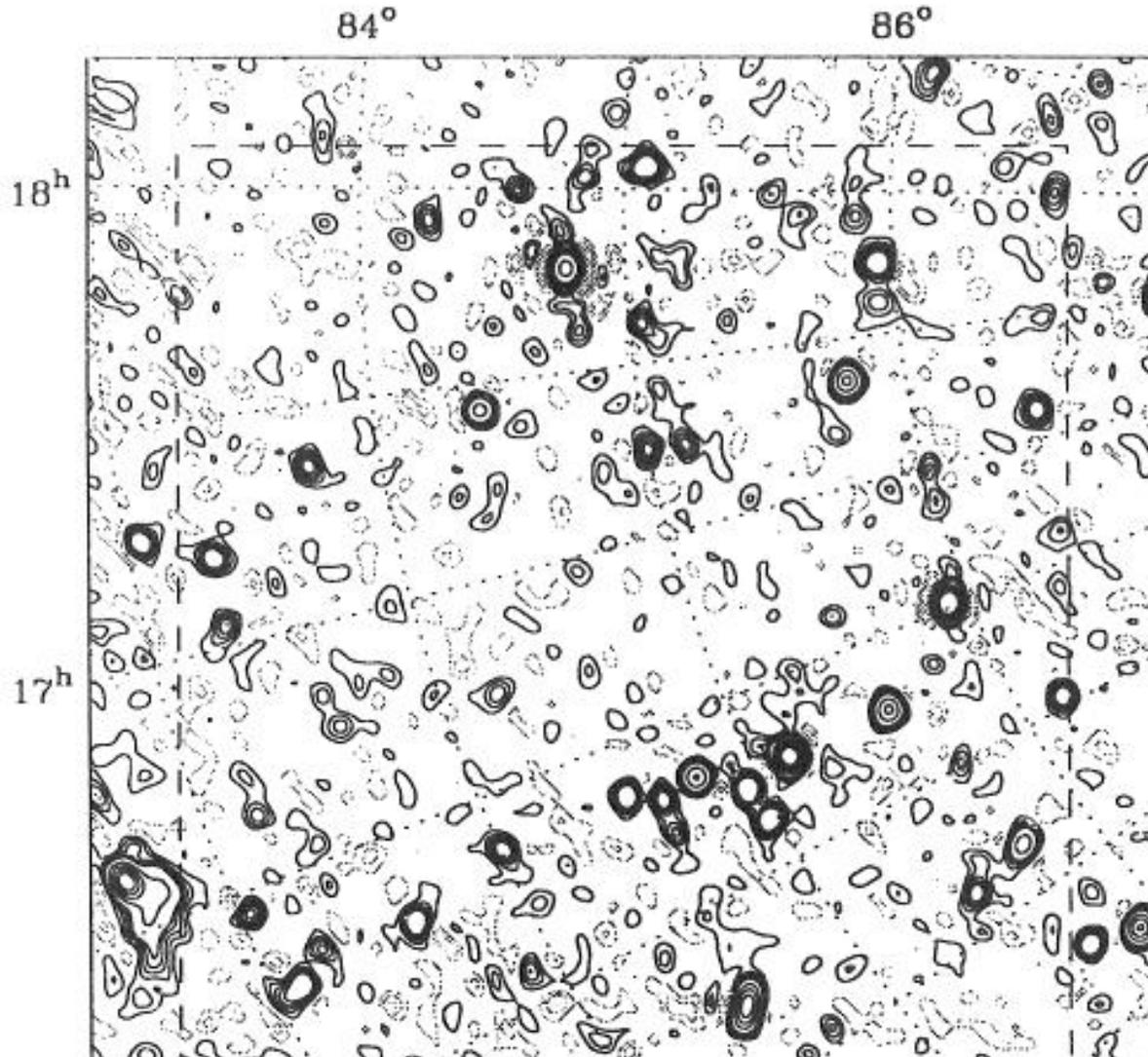
Two final sensitivity issues: polarization and confusion

- If we only observe with one antenna and receiver, we miss half the signal (for unpolarized sources).
- Must also have a second antenna with opposite sense of polarization
- Second antenna must have its own receiver system (so it costs more, but gives better sensitivity by $\sqrt{2}$)
⇒ *Why is sensitivity better by $\sqrt{2}$?*

Antenna with one polarization misses half the signal



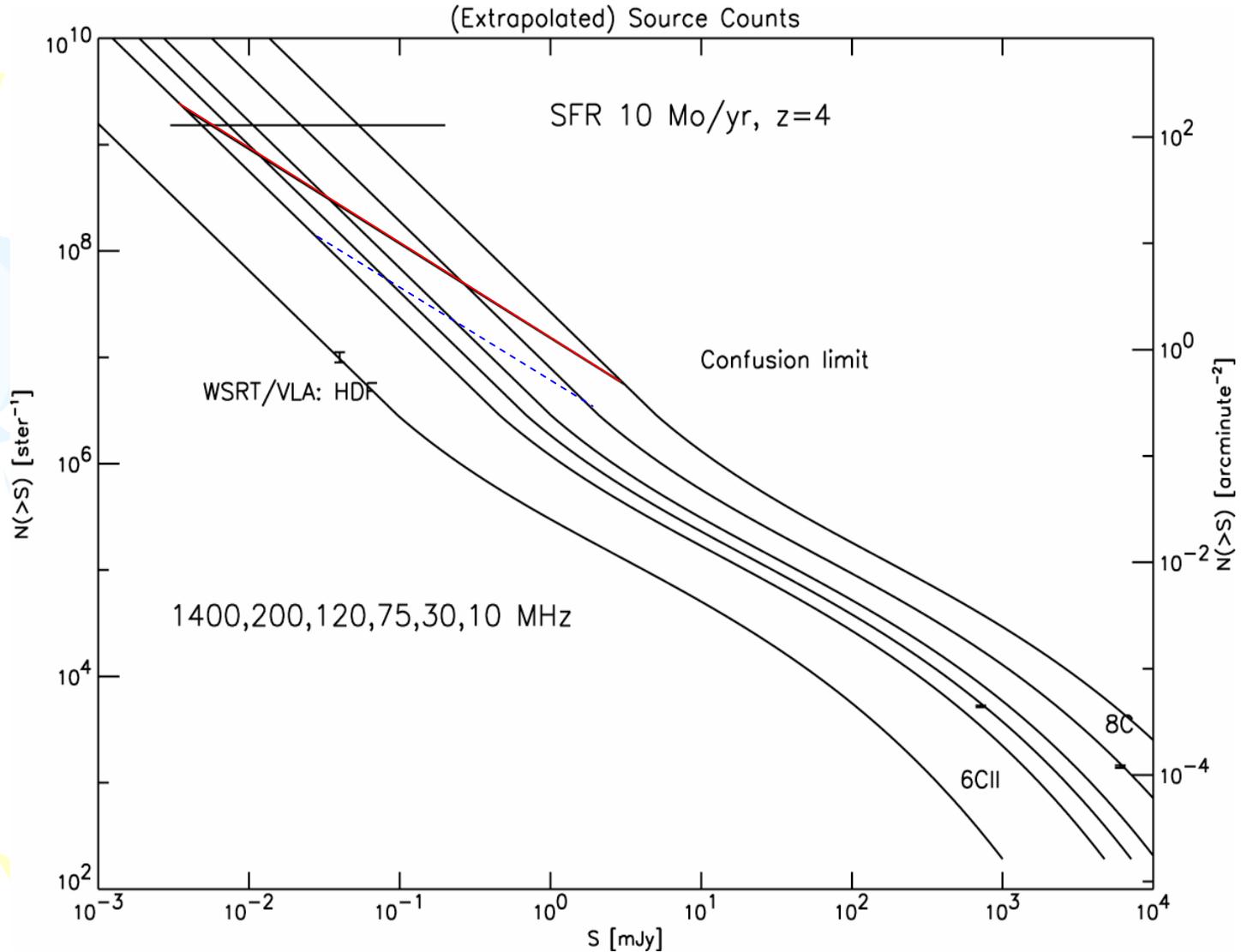
Confusion is where sources (almost) overlap each other



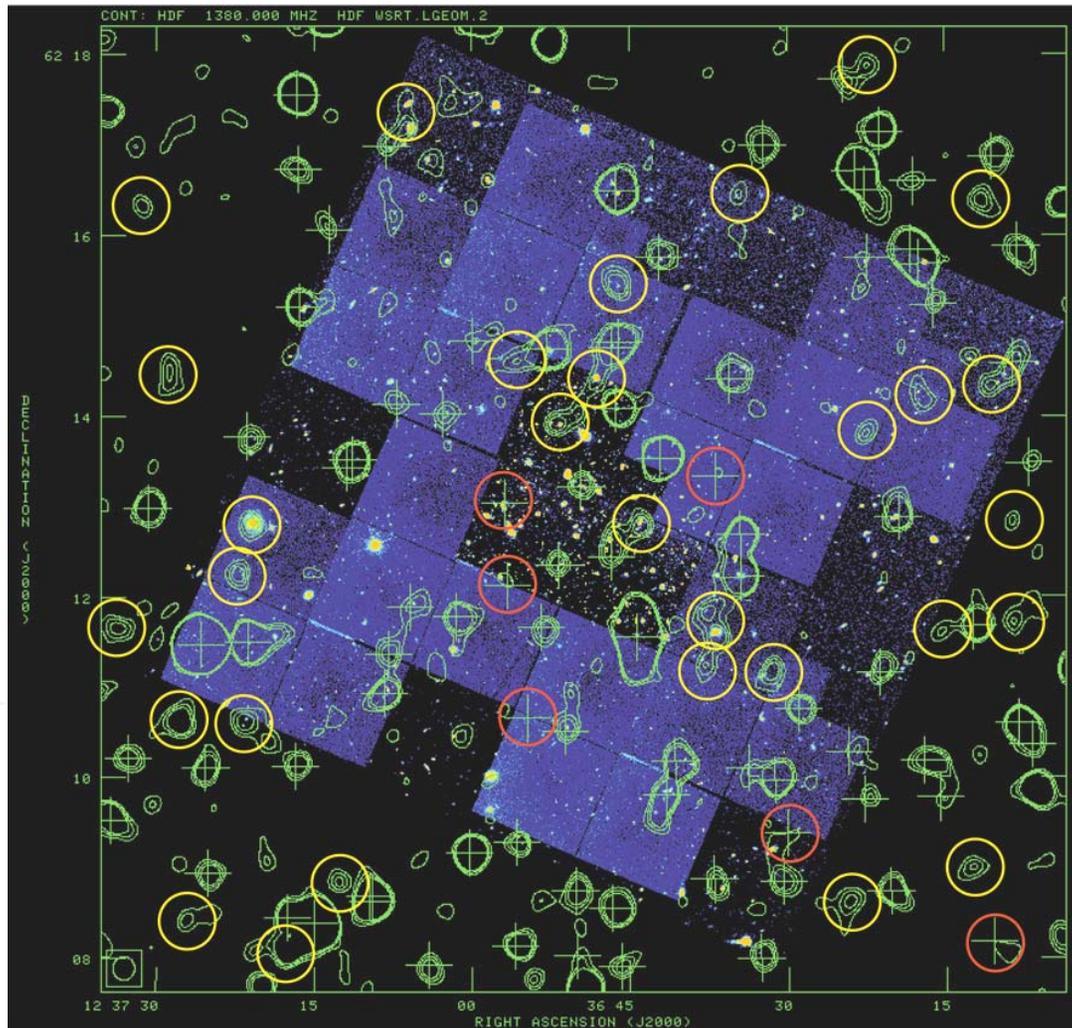
To overcome confusion requires a smaller beam

- Common definition of “confusion level” is 1 source/20 beams
- Source density increases as we go to weaker sources
- To estimate, need source number vs. strength curves (from observations); see next panel
- A more sensitive telescope needs greater angular resolution

Curves showing source density vs. S (flux density)



Hubble Deep Field (HDF), observed by WSRT & VLA



Next lecture we will look at interferometers

